

### Winter ice-wave modeling with WAVEWATCH III in Lake Erie

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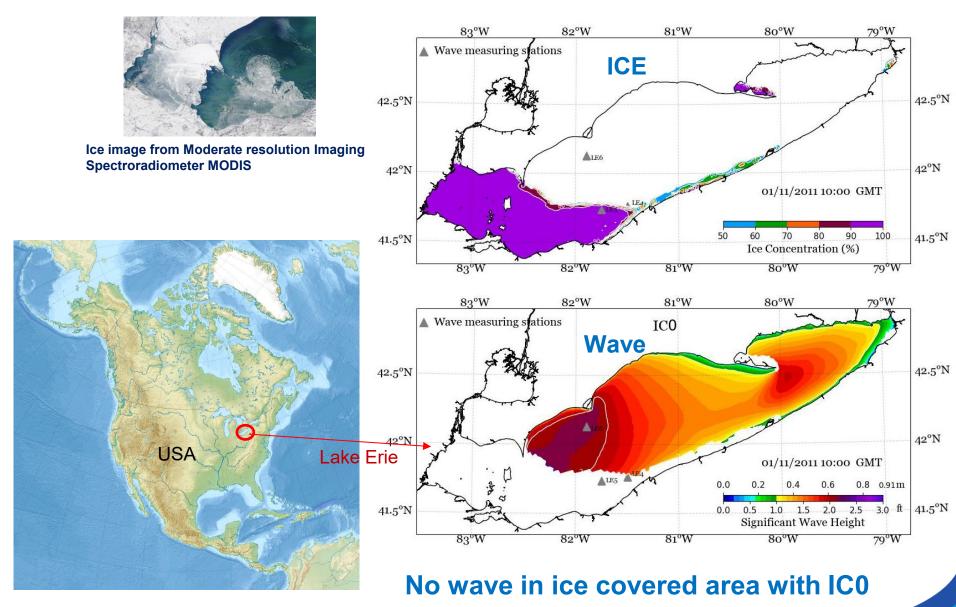
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## The problem: The current using of ice module IC0

