

Wave Field Reconstruction and Prediction using X-Band Marine Radar



R. Carrasco, J.C. Nieto-Borge, J. Seemann and J. Horstmann.
Institute of Coastal Ocean Dynamics
Helmholtz-Zentrum Hereon, Geesthacht, Germany

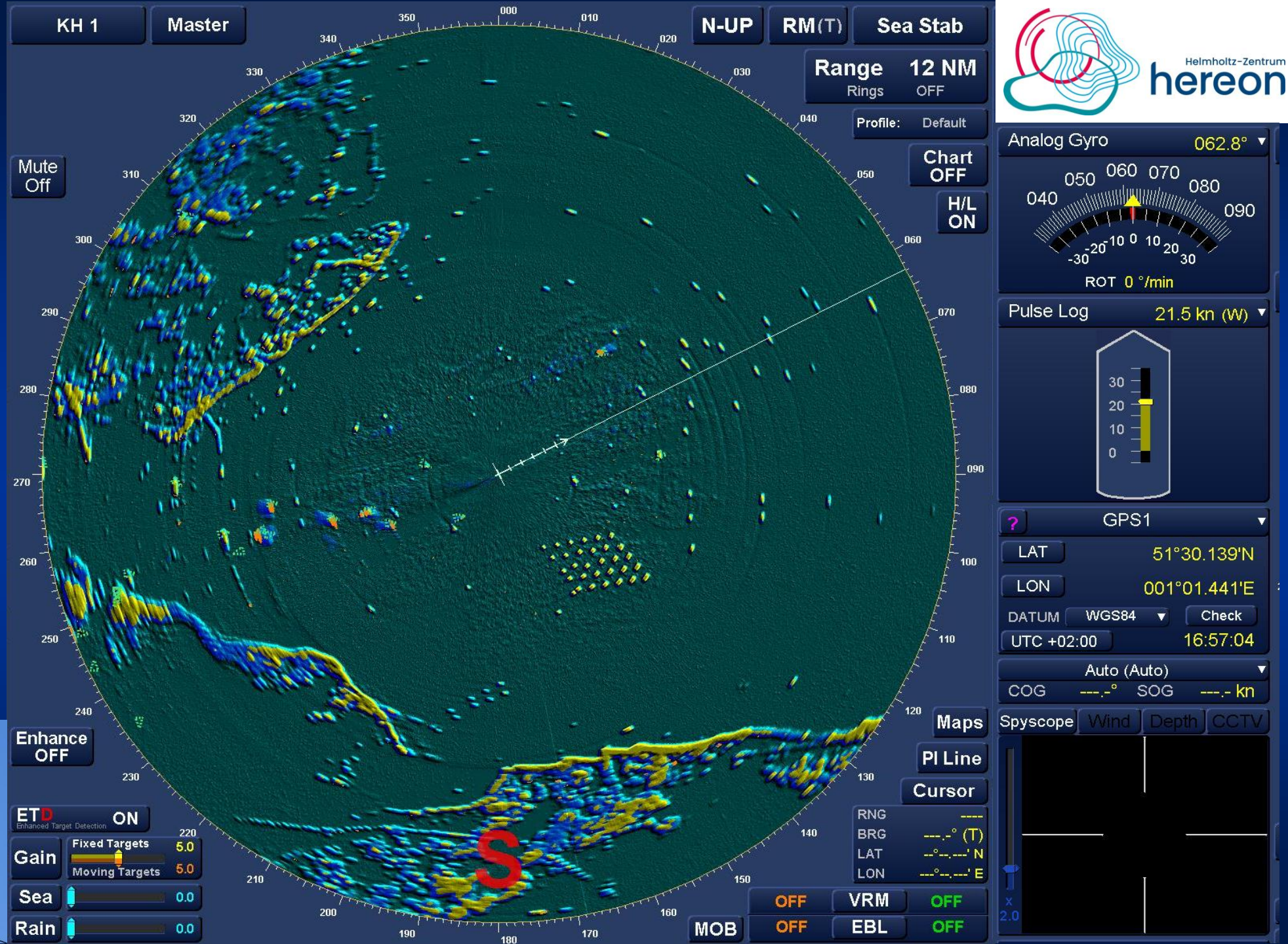


Gefördert durch:



aufgrund eines Beschlusses
des Deutschen Bundestages

Typical use of X-Band Radars



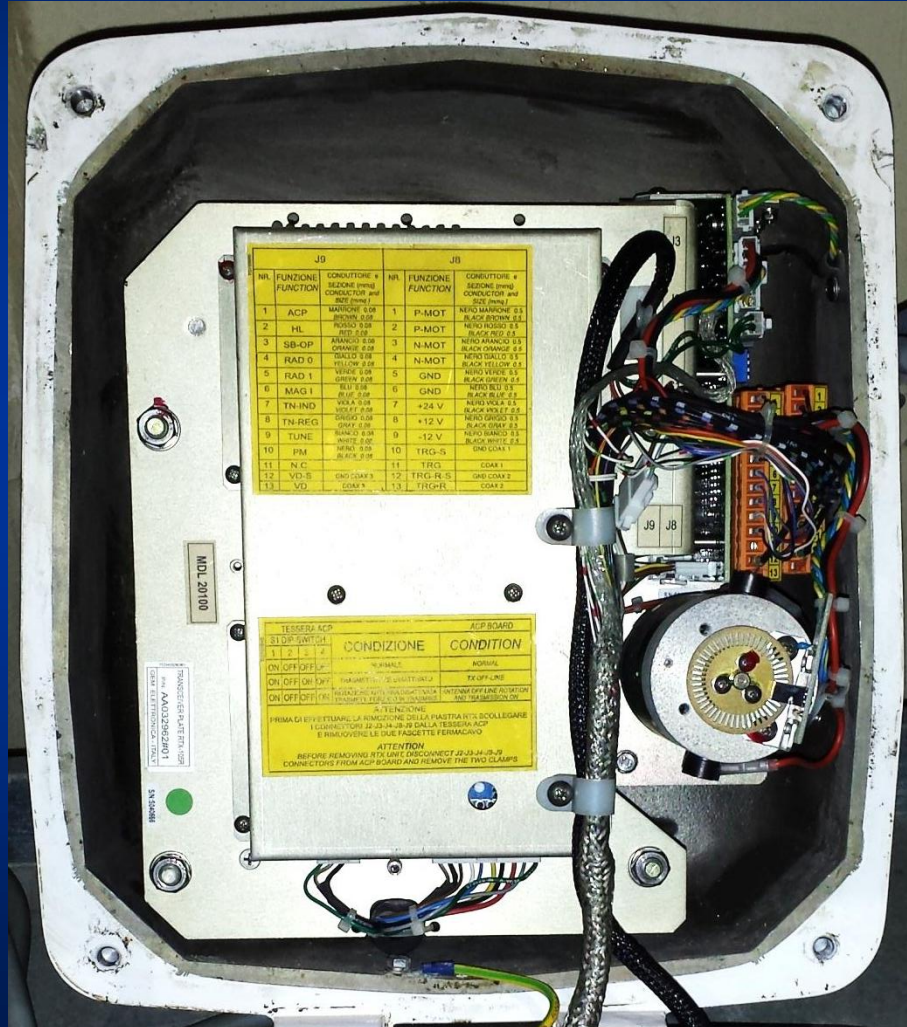
Main Radar Imaging Mechanisms

- Bragg scattering: Image intensity \propto Bragg wave intensity
- Wave-current interaction
- Contributions of longer waves
 - Tilt modulation
 - Hydrodynamic modulation
- Further modulation mechanisms

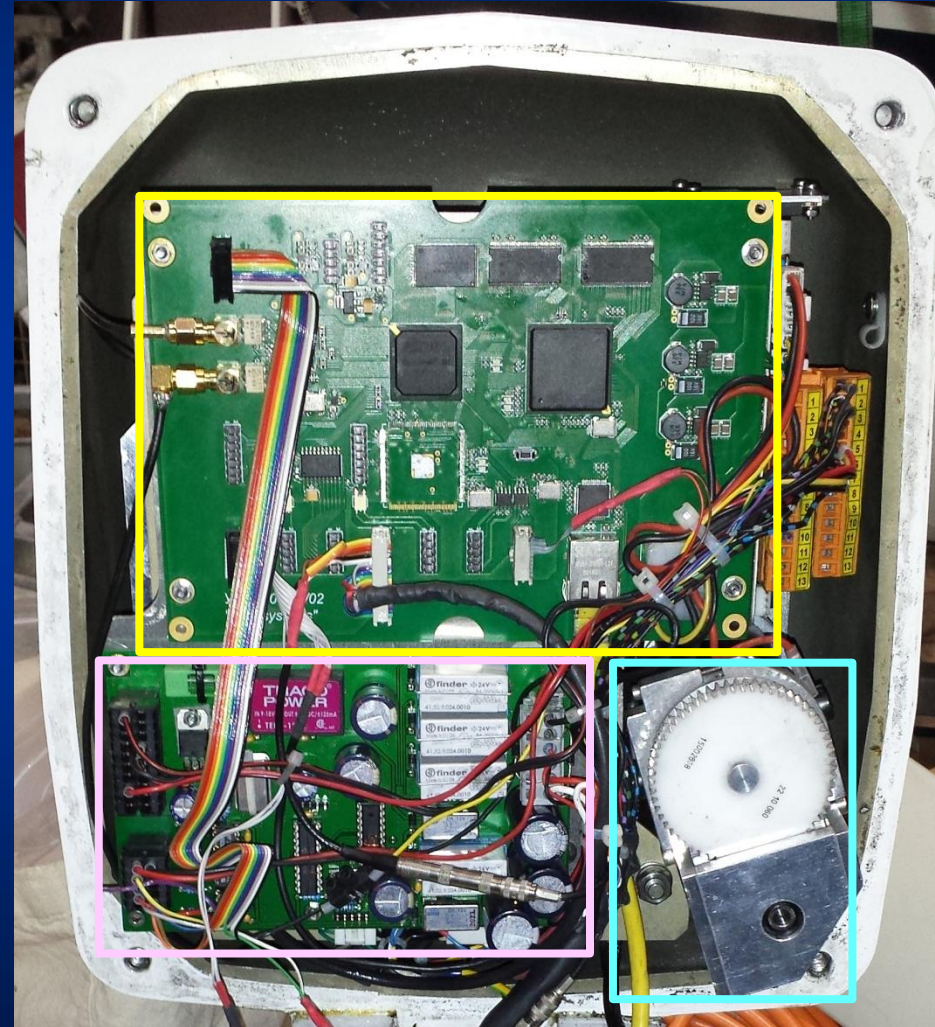


Hereon Coherent Marine Radar

Original GEM 12 kw Radar



Hereon modified Radar



- Acquisition Board
- Low noise Linear amplifier
- Step Motor
- Motor control Board
- Software for Radar data acquisition, adapted for scientific use

Hereon Marines Radar

Bunkerhill, Sylt



**X-Band (9.3 GHz)
4, 12 and 25 kW
4 - 12 feet Antenna
HH & VV-Polarization
Incoherent and Coherent
7.5 m range resolution
Up to 0.6° radial resolution**

