





4TH INTERNATIONAL WORKSHOP ON WAVES, STORM SURGES, AND COASTAL HAZARDS

Incorporating the 18th International Waves Workshop



A weakly dispersive and fully nonlinear wave model for the simulation of nearshore wave transformation and overtopping

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Context and objectives



- Protection of coastal infrastructures (including nuclear power plants)
 and areas against flooding hazards due to waves.
- Coastal protections designed from average overtopping discharges.
- Average overtopping discharges estimated with empirical formulas (e.g. EurOtop, 2018)
 - well suited for simple configurations, invariant alongshore,
 - can be insufficient for complex sea states and/or complex nearshore bathymetry and breakwater geometry.
- → Develop and validate a **numerical <u>phase-resolving</u> model** for simulating
- irregular wave transformation in the nearshore zone,
- 2. wave breaking (and associated effects, e.g. wave setup),
- average overtopping discharges over coastal protections.



Coastal nuclear power plant



Wave overtopping

1HD wave model



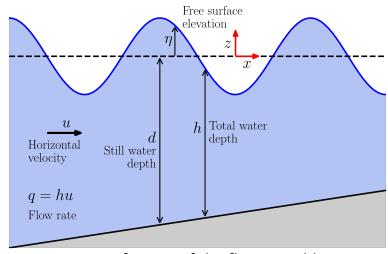
- Mathematical model: enhanced Serre-Green-Naghdi (eSGN) equations (Bonneton et al., 2011)
- Decoupled form, separating the hydrostatic NLSWE and the dispersive part (Kazolea et al., 2023):

$$h_t + q_x = 0$$

$$q_t + (hu^2)_x + gh\eta_x = \Phi$$

$$\Phi = \Psi + \frac{gh}{\alpha}\eta_x$$

$$(I + \alpha \mathcal{T})\Psi = -\frac{gh}{\alpha}\eta_x - Q + D_{wb}$$



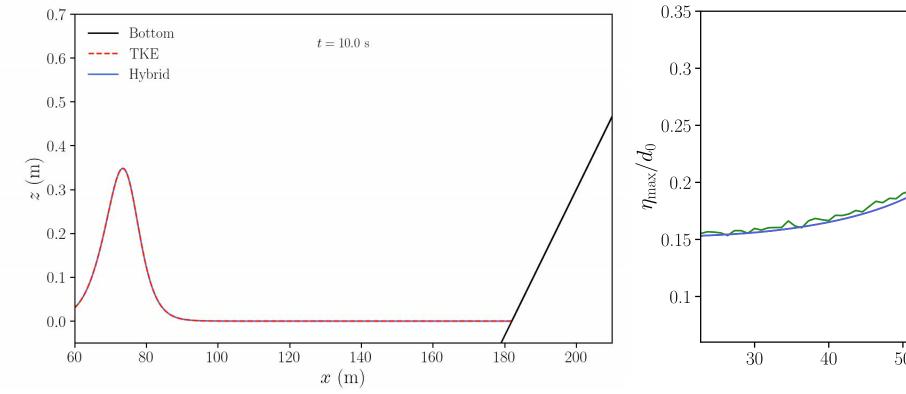
Definition of the flow variables

- Two wave-breaking modelling strategies tested:
 - 1) neglect dispersion (Φ) to model breaking waves as **shocks** with the NLSWE (=> **hybrid** approach),
 - 2) add the energy dissipation term $D_{wb} = (2v_T h u_x)_x$ with v_T computed with a one-equation turbulence model on the turbulent kinetic energy (**TKE**).
- Numerical methods:
 - NLSWE solved with 3rd or 4th order finite volume (FV) MUSCL schemes,
 - Dispersive terms discretised with 2nd order finite difference (FD) scheme.