#### IC0 take ice covered area as land



# The problem: ice modules in WaveWatch3 (WW3)

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	Description	Attenuation coefficient empirical relationship	Values of tunable parameters used	References
IC0	ICO Simple ice blocking	N/A (see references for description)	N/A	WW3DG (2019)
IC1	IC1 Simple ice damping	$\alpha = 2 C_1$	$C_1$ (damping coefficient, m <sup>-1</sup> ): $2.0 \times 10^{-5}$	Rogers and Orzech (2013), WW3DG (2019)
IC2	IC2 Viscoelastic damping with ice modeled as continuous thin elastic plate	N/A (see references for description)	$C_1$ (ice thickness, m): 0.15 $C_2$ (eddy viscosity, m <sup>2</sup> s <sup>-1</sup> ): $1.0 \times 10^{-5}$ $C_3$ (water depth, m): 20	Rogers and Orzech (2013), WW3DG (2019)
IC3	IC3 Viscoelastic damping with ice modeled as frazil ice floes	N/A (see references for description)	$C_3$ (water depth, in): 0.15 $C_1$ (ice thickness, m): 0.15 $C_2$ (effective viscosity of ice, $m^2 s^{-1}$ ): 3 $C_3$ (ice density, kg m <sup>-3</sup> ): 917 $C_4$ (effective shear modulus of ice, Pa): 0	Wang and Shen (2010), WW3DX (2019)
IC4M1	IC4M1 Empirical exponential damping as a function of wave period (T), with higher damping for smaller-period waves	$a = e^{\left(\frac{-2cC_1}{T} - C_2\right)}$	$C_1$ , $C_2$ (empirical): 0.18, 7.3	Collins and Rogers (2017), Wadhams et al. (1988), WW3DG (2019)
IC4M2	IC4M2 Empirical polynomial-fit damping as a function of wave period $(T)$ , designed to be flexible	$a = C_1 + C_2\left(\frac{T}{2a}\right) + C_3\left(\frac{T}{2a}\right)^2 + C_4\left(\frac{T}{2a}\right)^3 + C_5\left(\frac{T}{2a}\right)^4$	$C_1$ – $C_5$ (empirical): $0, 0, 2.12 \times 10^{-3}, 0,$ $4.59 \times 10^{-2}, 1.1$	Collins and Rogers (2017), Meylan et al. (2014), WW3DG (2019)
IC4M3	IC4M3 Empirical quadratic decay as a function of wave period (T) and ice thickness, with higher attenuation for thicker ice and smaller-period waves	$\begin{split} \alpha &= \exp[-3.203  +  2.058 C_1 - 0.9375 T \\ -0.4269 C_1^2  +  0.1566 C_1 T  +  0.0006 T^2] \end{split}$	$C_1$ (ice thickness, m): 0.15	Collins and Rogers (2017), Horvat and Tziperman (2015) WW3DG (2019)
IC4M4	IC4M4 Empirical damping as a step function of significant wave height (Hs), with linear damping for Hs ≤ 3 m and capped damping for Hs > 3 m	$\alpha = \begin{cases} 2 C_1 & \text{for } H_x \le 3 \text{ m} \\ 2 C_2 H_x^{-1} & \text{for } H_x > 3 \text{ m} \end{cases}$	$C_1$ , $C_2$ (empirical): 5.35 $\times$ 10 <sup>-6</sup> , 16.05 $\times$ 10 <sup>-6</sup>	Collins and Rogers (2017), Kohout et al. (2014), WW3DG (2019)
IC4M5	IC4M5 Empirical damping as a step function of wave period (T), with four user- defined steps and damping coefficients	$\alpha = \begin{cases} 2 C_1 & \text{for}  T^{-1} < C_5 \\ 2 C_2 & \text{for}  C_5 \le T^{-1} < C_6 \\ 2 C_3 & \text{for}  C_6 \le T^{-1} < C_7 \\ 2 C_4 & \text{for}  T^{-1} \ge C_7 \end{cases}$		Collins and Rogers (2017), WW3DG (2019)
IC4M6	IC4M6 Empirical damping as a step function of wave period (T), with up to ten user-defined steps and damping coefficients	$\alpha = \begin{cases} 2 C_{A1} & \text{for} & T^{-1} < C_{B1} \\ 2 C_{A2} & \text{for} & C_{B1} \le T^{-1} < C_{B2} \\ & \dots \\ & \\ 2 C_{A9} & \text{for} & C_{B8} \le T^{-1} < C_{E9} \\ & \\ 2 C_{A10} & \text{for} & C_{E9} \le T^{-1} < C_{E10} \end{cases}$	$\begin{split} &C_{\rm AI}C_{\rm A10} \ (\text{damping coefficients,} \\ &\text{m}^{-1})\text{:} \\ &5.0 \times 10^{-6}, 7.0 \times 10^{-6}, 1.5 \times 10^{-5}, \\ &1.0 \times 10^{-4}, 0, 0, 0, 0, 0, 0 \\ &C_{\rm BI}C_{\rm B10} \ (\text{step bounds, Hz})\text{:} \\ &0.10, 0.12, 0.16, 99.0, 0, 0, 0, 0, \\ &0, 0 \end{split}$	Collins and Rogers (2017), WW3DG (2019)
IC4M7	IC4M7 Empirical damping as a function of wave period $(T)$ and ice thickness	$\alpha=0.2T^{-213}C_1$	$C_1$ (ice thickness, m): 0.15	Doble et al. (2015), WW3DG (2019)
IC5	IC5 Viscoelastic damping with ice modeled as thin elastic plate restricted to one dimension	N/A (see references for description)	$C_1$ (ice thickness, m): 0.15 $C_2$ (effective viscosity, m <sup>2</sup> s <sup>-1</sup> ): $1.6 \times 10^7$ $C_3$ (ice density, kg m <sup>-3</sup> ): 917 $C_4$ (effective shear modulus, Pa): $4 \times 10^{12}$	Mosig et al. (2015), WW3DX (2019)