FS Merian

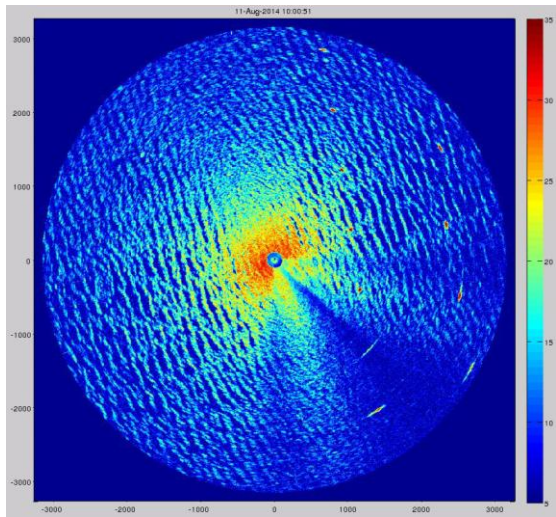


FINO-3, German Bight

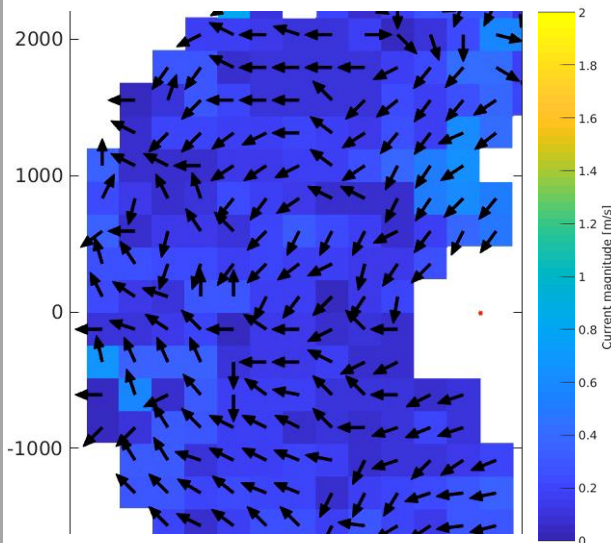


Main Marine Radar Applications

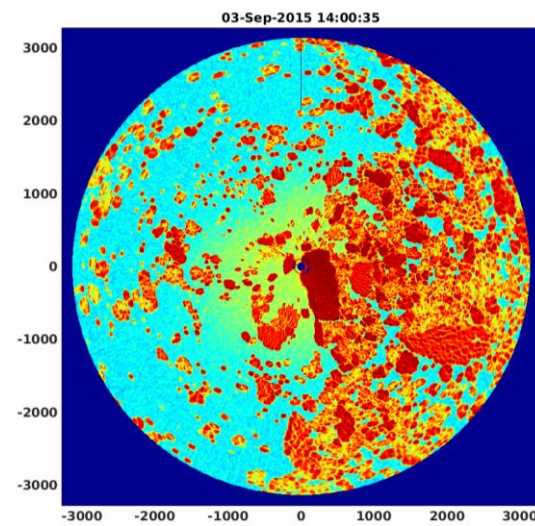
Seastate



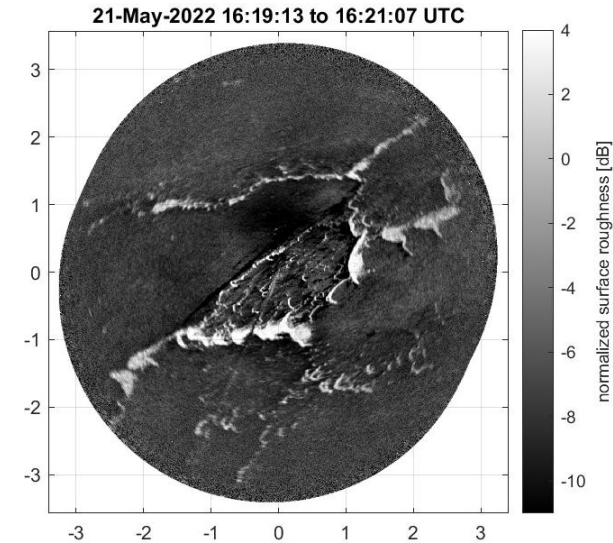
Currents



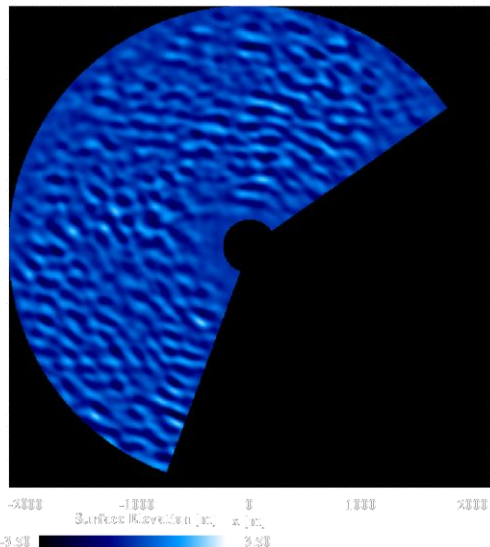
Sea Ice



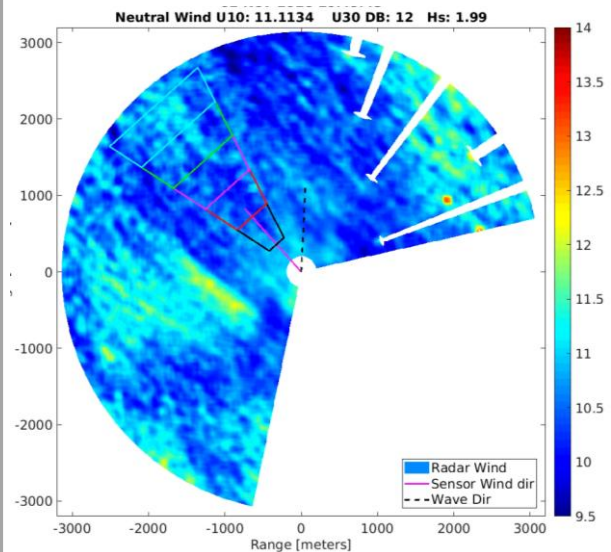
Sargassum flows



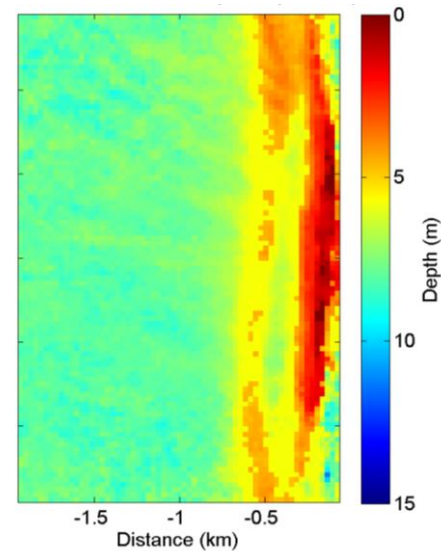
Individual Waves



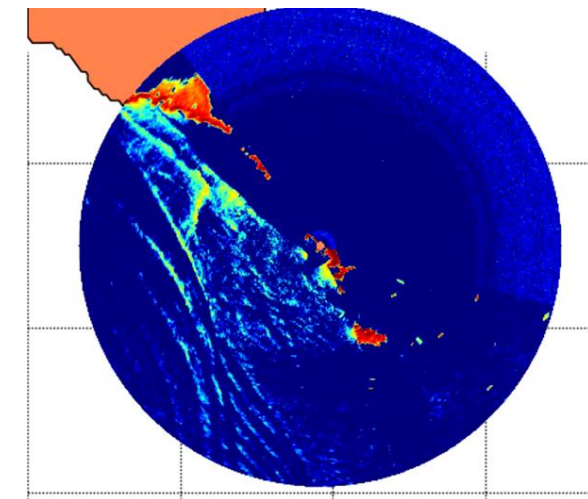
Wind



Bathymetry



Internal Waves

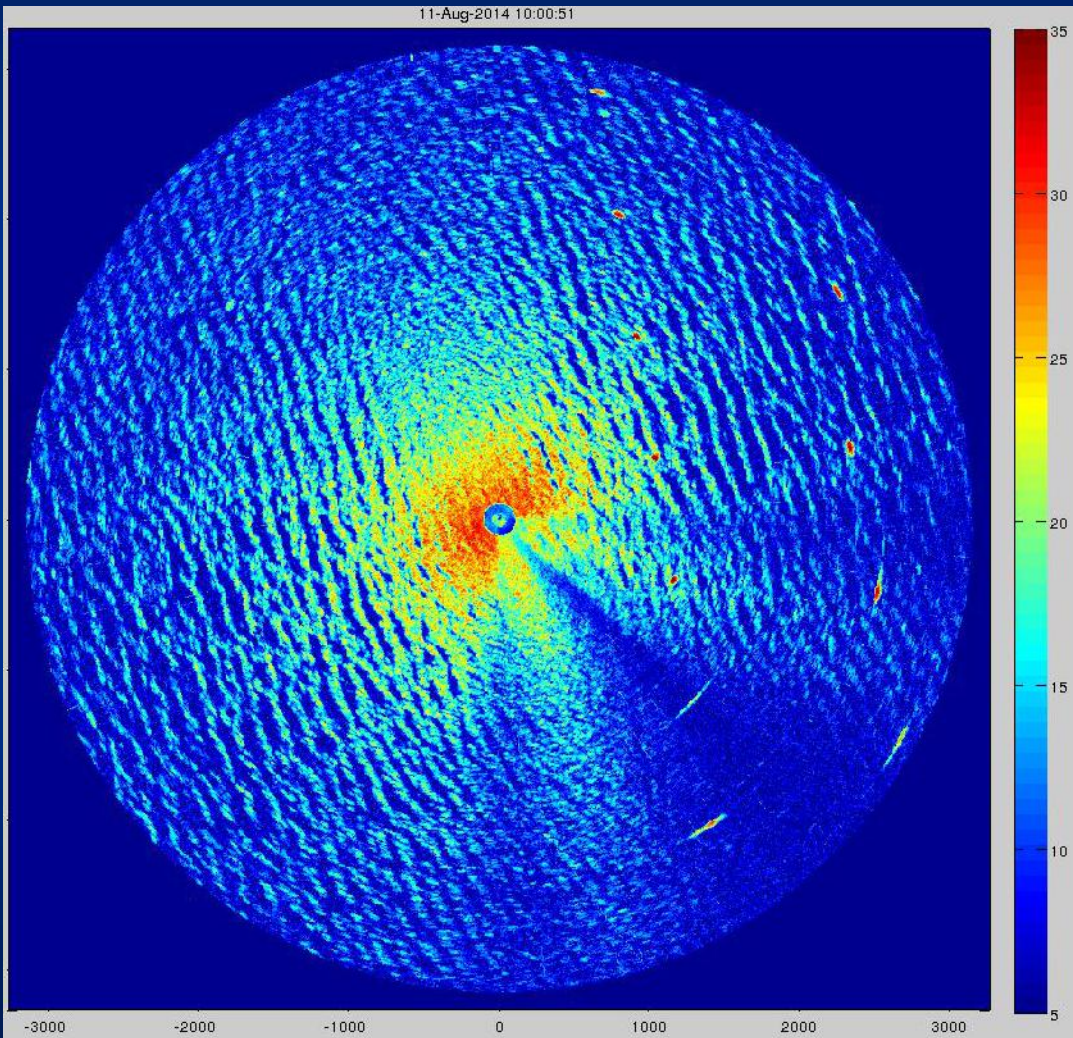


Marine Radar on FINO-3

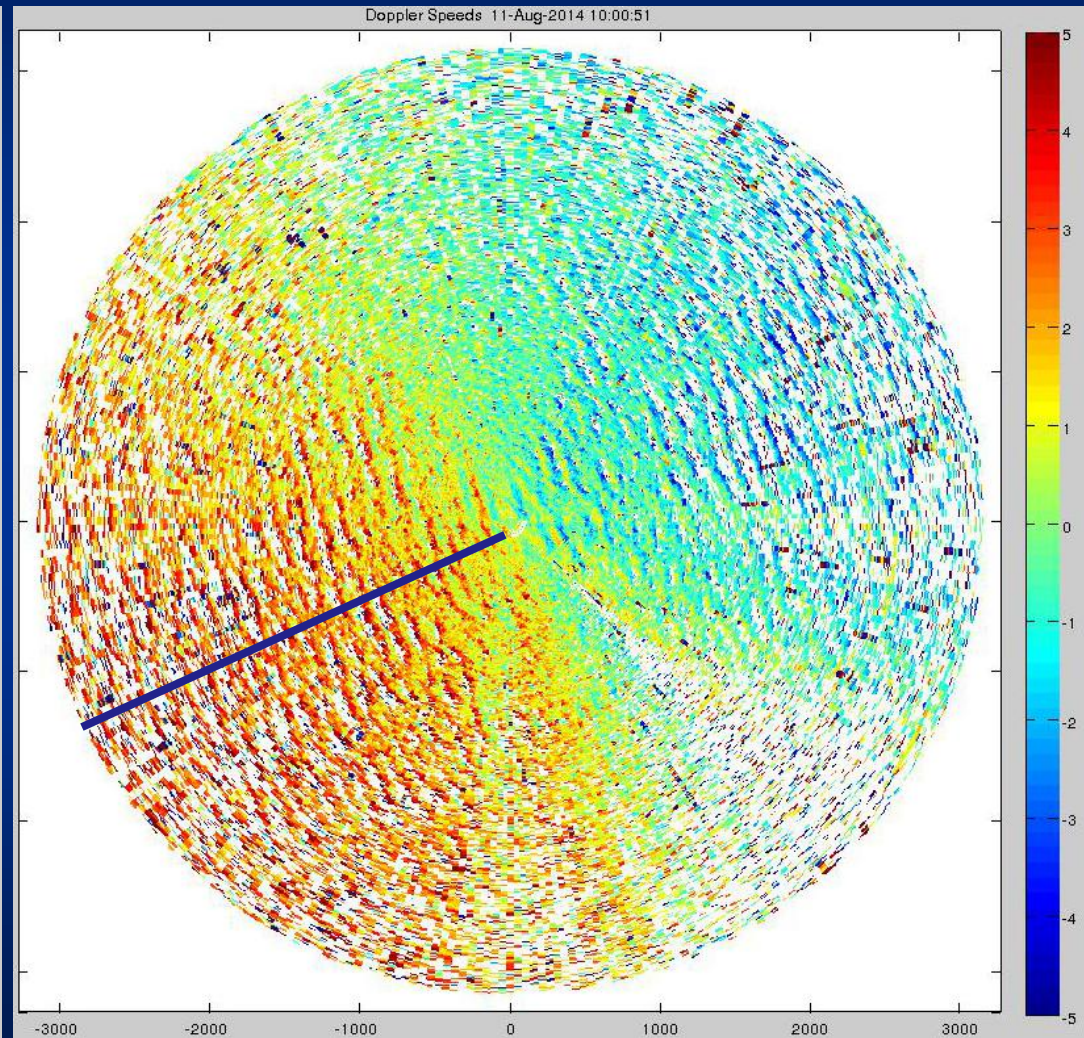


Wave Measurements with the Coherent Marine Radar

$$\mathbf{u}_{\text{tot}} = \mathbf{u}_{\text{wind}} + \mathbf{u}_{\text{cur}} + \mathbf{u}_{\text{orb}} + \mathbf{u}_{\text{break}} + \mathbf{u}_{\text{shad}} + \mathbf{u}_{\text{rest}}$$