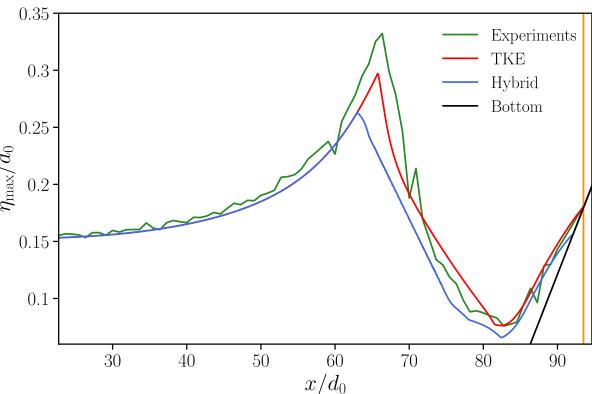
Comparison of the two wave-breaking approaches



- Experiments of solitary wave propagation, shoaling and breaking from Hsiao et al. (2008)
- **Decrease in amplitude** well captured with both approaches
- Oscillations produced by the hybrid approach, prevents use of fine meshes → TKE favoured for further applications



Shoaling and breaking of a solitary wave $(a/d_0 = 0.152)$ with both breaking approaches



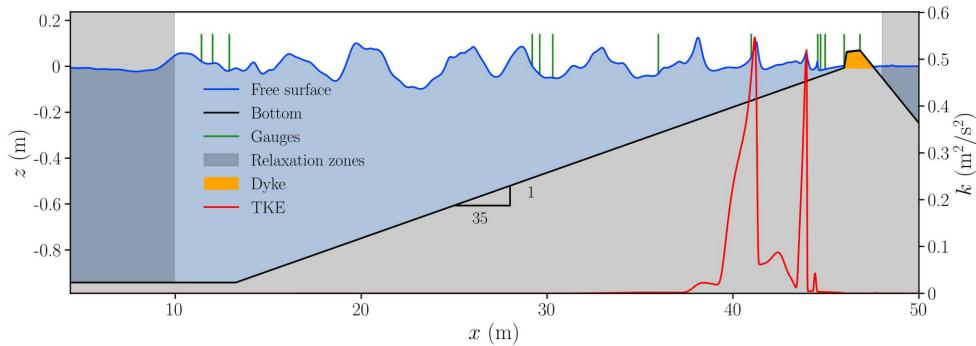
Spatial evolution of the solitary wave amplitude ($a/d_0 = 0.152$) in the experiments and with both breaking approaches

The wave overtopping experiments (Altomare et al., 2016; Suzuki et al., 2017)