#### Which one should we use?

They are mostly based on the Arctic and Antarctic researches

We have tested all 12 modules

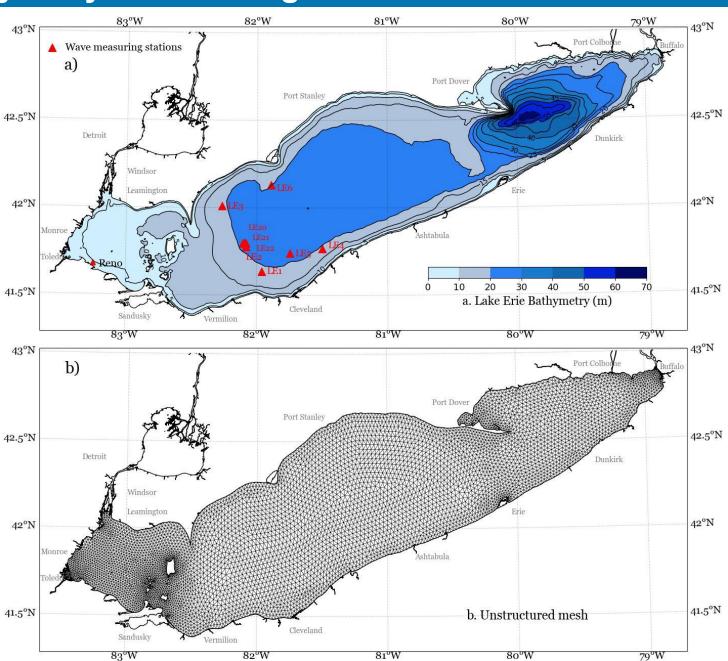
IC0 take ice as land

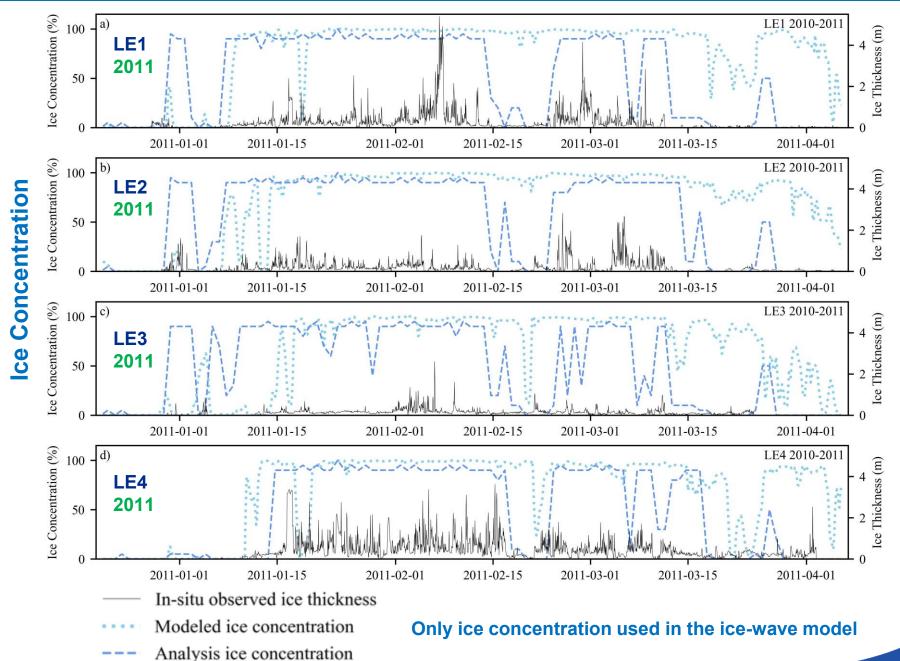
IC1 and IC4M4 are similar with constant parameters IC4M4 with wave height considered