Intensity

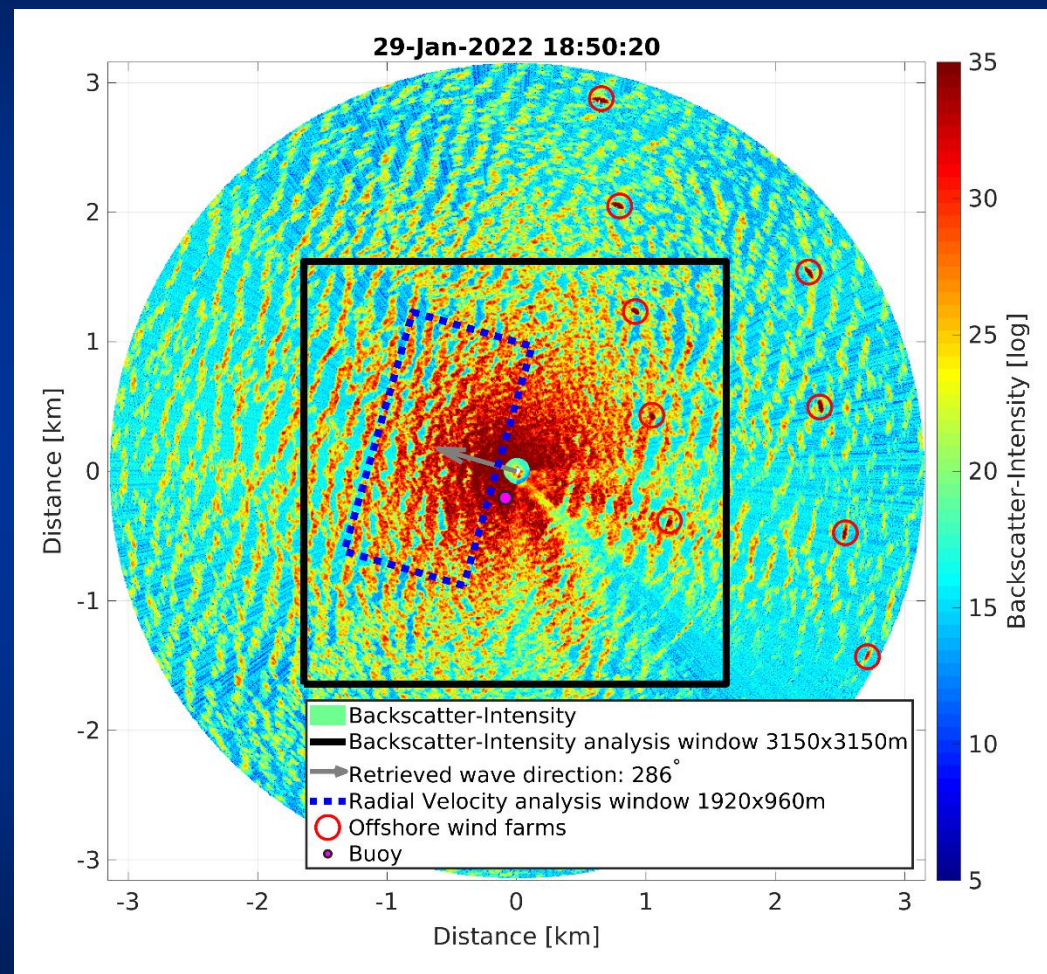


Doppler Velocity

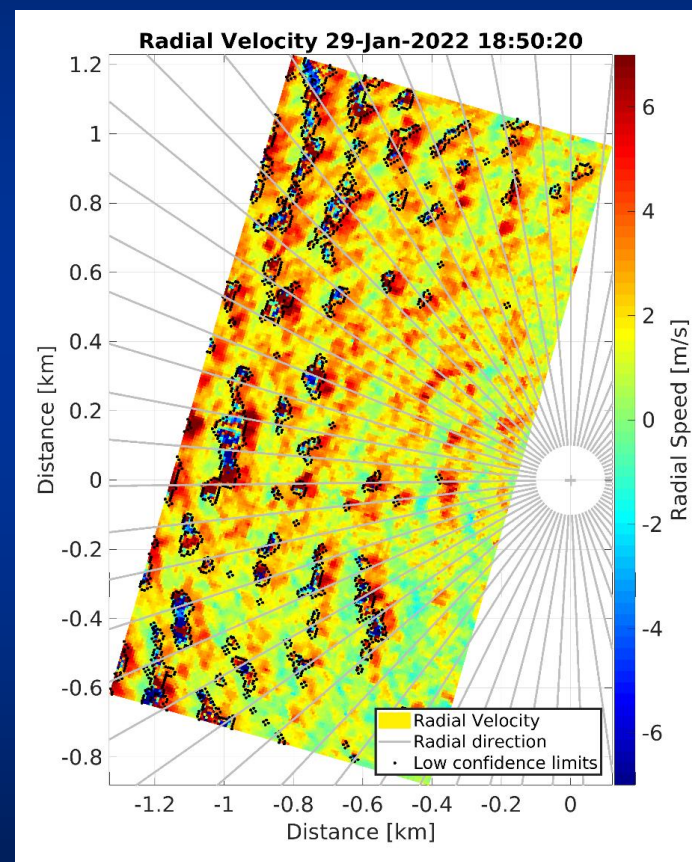


Significant Wave Height measurements by Coherent Marine Radar

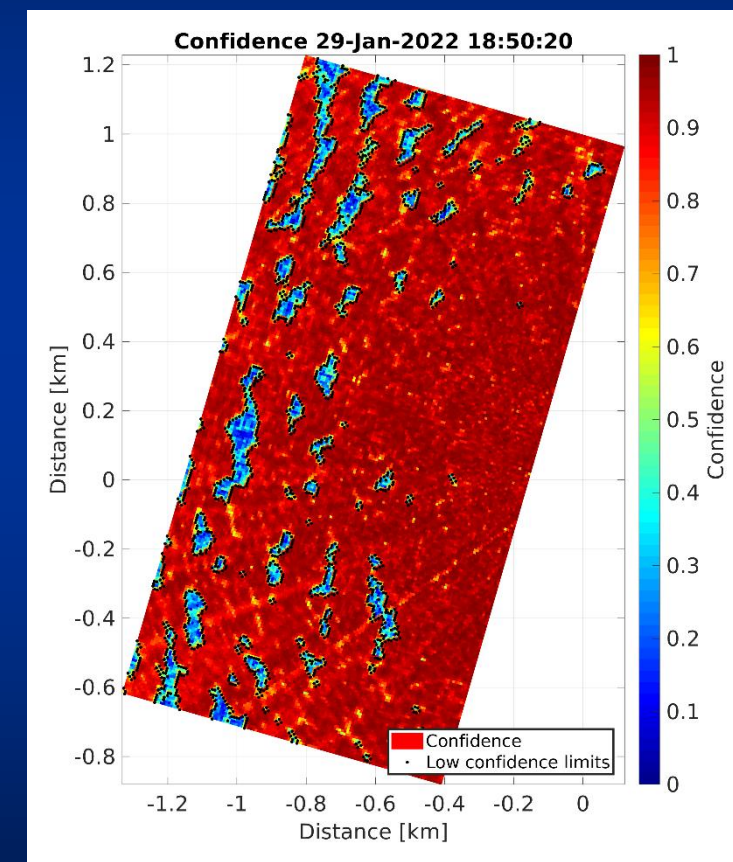
R. Carrasco, J. -C. Nieto-Borge, J. Seemann and J. Horstmann, "Significant Wave Height Retrieved From Coherent X-Band Radar: A Physics-Based Approach," in *IEEE Transactions on Geoscience and Remote Sensing*, vol. 62, pp. 1-15, 2024, Art no. 5102115, doi: 10.1109/TGRS.2024.3354042.



Backscatter-Intensity



Doppler Speed

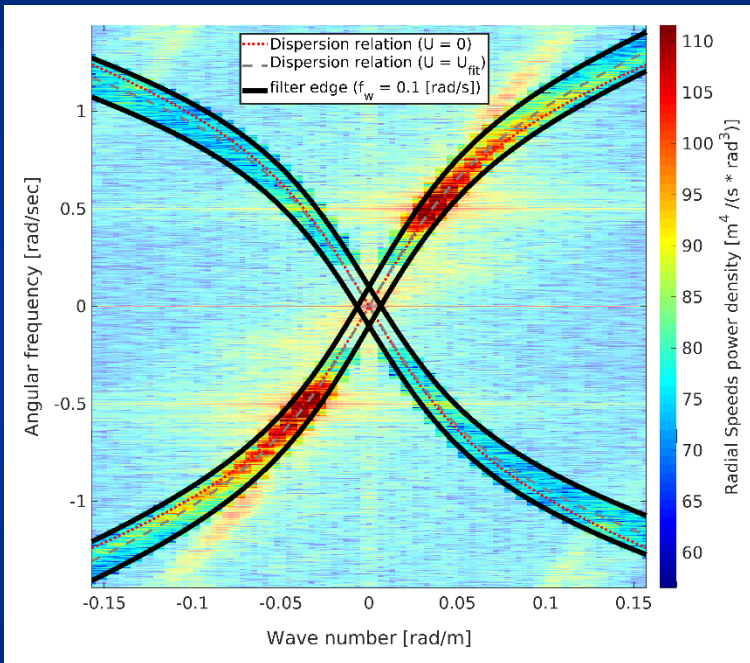


Doppler Confidence

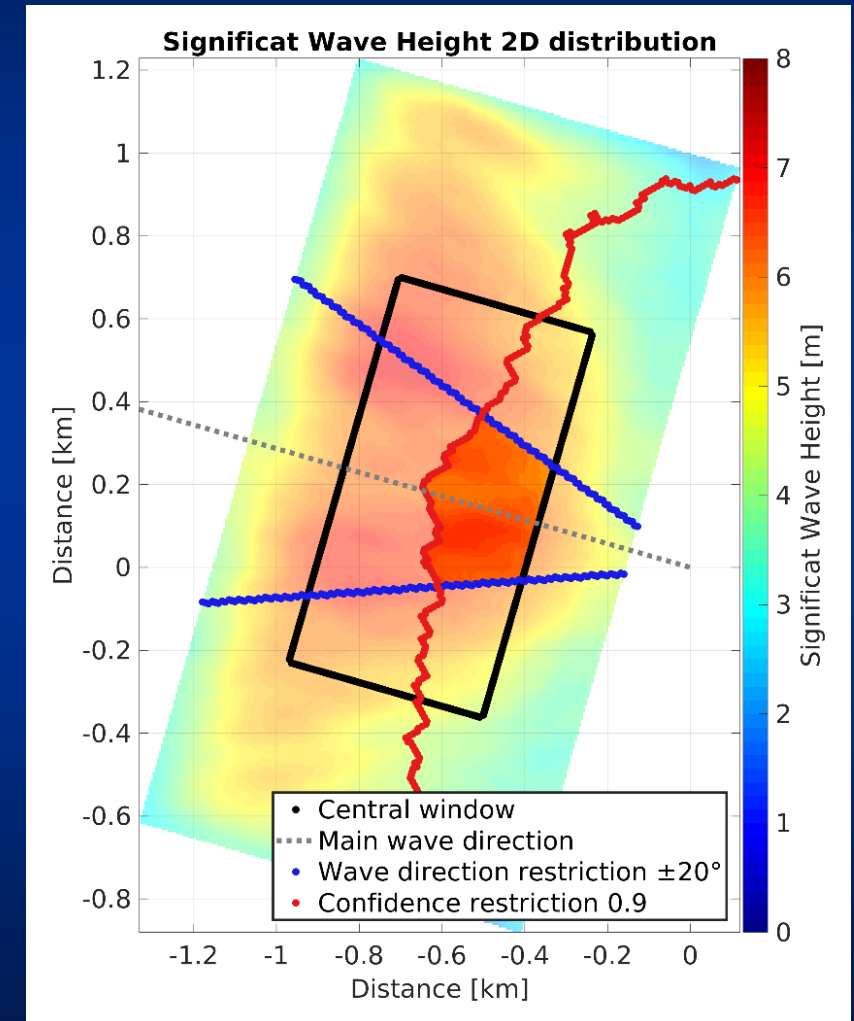
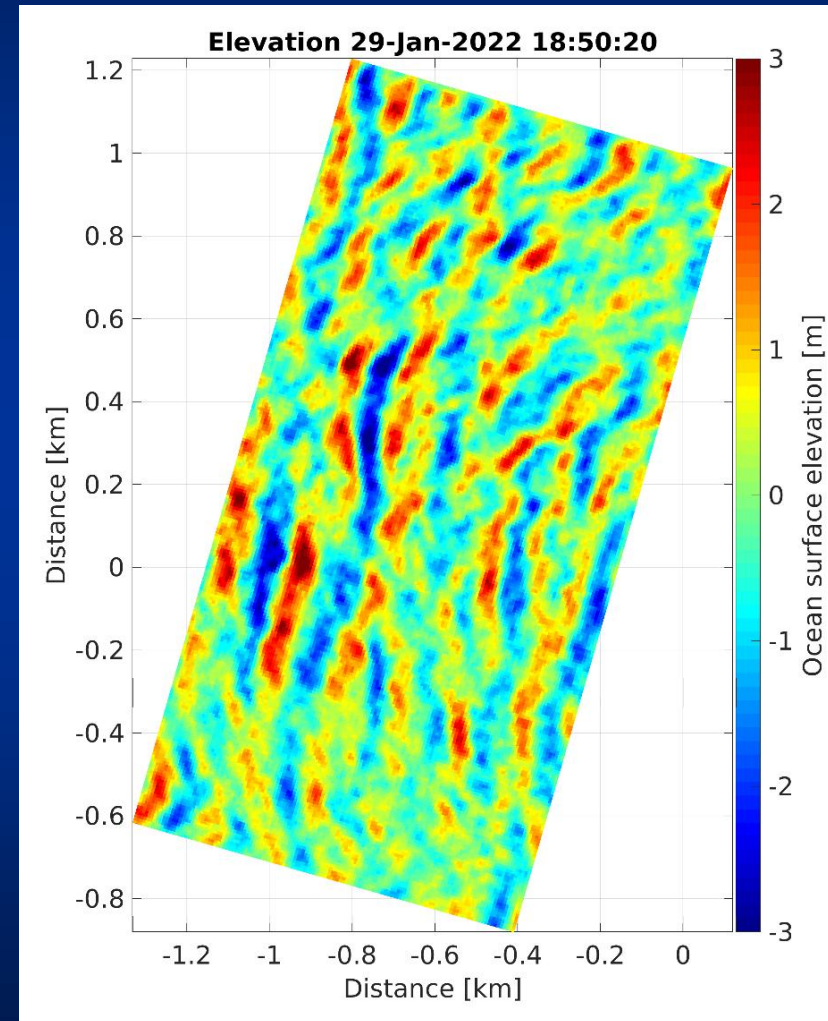
Significant Wave Height measurements by Coherent Marine Radar