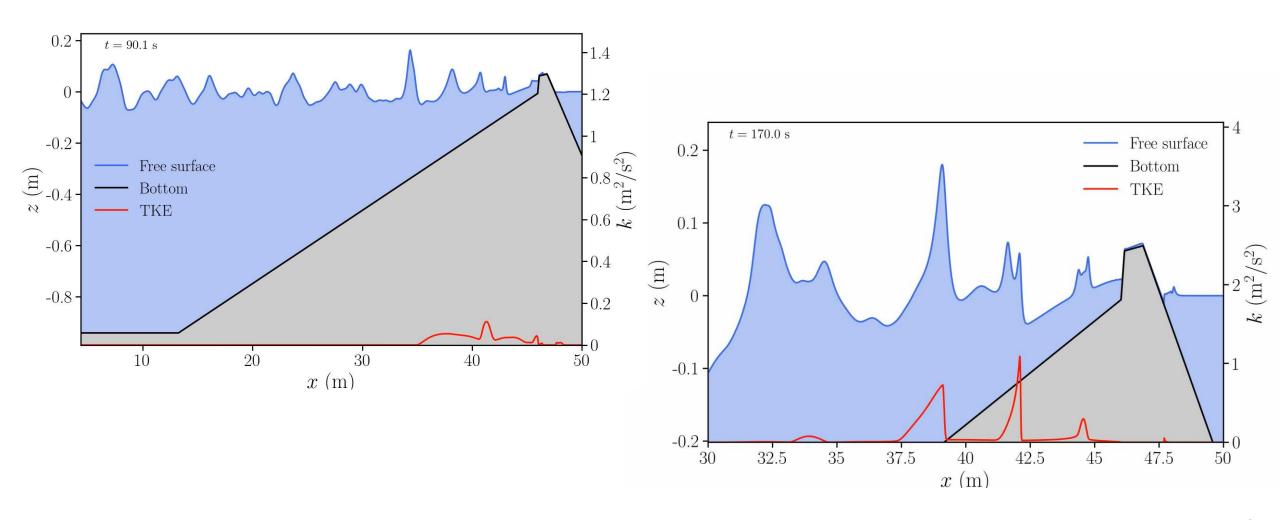


- Overtopping experiments in a wave flume by Flanders Hydraulics, Belgium
- **3 dyke slopes**: 1:2, 1:3 or 1:6
- Foreshore slope 1:35 → significant wave transformations and intense breaking
- Irregular sea states with $H_{m0} \in [11, 25]$ cm and $T_p \in [2, 2.5]$ s
- 111 trials, all simulated over the full duration \approx 40 min, i.e. more than 1000 waves, with the TKE breaking model.





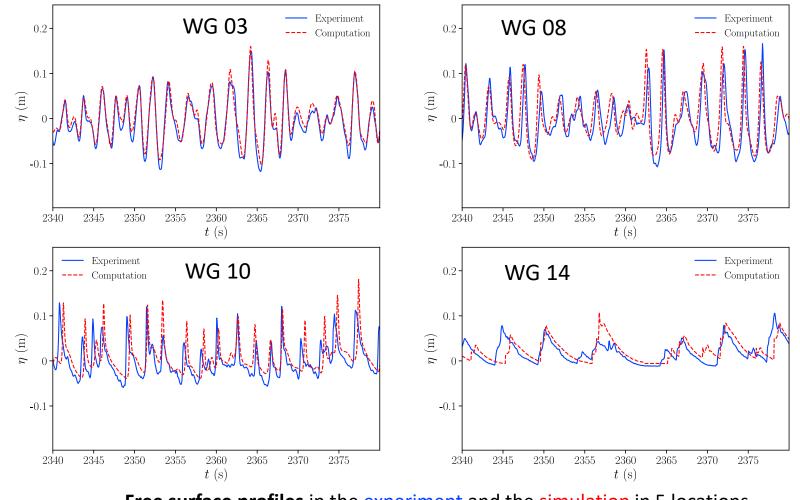
Visualisation of wave breaking and wave overtopping



Free surface profiles



• Mean index of agreement d_r (Willmott *et al.*, 2012) for the 111 cases: **0.85** for the deep-water gauges (**very good**), **0.64** for all gauges (**reasonable**)



 Experiment WG 09 ---- Computation 2360 2345 2350 2355 2365 2370 2375 2340 t (s) 0.2 G08 G09 G10 G14 G03 Free surface -0.2 (E) -0.4 Bottom Wave gauges Relaxation zone -0.6 -0.8 20 30 40 x (m)