All other ice modules are related to wave frequency

#### We have tested them all

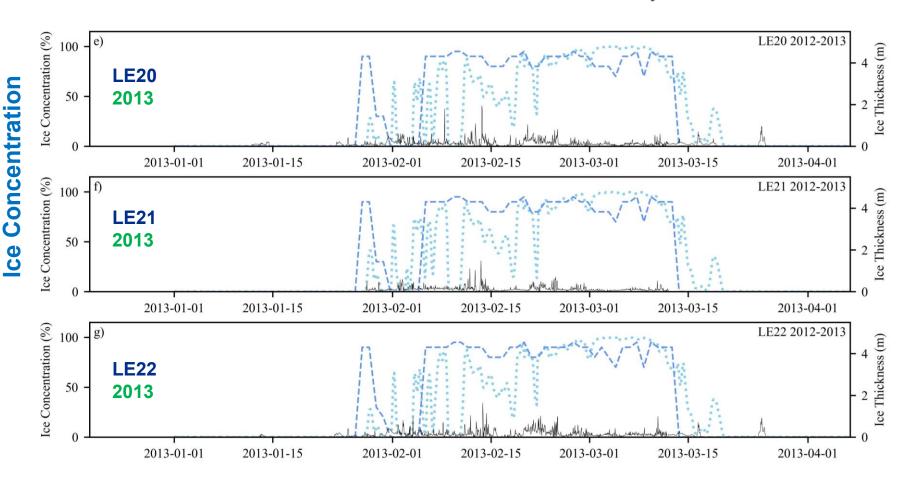
## Bathymetry and model grid







- Modeled ice concentration
- Analysis ice concentration



## Wave height from 12 ice modules (modeled vs observed, at LE4, 2011)

#### IC4M4 performs the best

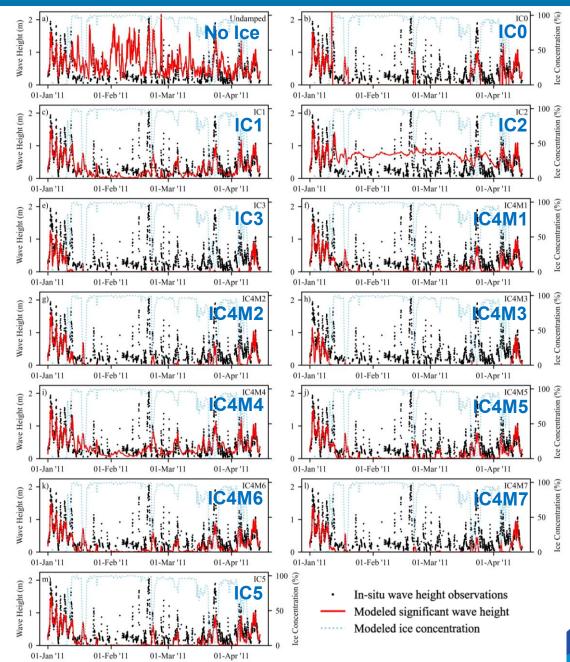
Table 4
Skill Statistics for Ice-Wave Damping Cases, Calculated by Comparing Modeled Significant Wave Height to In-Situ Observed Significant Wave Height From 1 January to 15 April 2011

	LE4 $(n = 1,482)$		LE5 $(n = 1,080)$		LE6 (n = 637)	
	RMSE	Bias	RMSE	Bias	RMSE	Bias
Undamped	0.37	+0.15	0.30	+0.06	0.27	+0.11
IC0	0.46	-0.23	0.59	-0.34	0.54	-0.23
IC1	0.34	-0.13	0.43	-0.19	0.43	<u>-0.1</u> 2
IC2	0.41	0.19	0.44	+0.18	0.34	+0.12
IC3	0.54	-0.38	0.68	-0.52	0.59	-0.40
IC4M1	0.42	-0.26	0.56	-0.37	0.51	-0.23
IC4M2	0.47	-0.31	0.63	-0.45	0.55	-0.28
IC4M3	0.55	-0.39	0.69	-0.52	0.61	-0.43
IC4M4	0.32	-0.06	0.38	-0.11	0.39	-0.08
IC4M5	0.41	-0.24	0.55	-0.34	0.50	-0.21
IC4M6	0.39	-0.22	0.52	-0.32	0.49	-0.21
IC4M7	0.49	-0.34	0.66	-0.48	0.56	-0.32
IC5	0.40	-0.23	0.53	-0.32	0.50	-0.21

IC4M4 Empirical damping as a step function of significant wave height (Hs), with linear damping for Hs ≤ 3 m and capped damping for Hs > 3 m