Surface elevation

Hs calculation

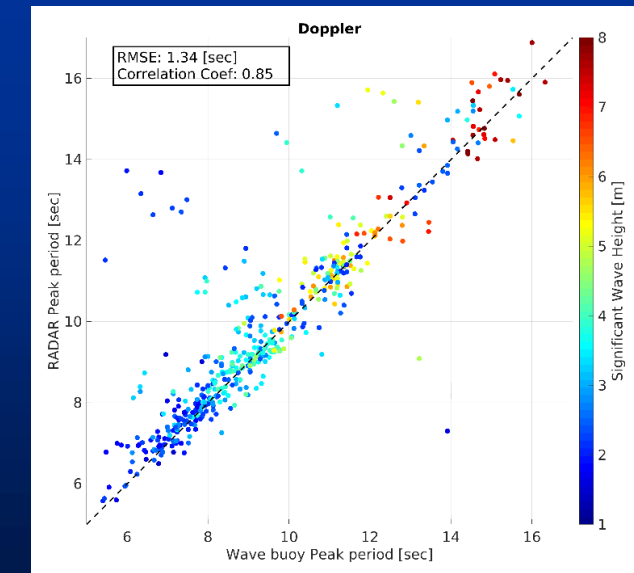
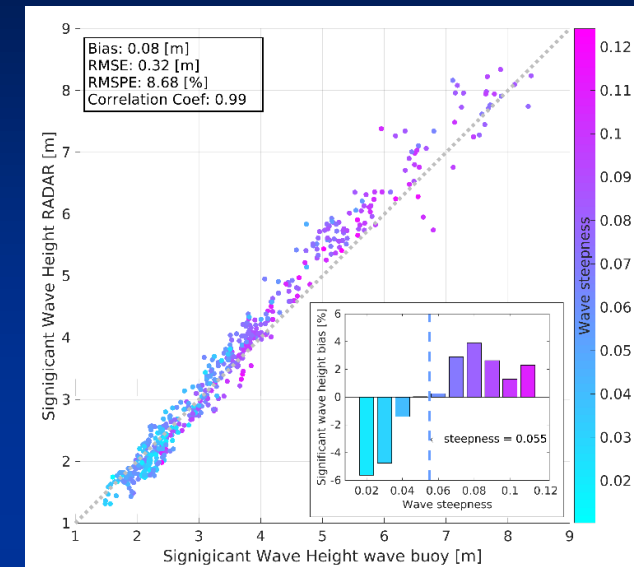
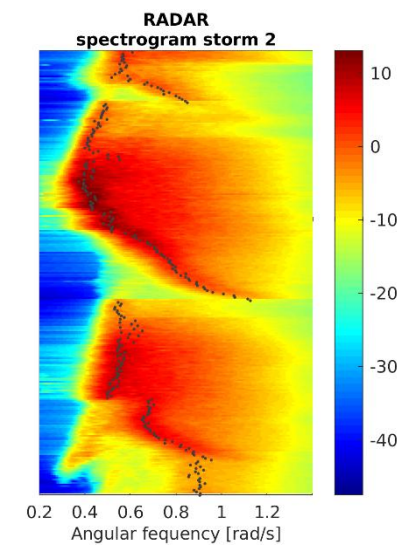
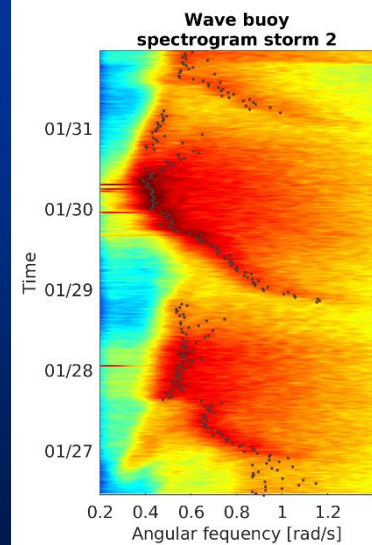
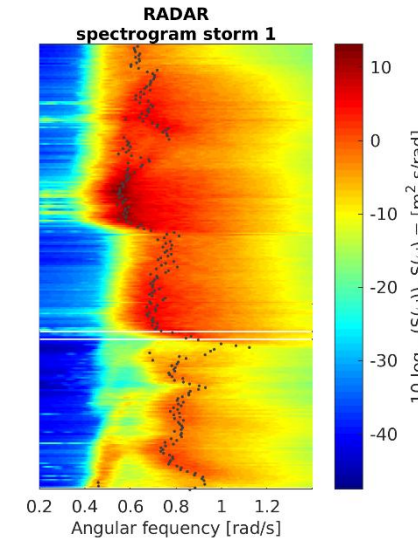
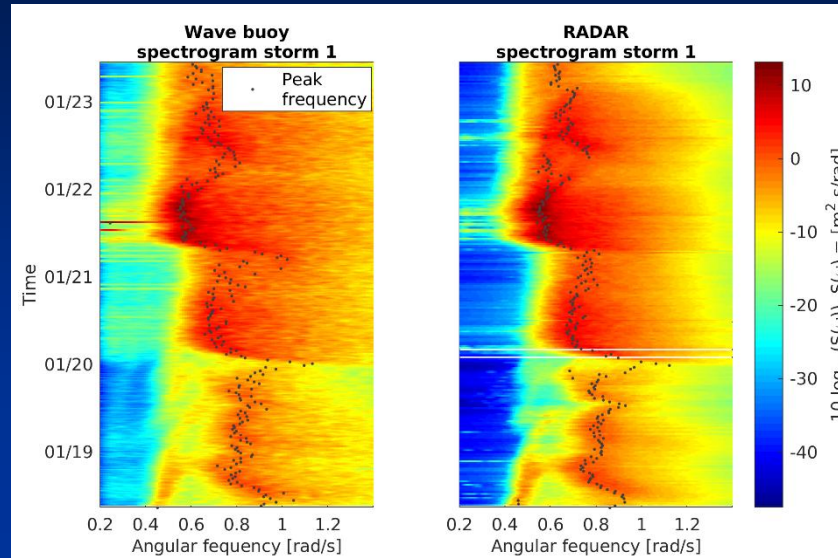
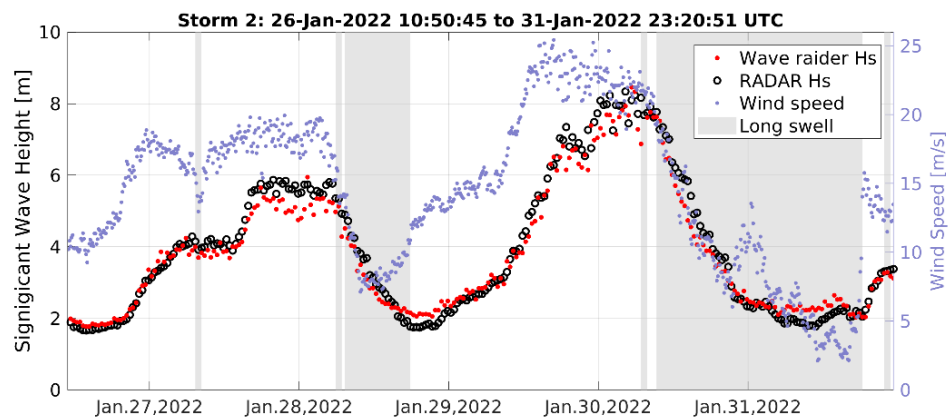
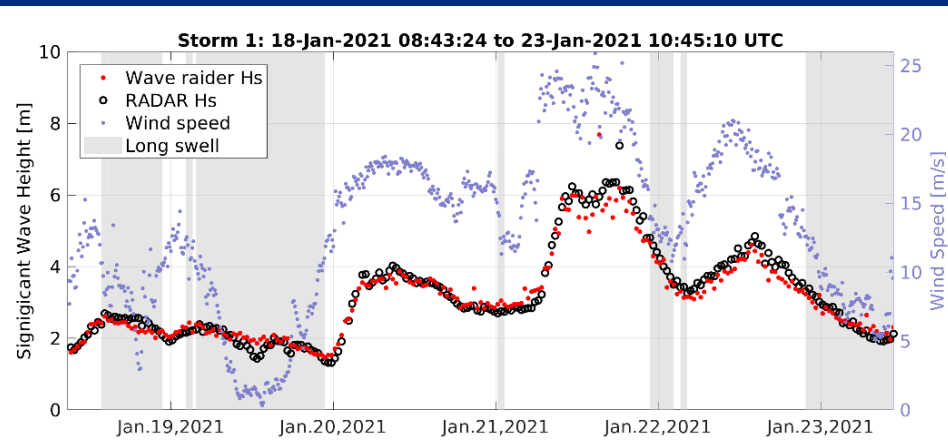


Dispersion relation
filtering +
linear wave theory

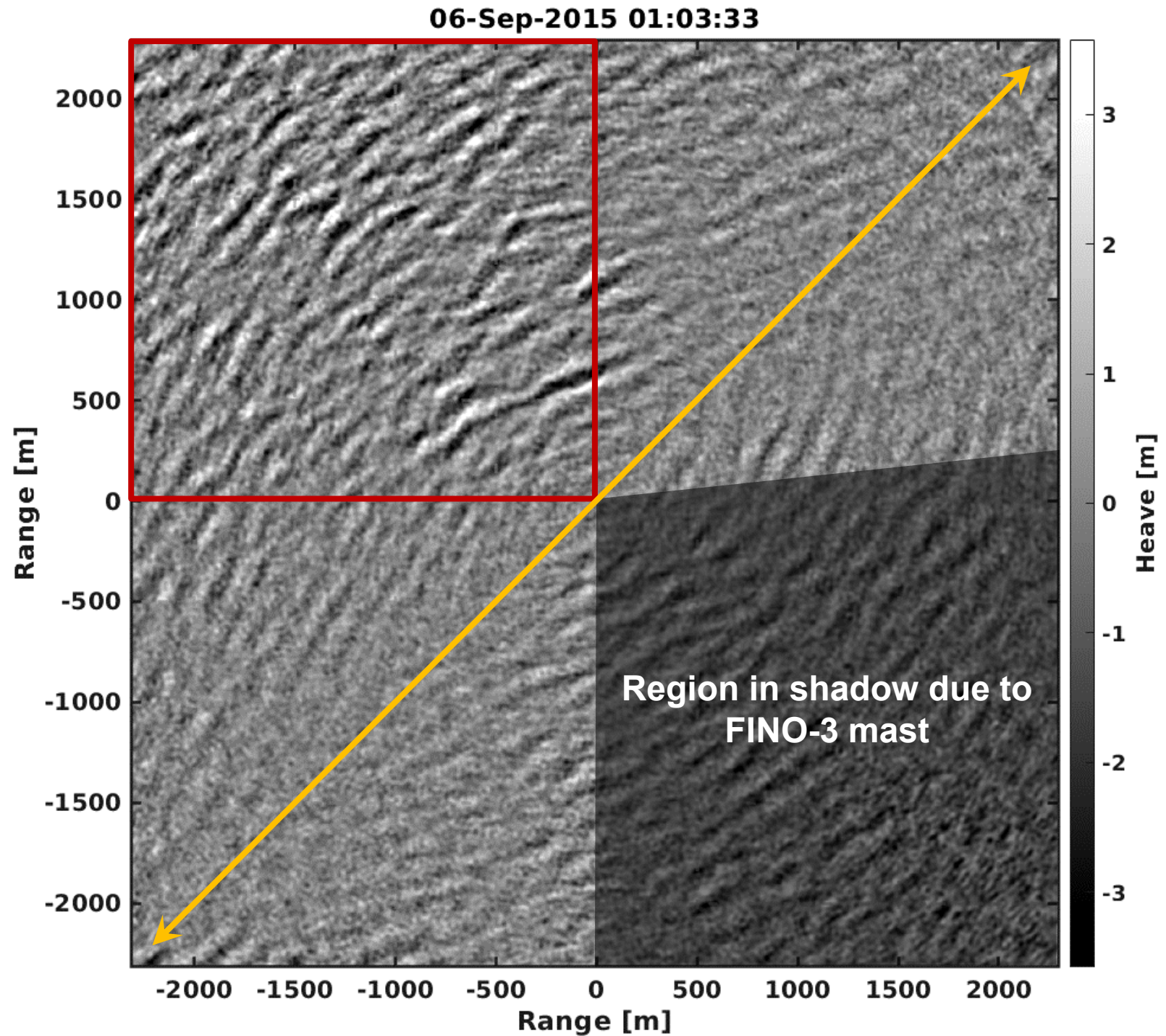
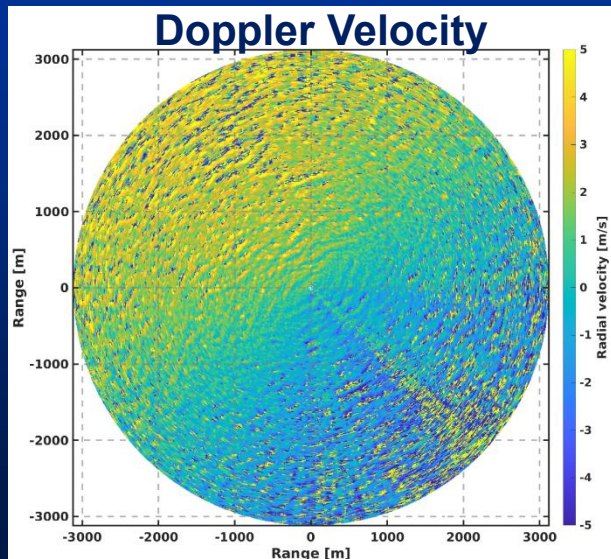