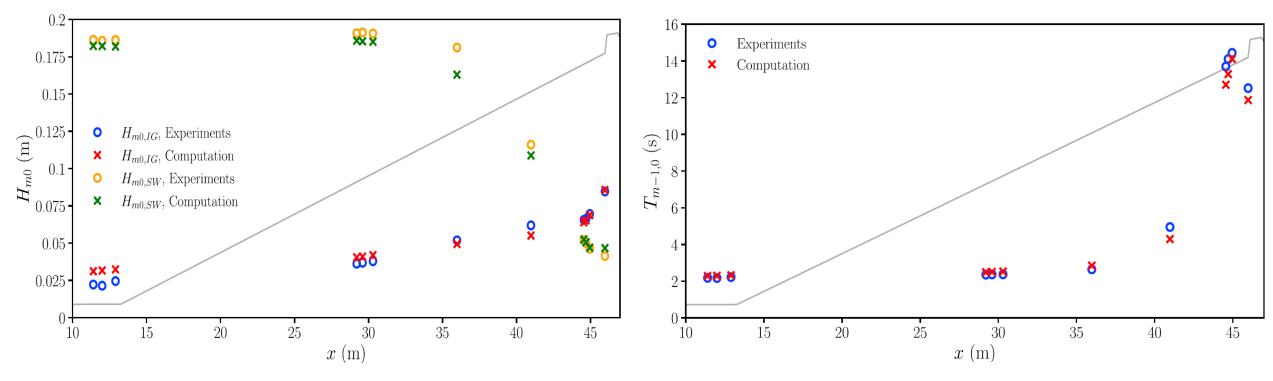
Position of the gauges

Free surface profiles in the experiment and the simulation in 5 locations Slope 1:2, h = 0.942 m, $H_{m0} = 0.189$ m, $T_n = 2.13$ s

Significant wave height and energy period







Spatial evolution of the **infragravity** and **short waves significant** wave heights H_{m0} in the experiment and the simulation

Spatial evolution of the **energy period** $T_{m-1,0}$ in the experiment and the simulation