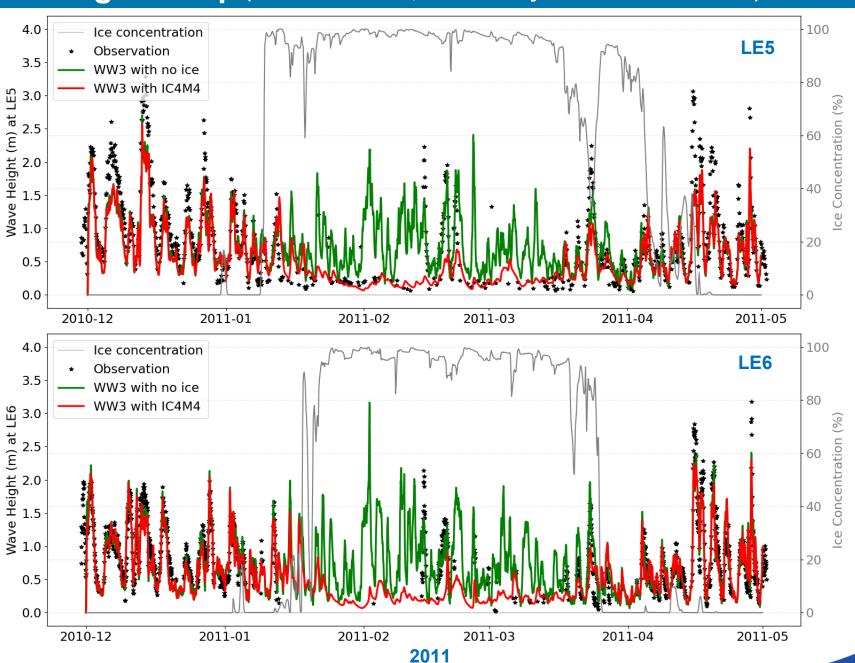
$$\alpha = \begin{cases} 2 C_1 & \text{for } H_s \le 3 \text{ m} \\ 2 C_2 H_s^{-1} & \text{for } H_s > 3 \text{ m} \end{cases}$$

IC1 Simple ice damping  $\alpha = 2 C_1$ 

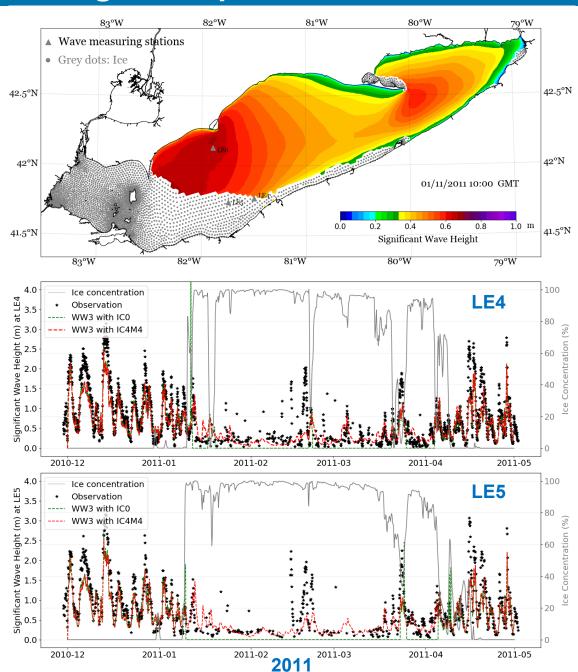


# Wave height comp (no ice vs IC4M4, and overlayed with observations)

**Wave Height** 



### Wave height comp zoom in (IC0 vs IC4M4, and overlayed with observations)



**Wave Height** 

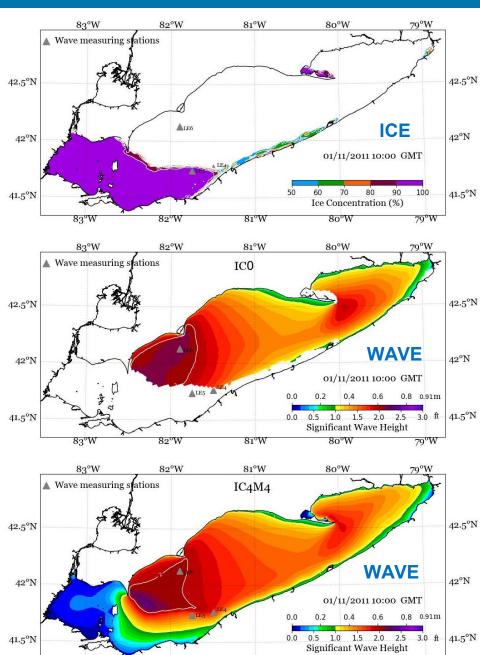
Wave prediction rely on the accuracy of ice forecast

Ice Concentration

## An example of ice event (ICO vs IC4M4)



Ice image from Moderate resolution Imaging Spectroradiometer MODIS On Jan 11, 2011