Significant Wave Height measurements by Coherent Marine Radar

Correlation Coef: 0.99
RMSE: 0.32 m RMSPE: 8.7 %

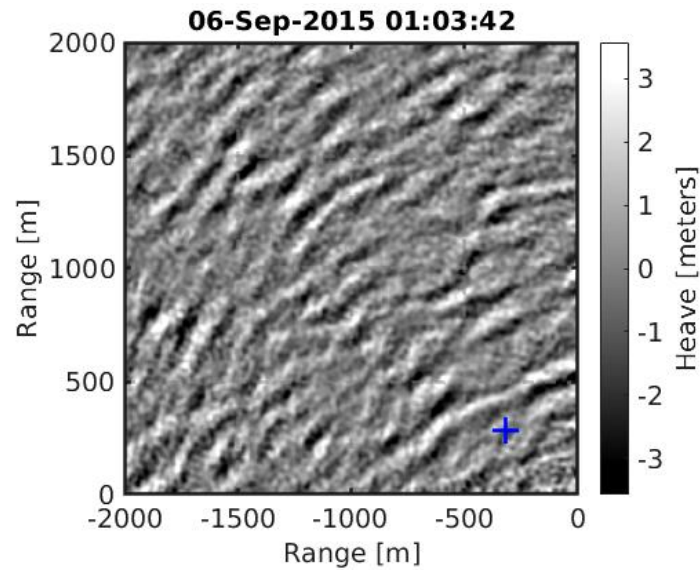


Wave fields observation in space and time

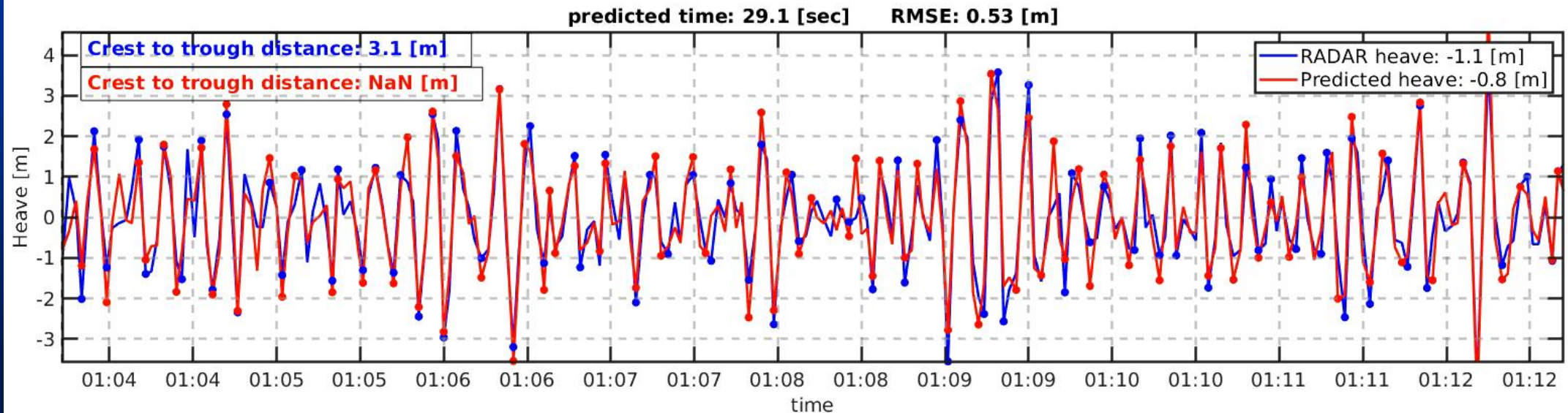
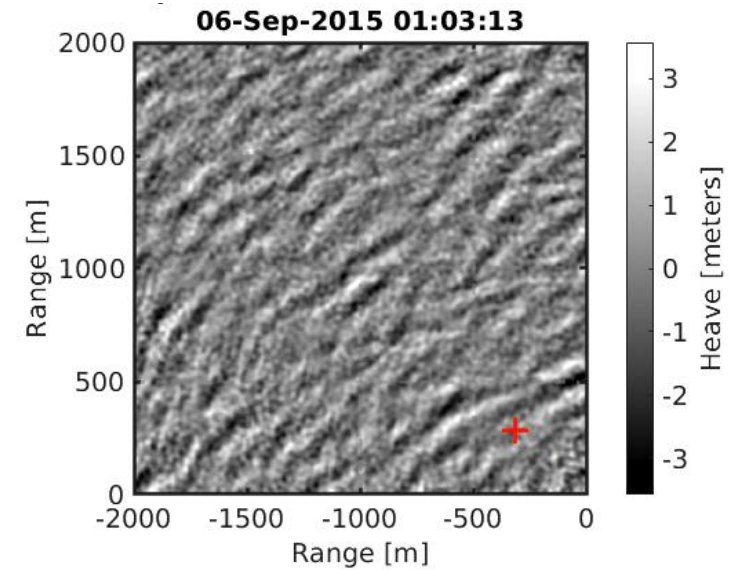


Short term prediction of wave fields over 30 s

Radar wave field

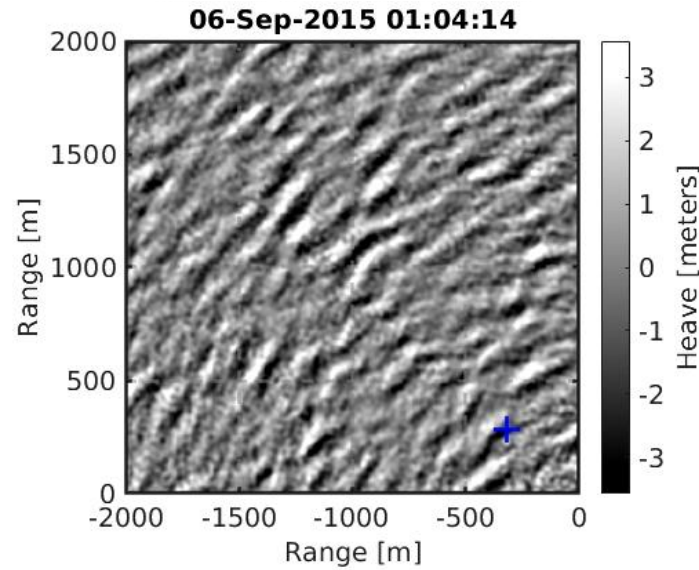


Forecast

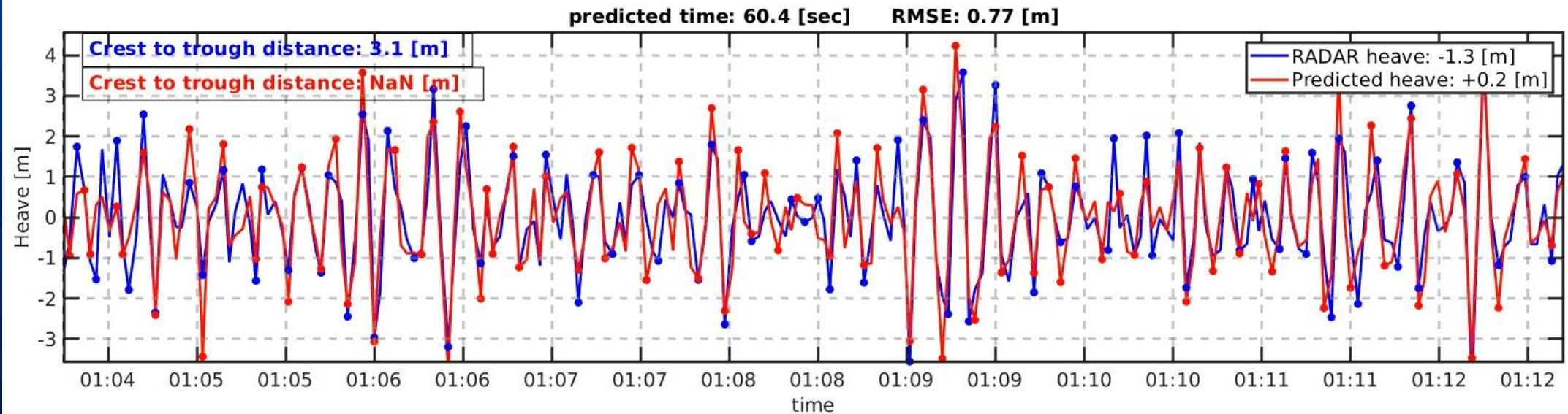
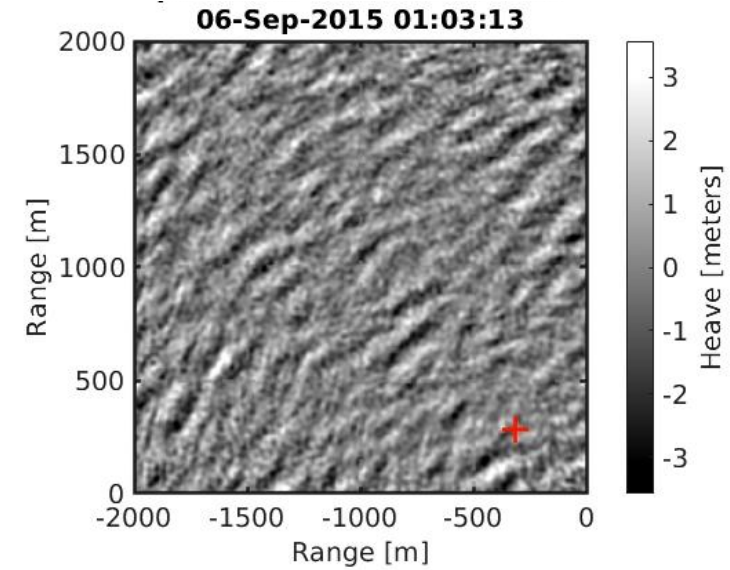


Short term prediction of wave fields over 60 s

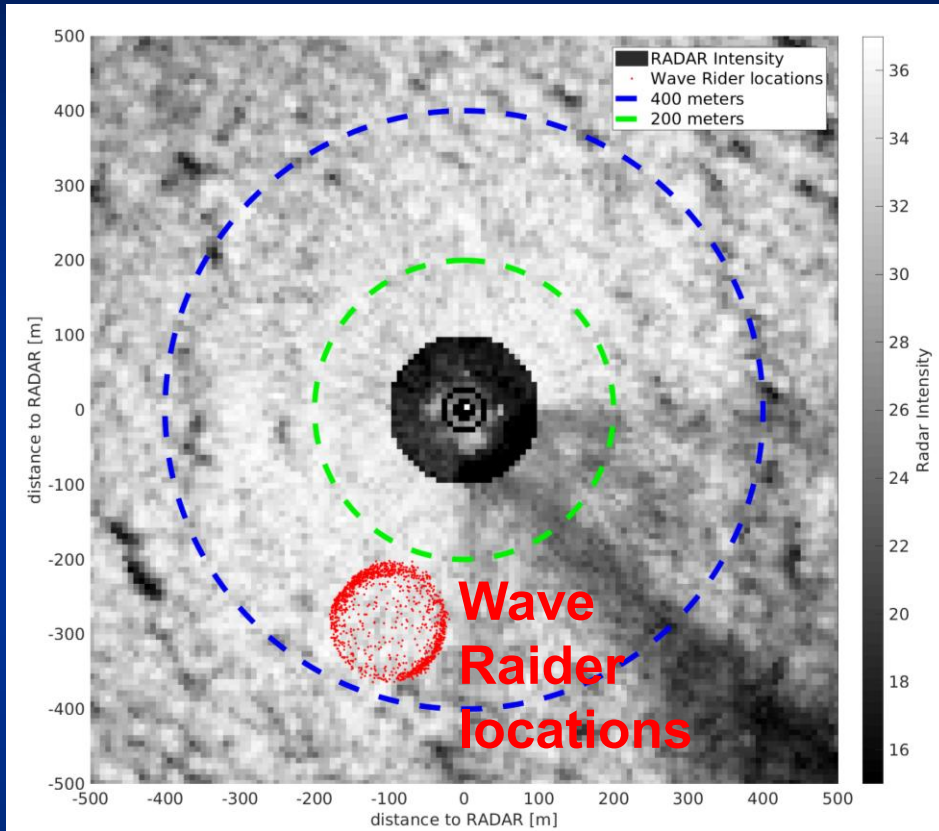
Radar wave field



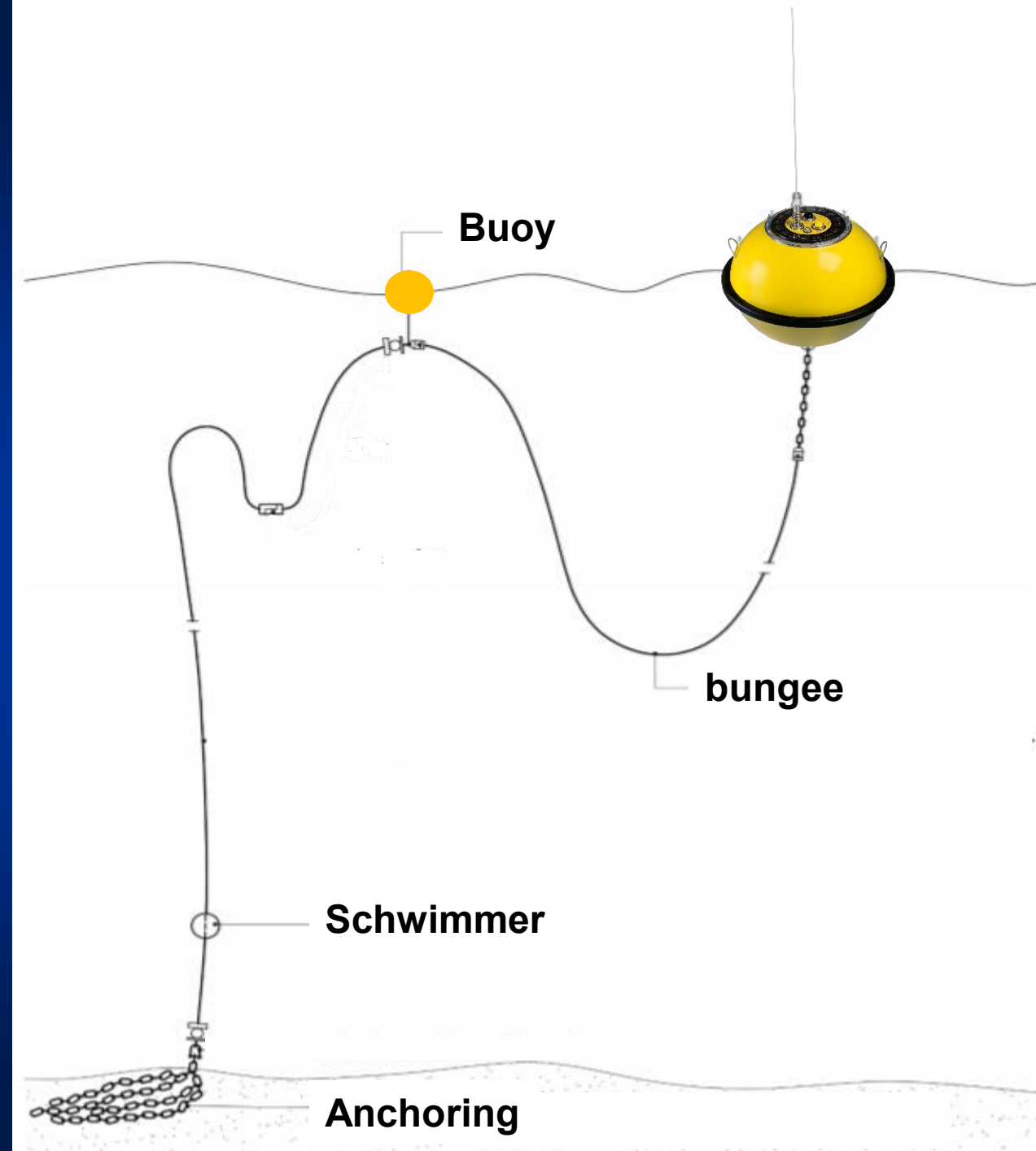
Forecast



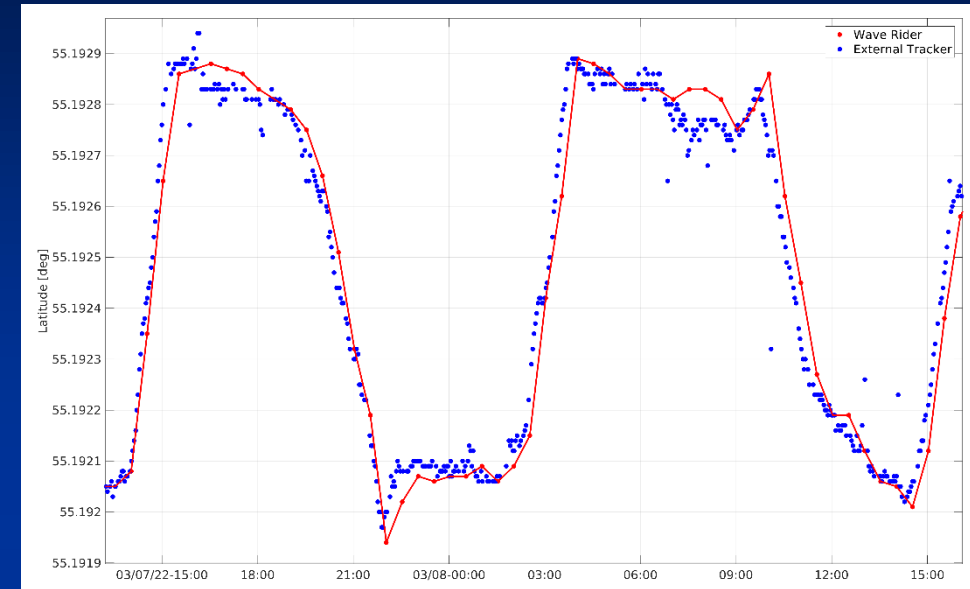
Single wave measurement validation challenges:



- Time delay
- Accurate Position
 - Tidal currents ~ 0.5 m/s
 - Waves orbital motion

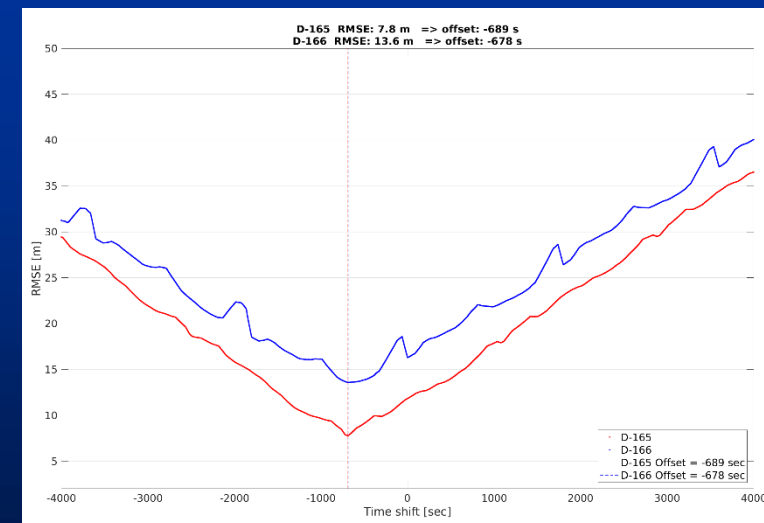


Wave Raider + external tracker

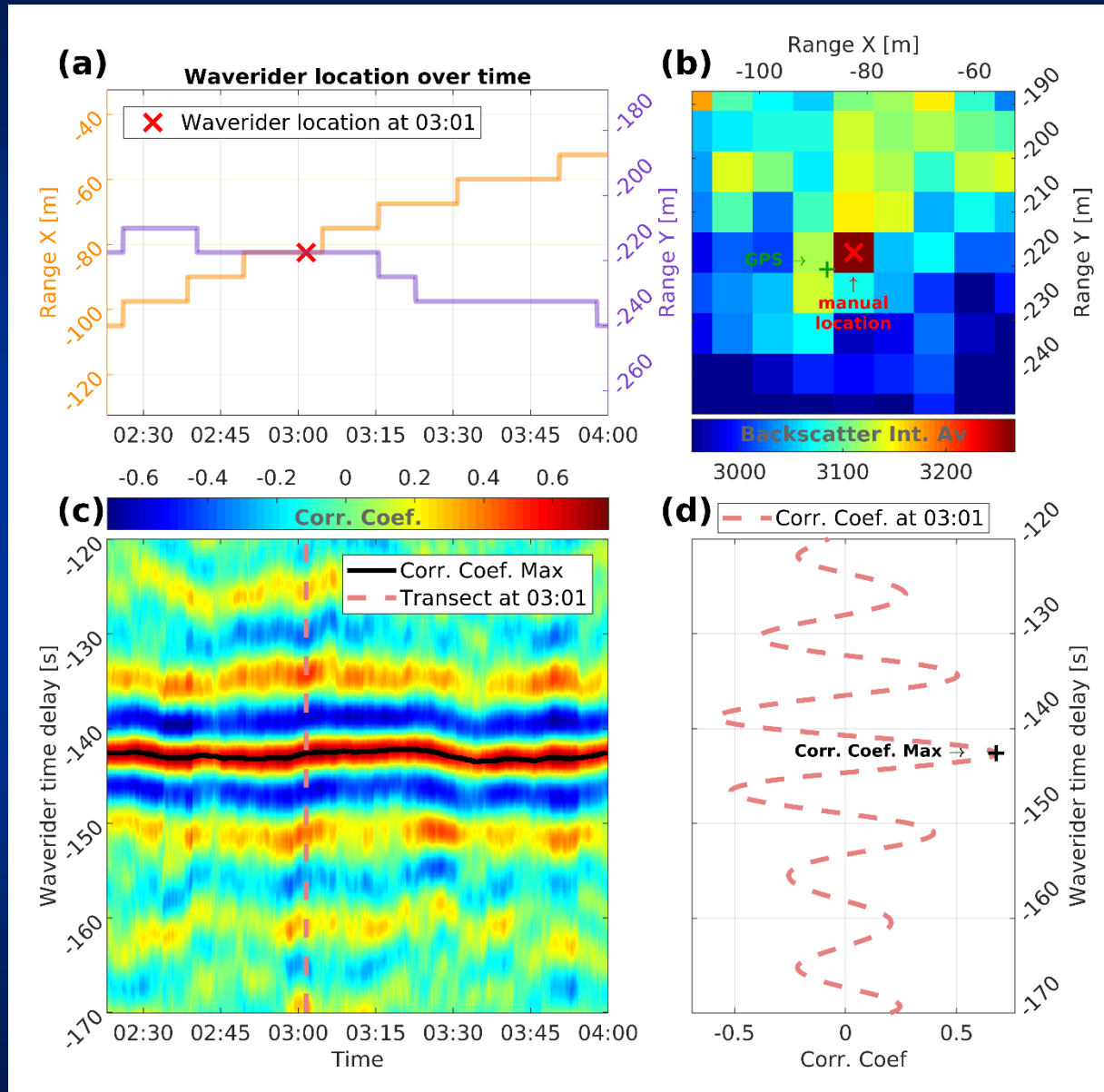


Sampling time:

- Wave Raider: 30 minutes
- External Tracker: 2.5 minutes



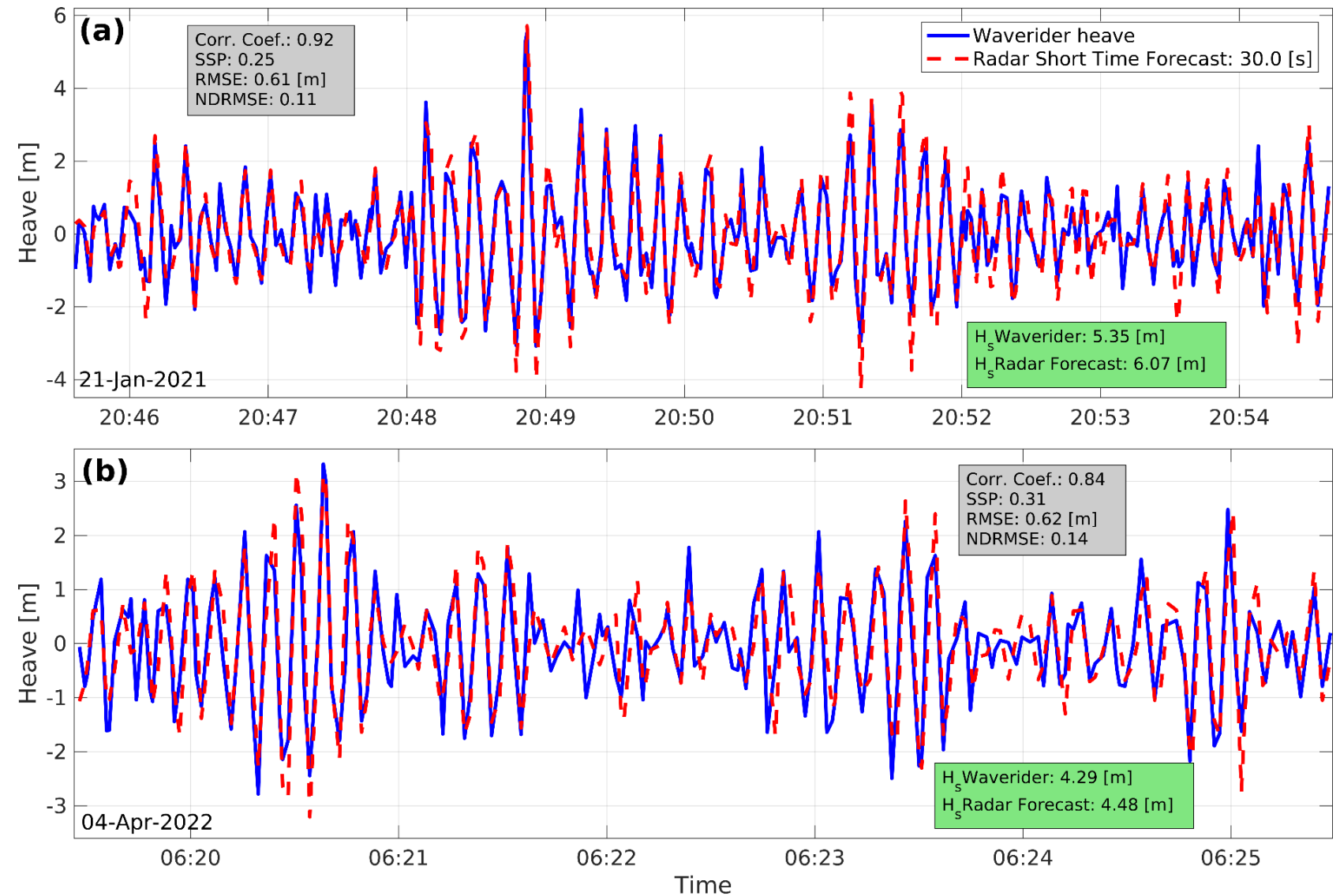
Synchronization: Wave Raider + external tracker



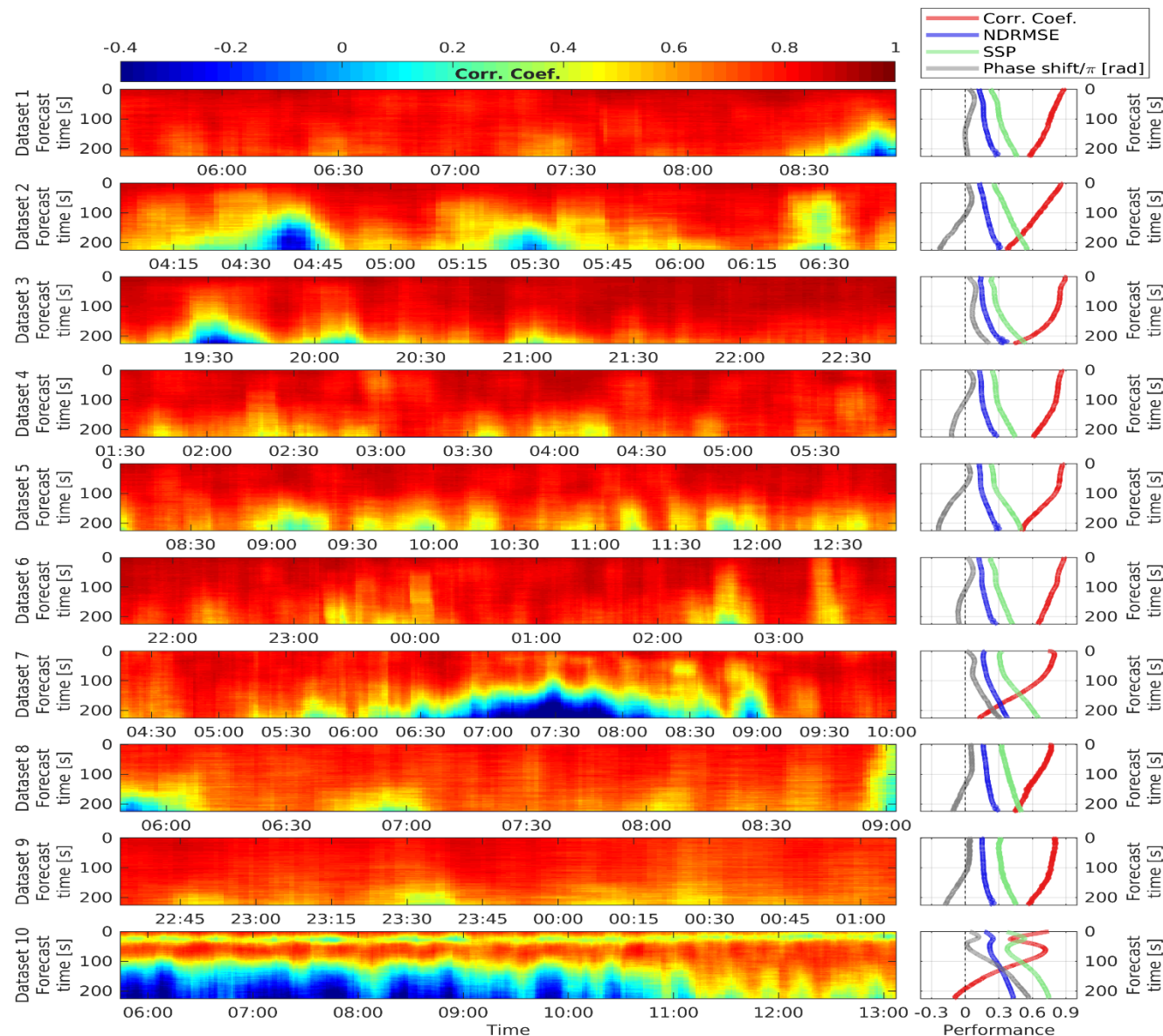
Individual waves propagation 30s

Wave field propagation by linear wave theory

$$\hat{\eta}_{pro}(k_x, k_y) = \hat{\eta}_+(k_x, k_y)e^{-i\omega(\mathbf{k})t_{pro}}$$