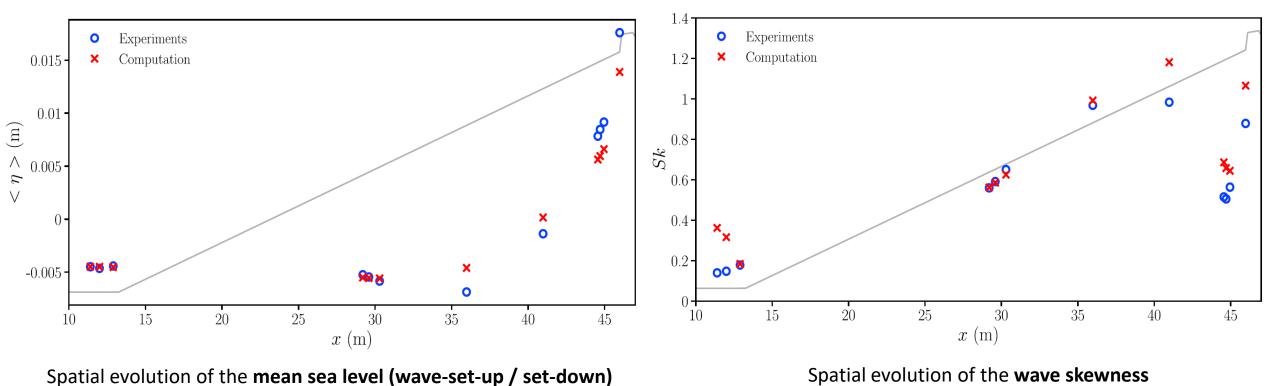
Wave setup and skewness

in the experiment and the simulation



in the experiment and the simulation

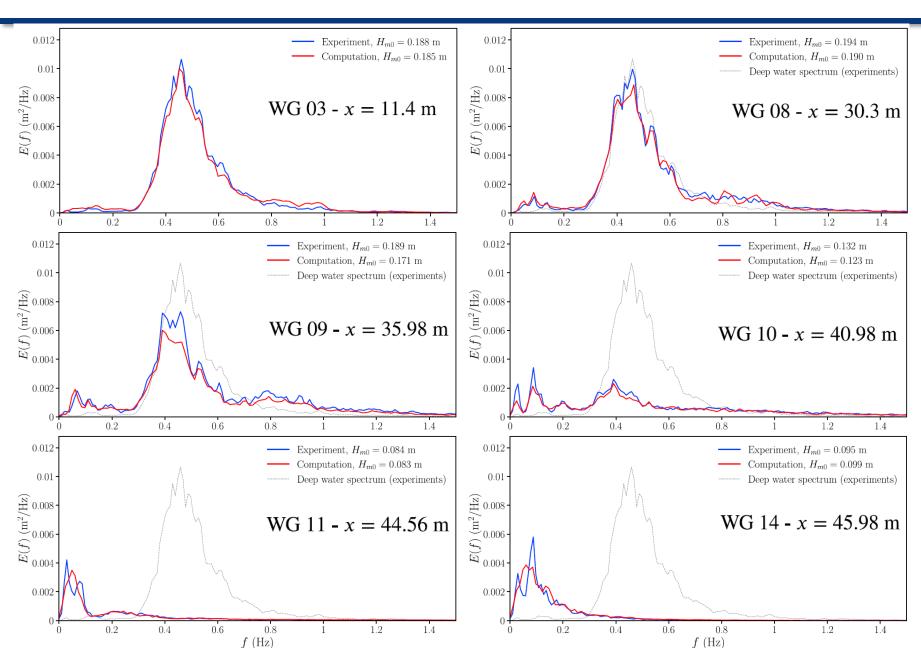




Case with slope 1:2, h = 0.942 m, $H_{m0} = 0.189 \text{ m}$, $T_p = 2.13 \text{ s}$

Total wave spectra

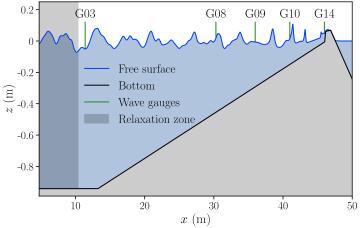




Total wave spectra in the experiment and the simulation at 6 locations.

Slope 1:2, h = 0.942 m,

$$H_{m0} = 0.189$$
 m, $T_p = 2.13$ s



Grid convergence on the average discharge



 Representative wavelength of the incident waves at the toe of the dike:

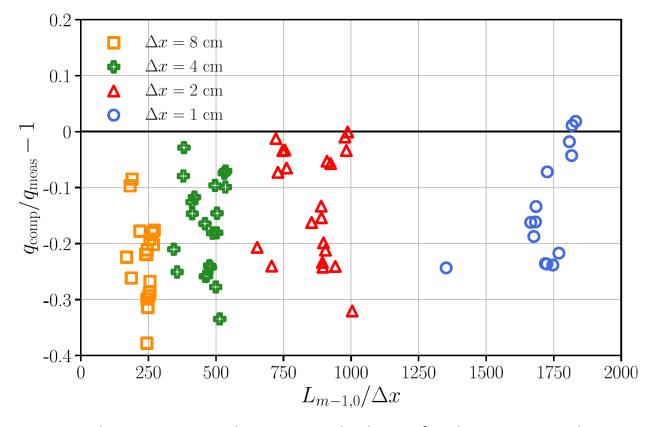
$$L_{m-1,0} = T_{m-1,0} \sqrt{g(d+H_{m0})}$$

- No instabilities when using fine grid sizes
- Computational time:

$$1000 - 1400$$
 waves (40 min) CFL = 0.3

- $\rightarrow \Delta x = 2 \text{ cm}$: $\approx 3 \text{ hours}$
- $\rightarrow \Delta x = 1 \text{ cm}$: $\approx 13 \text{ hours}$

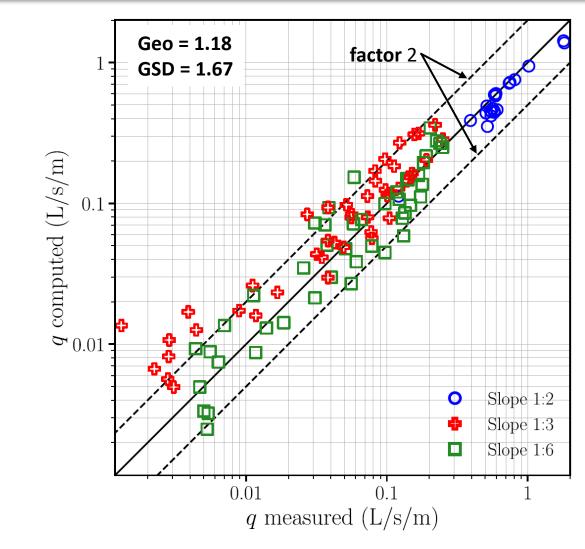
on one core of an Intel Xeon 6140 processor