81°W

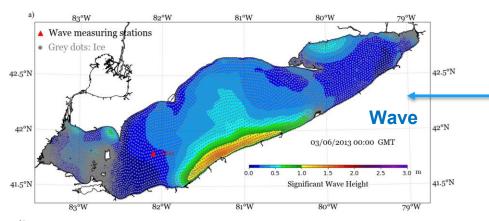
80°W

79°W

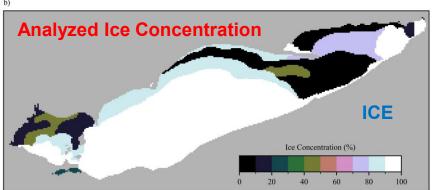
82°W

Right panels: model results

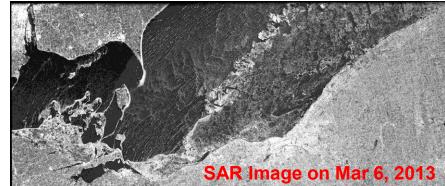
## **Another example of ice event with IC4M4**



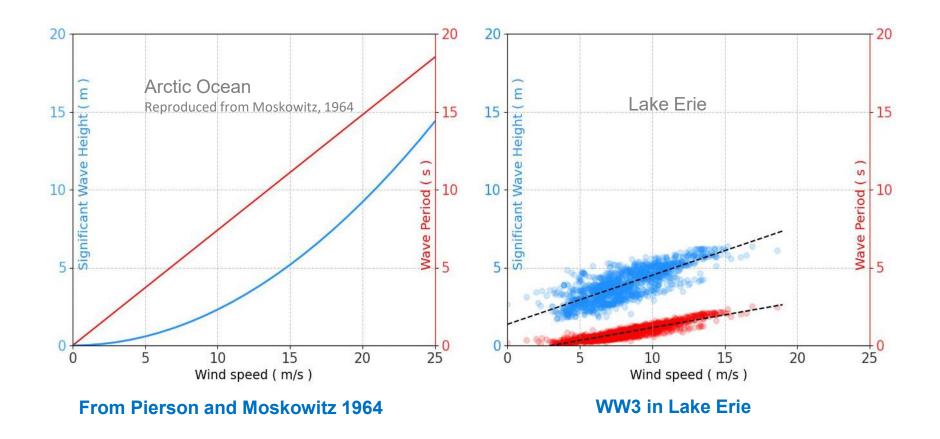
Modeled wave height overlayed with ice (dots) On Mar 06, 2013



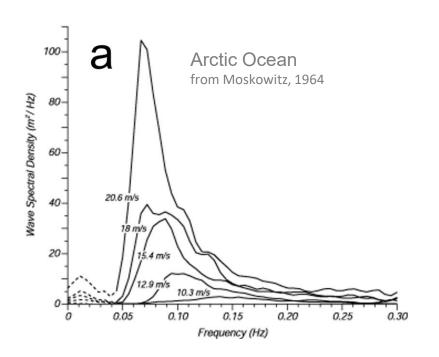


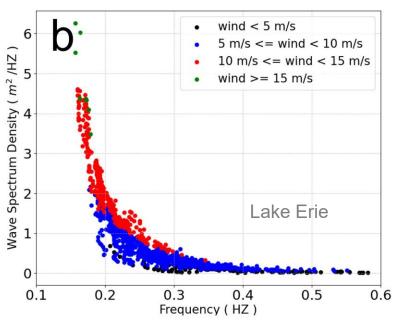


## Wave height, period vs wind speed in Arctic Ocean and Lake Erie



## Wave spectra vs wind speed in Arctic and Lake Erie





From Moskowitz 1964

WW3 in Lake Erie

Wave energy dominants in 0.05~0,1 HZ in Arctic Ocean vs in 0.1~0.2 HZ in Lake Erie

### Conclusion

- The ice module IC4M4 in the WAVEWATCH III (WW3, version 6.07.1) demonstrated the best performance among those tested, and consistently outperforms the IC0 simple blocking scheme currently used in the NOAA's operational Great Lakes Wave modeling system (GLWUv2.0) for both hindcast and forecast configurations.
- The ice modules in WW3 are mostly based on observations and studies from the Arctic Ocean and the Antarctic Ocean. Formulae based on frequency are not suitable for the Lake Erie where they cause too much damping. With the ice module IC4M4, although the module is also based on the Antarctic Ocean study, the wave attenuation is based on incoming wave height that also fits the shallow lakes.

## **Model implementation**

Website: <a href="https://www.glerl.noaa.gov/emf/waves/WW3/">https://www.glerl.noaa.gov/emf/waves/WW3/</a>