Feasibility study: over time domain



Red CC: forecast wave field in phase vs real wave field

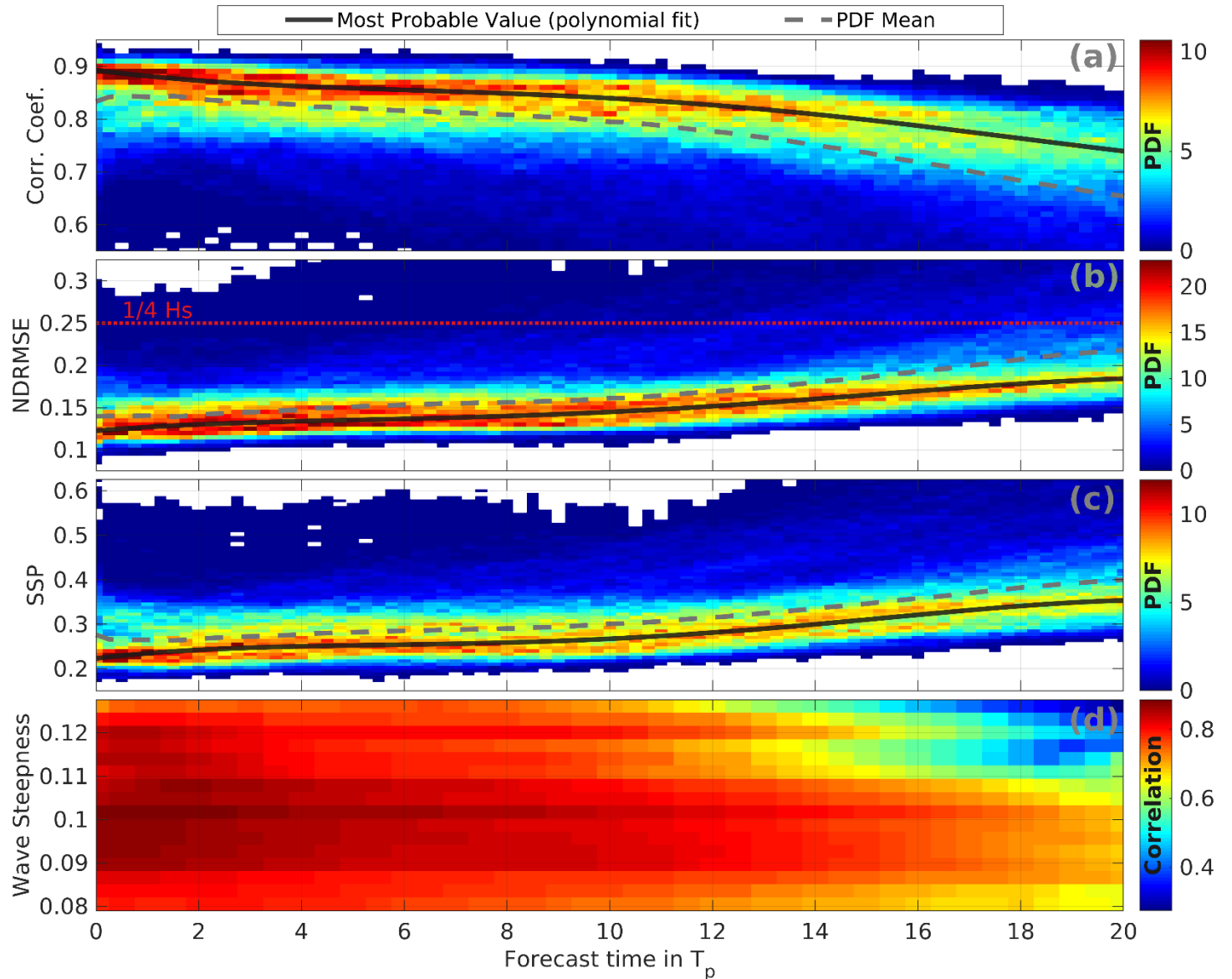
Blue CC: negative forecast wave field not in phase vs real wave field

Feasibility study: Probability Density Function

$$\text{PCC} = \frac{\text{COV}(\kappa, \eta)}{\sigma_{\kappa} \sigma_{\eta}}$$

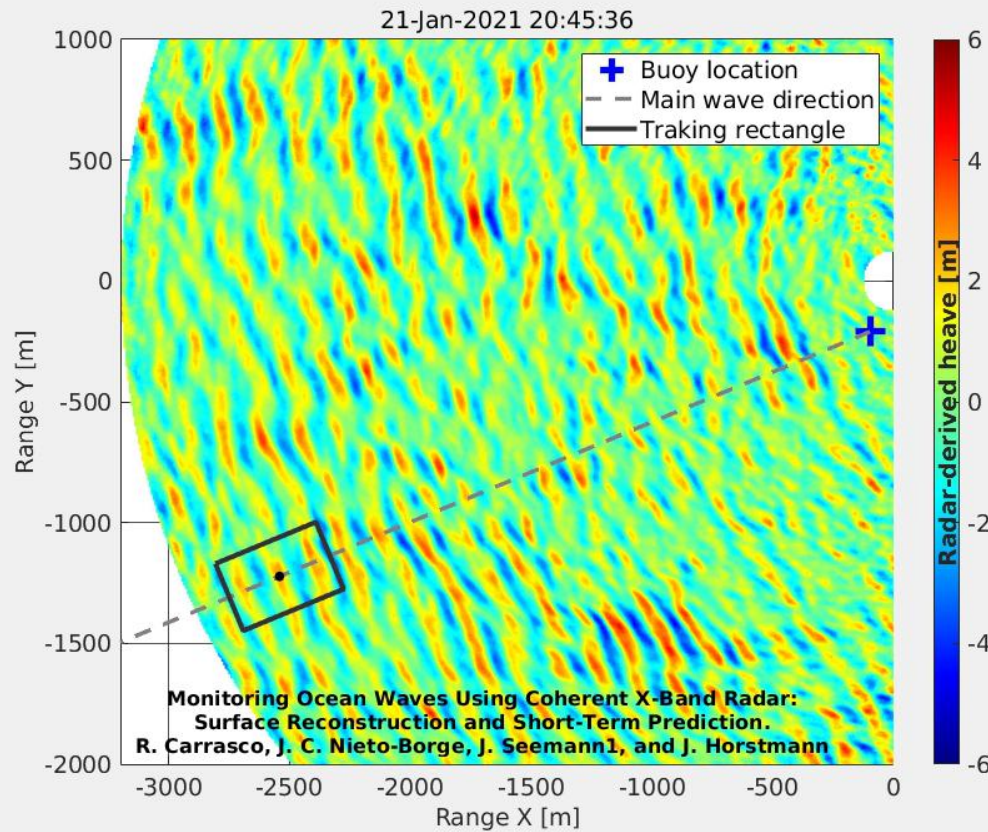
$$\text{NDRMSE} = \sqrt{\frac{1}{n} \sum_{i=1}^n \left(\frac{\kappa_i - \eta_i}{H_s} \right)^2}$$

$$\text{SSP} = \frac{\left(\int |\mathcal{F}\{\kappa(t)\}(\omega) - \mathcal{F}\{\eta(t)\}(\omega)|^2 d\omega \right)^{1/2}}{\left(\int |\mathcal{F}\{\kappa(t)\}(\omega)|^2 d\omega \right)^{1/2} + \left(\int |\mathcal{F}\{\eta(t)\}(\omega)|^2 d\omega \right)^{1/2}}$$

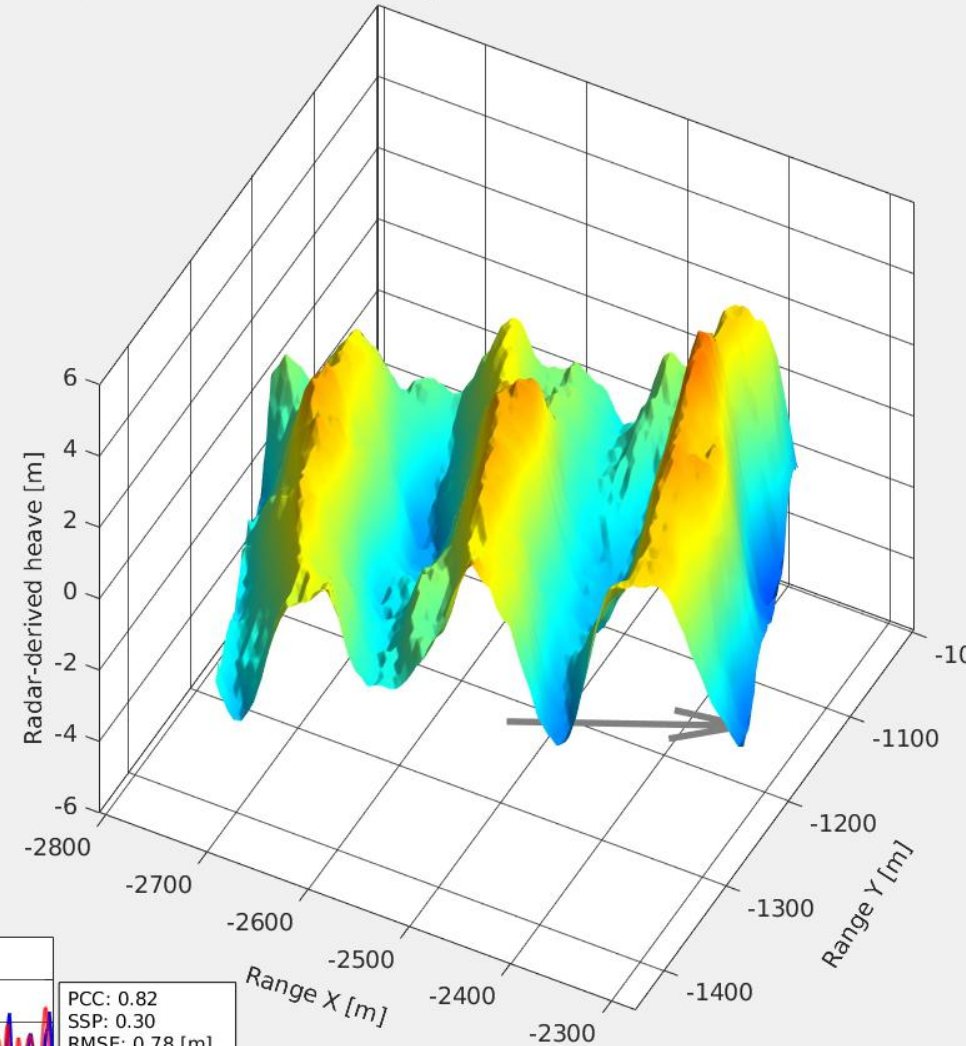


Radar-derived wave field evolution

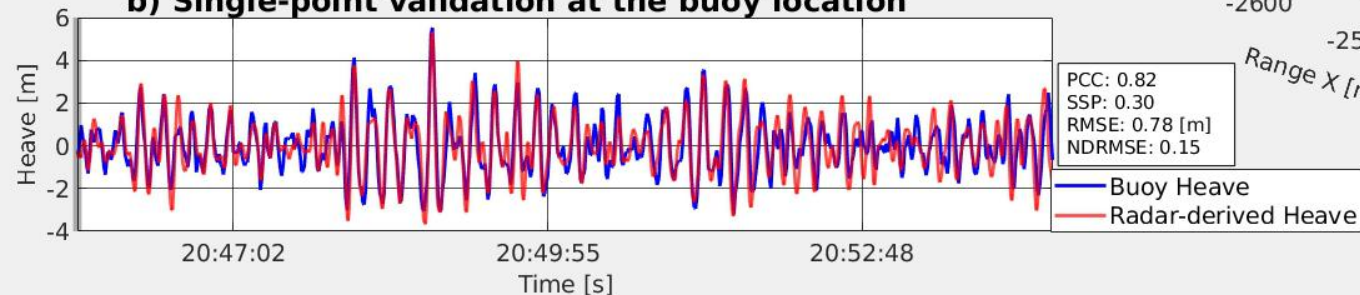
a) Radar-derived 2D surface reconstruction