Relative error on the average discharge for decreasing grid sizes for the 21 cases with dike slope 1:2

Average overtopping discharges (all 111 tests – log scale)





$$\mathrm{Geo} = \mathrm{exp}\left(\overline{\ln\left(rac{q_{\mathrm{comp}}}{q_{\mathrm{meas}}}
ight)}
ight)$$
 $\mathrm{GSD} = \mathrm{exp}\left(\sqrt{\overline{\ln\left(rac{q_{\mathrm{comp}}}{q_{\mathrm{meas}}}
ight)^2 - \ln\left(\mathrm{Geo}
ight)^2}}
ight)$

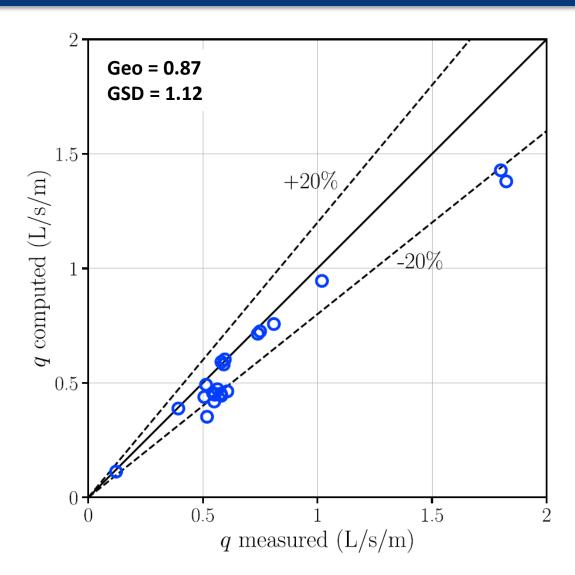
Dataset	N	Relative error (%)	Geo	GSD
00-025	21	13	0.87	1.12
13–116	90	67	1.27	1.72
All	111	57	1.18	1.67

- Good agreement on the average discharge over 3 orders of magnitude
- Mean absolute relative error = 57 %
- Higher scatter for lower discharges

Average overtopping discharges (21 tests of dataset 00-025 – linear scale)







$$\mathrm{Geo} = \mathrm{exp}\left(\overline{\ln\left(rac{q_{\mathrm{comp}}}{q_{\mathrm{meas}}}
ight)}
ight)$$
 $\mathrm{GSD} = \mathrm{exp}\left(\sqrt{\overline{\ln\left(rac{q_{\mathrm{comp}}}{q_{\mathrm{meas}}}
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Dataset	N	Relative error (%)	Geo	GSD
00-025	21	13	0.87	1.12
13–116	90	67	1.27	1.72
All	111	57	1.18	1.67

• For cases with slope 1:2 (O), mean error = 13 %

(b) Dataset 00-025 only (21 tests), plotted using a linear scale. The dashed lines indicate overestimation or underestimation by 20%.

Conclusions and future work

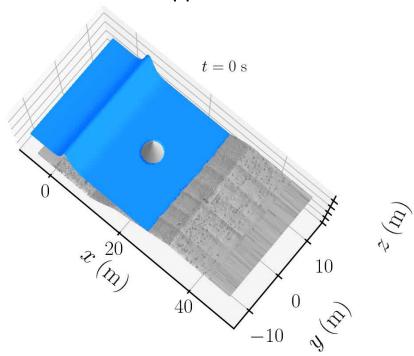


Conclusions

- Validation of our depth-averaged eSGN wave model for simulating the transformations of irregular sea states
 due to shoaling and intense breaking.
- Experimental validation for the overtopping of smooth dikes by irregular breaking waves (111 trials with over 1000 waves each)
- Reasonable computational time (a few hours with one processor) → potential industrial applications