c) Tracked wave along main wave direction



b) Single-point validation at the buoy location



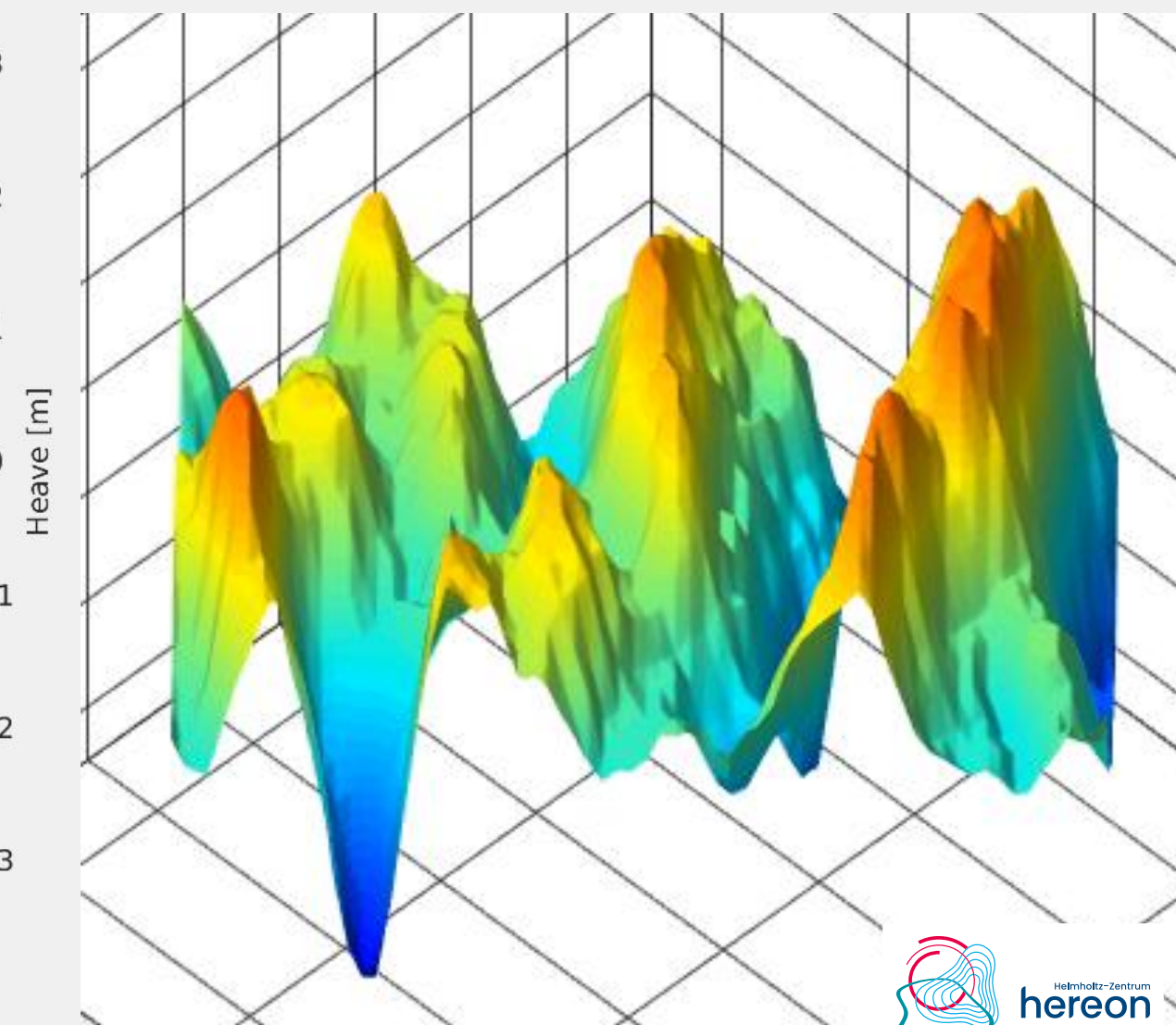
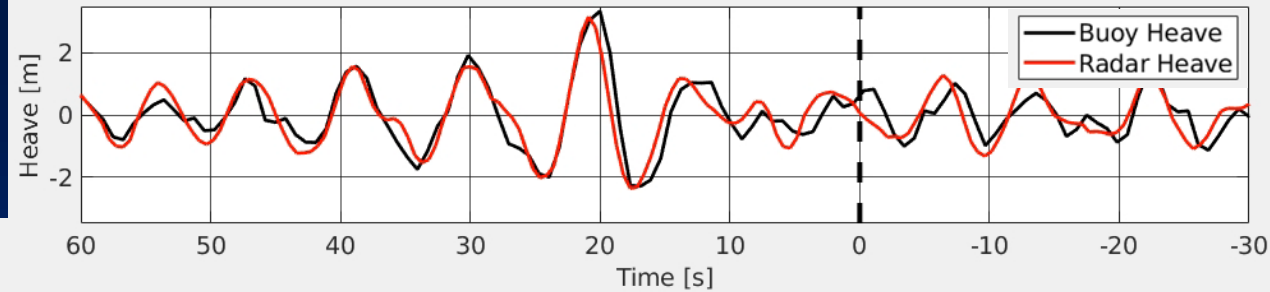
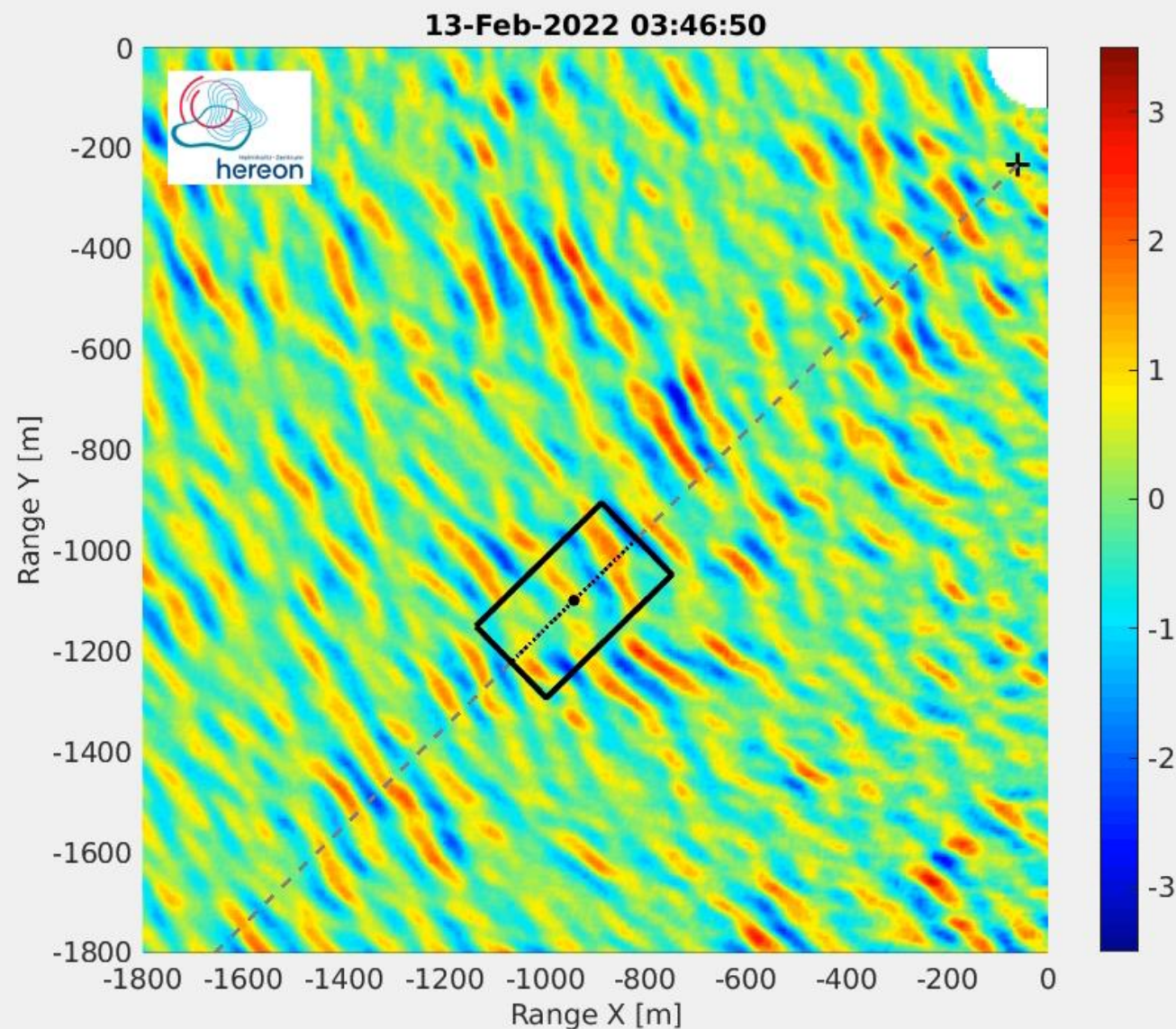
Summary

- Significant wave height accuracy 8.68 %, correlation coefficient 0.99
- Wave fields within distance of 3.2 kms
- Validation of Individual waves measurements
- Feasibility study short term prediction (Correlation over 0.8 for prediction time below 10 T_p)
- Calibration free

Outlook

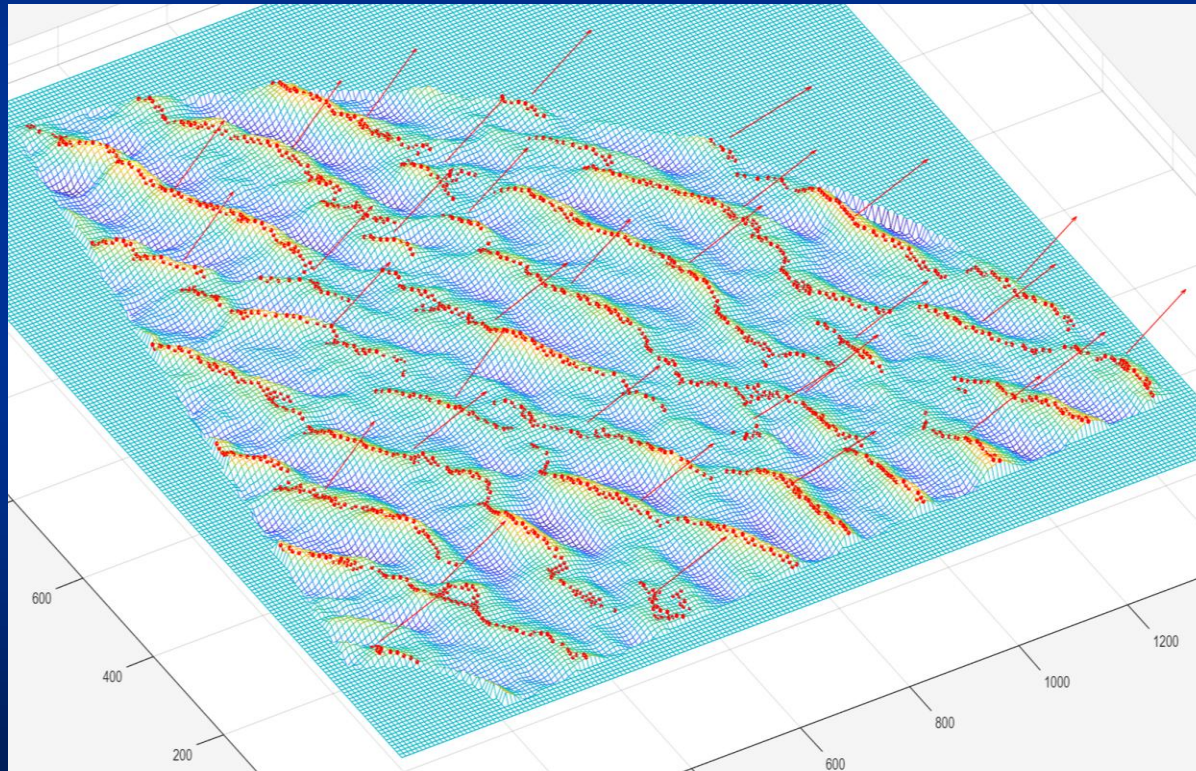
- Warning system parametrization
- Rogue wave detection in 3D

Outlook: Observation of Individual Waves in Space and Time

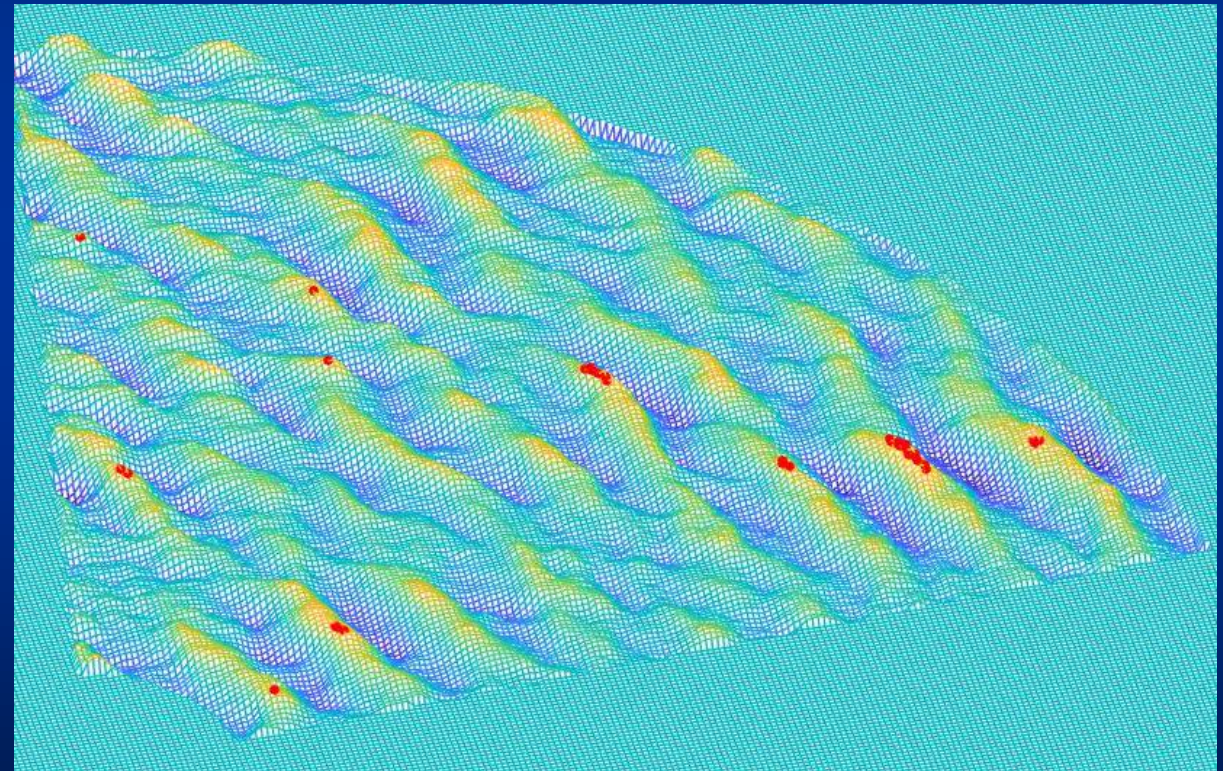


Outlook: Observation of Individual Waves in Space and Time

Wave crests and troughs



Extremes (> 5 m or steeper 0.12)



Radar-derived wave field evolution