Ongoing and future work

- Development of a 2HD model and experimental validation
- Application to realistic cases in 2HD
- Overtopping of porous structures
- Simulation of cases with vertical sea-walls







For all details and other validation cases, see:

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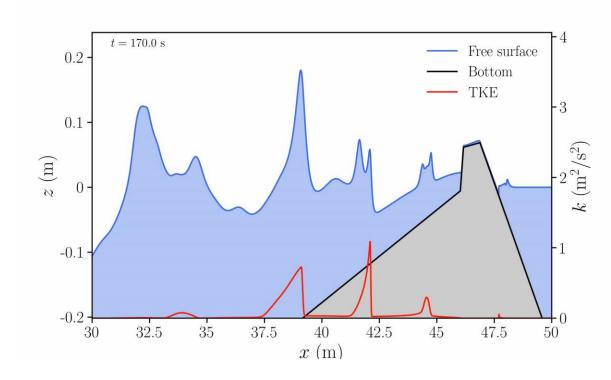
Coastal Engineering

journal homepage: www.elsevier.com/locate/coastaleng



Numerical modelling of nearshore wave transformation, breaking and overtopping of coastal protections with the enhanced Serre–Green–Naghdi equations

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Thank you for your attention!

We thank Flanders Hydraulics and Pr. Tomohiro Suzuki (now at KU Leuven) for sharing the data from the overtopping experiments

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Complete eSGN model of Bonneton et al. (2011)

$$h_t + q_x = 0$$

• Momentum eq.:
$$q_t + (hu^2)_x + gh\eta_x = \Phi$$

$$\Phi = \Psi + \frac{gh}{\alpha}\eta_x$$

$$(I + \alpha \mathcal{T})\Psi = -\frac{gh}{\alpha}\eta_x - Q$$

$$Q(u) = 2h^2h_xu_x^2 + rac{4}{3}h^3u_xu_{xx} - h^2d_xu_x^2 - h^2d_{xx}uu_x - ig[h_xd_{xx} + rac{1}{2}hd_{xxx} - d_xd_{xx}ig]hu^2$$

$$\mathcal{T}(v) = \left[rac{1}{3}(h_x^2 + h h_{xx}) + d_x^2 - h_x d_x - rac{1}{2}h d_{xx}
ight]v - rac{1}{3}h h_x v_x - rac{1}{3}h^2 v_{xx}$$



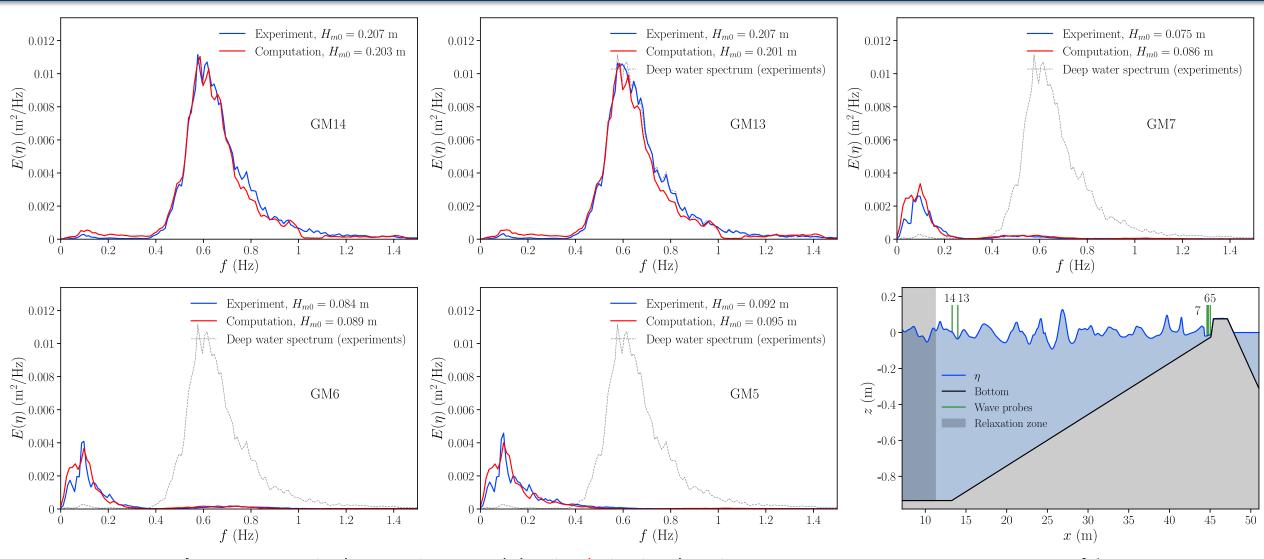
Wave breaking model

- Turbulent viscosity: $u_T = C_{
 u} \sqrt{k} l_T, \; l_T = \kappa h$
- $(hk)_t + (huk)_x = h
 u_T k_{xx} + Brac{hl_T^2}{\sqrt{C_
 u^3}} |u_z(z=\eta)|^3 hC_
 u^3 rac{k^{3/2}}{l_T}.$ • Transport equation for the TKE k:

Appendix – Total wave spectra for one case with slope 1/3





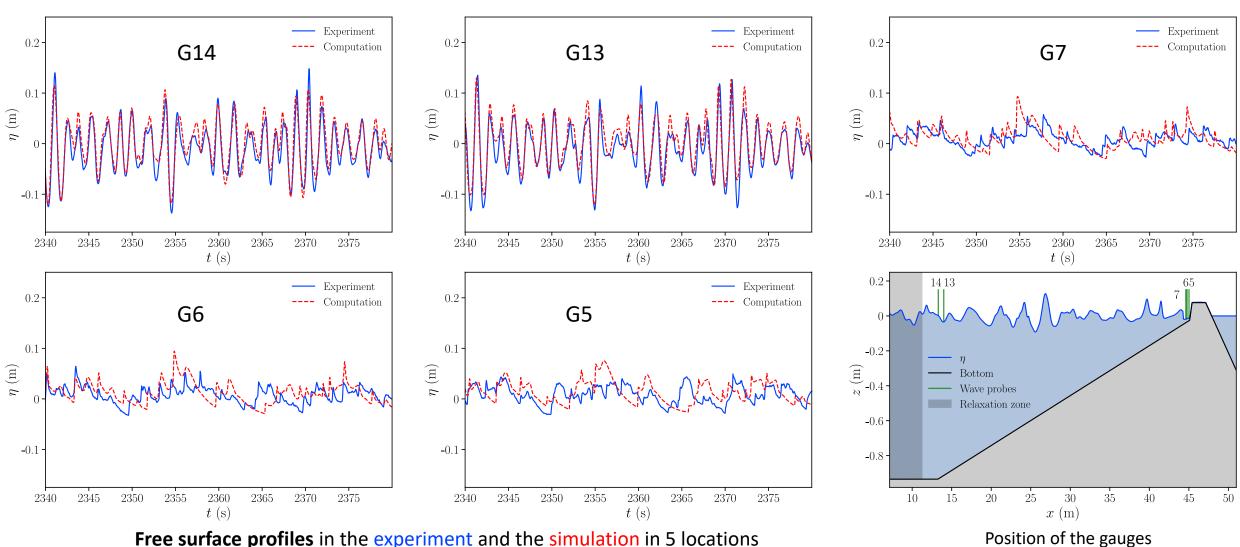


Total wave spectra in the experiment and the simulation in 5 locations Slope 1/3, water depth = 0.935 m, $H_{m0} = 0.201$ m, $T_p = 1.7$ s

Position of the gauges

Appendix – Free surface profiles for one case with slope 1/3





Free surface profiles in the experiment and the simulation in 5 locations Slope 1/3, water depth = 0.935 m, $H_{m0}=0.201$ m, $T_p=1.7$ s