

Implementation of the new French operational coastal wave forecasting system and application to a wavecurrent interaction study

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The need of a coastal wave model ...









The French operational model in 2014





The need of a coastal wave model ...









The French operational model in 2014



Homonim project : implementation of WW3 unstructured grids along the French coastline with a resolution of 200 m









1. The French operational coastal wave forecasting system

- The Mediterranean and Atlantic configurations
- Performances
- Operational system
- 2. Impact of currents and water level on waves
 - Between circulation and wave operational grids
 - Between embedded high resolution grids
- **3.** Conclusions and Perspectives





1. The Atlantic and Mediterranean configurations





92757 nodes SHOM bathymetry Resolution of 10 km offshore and around 200 m nearshore





1. The Atlantic and Mediterranean configurations





- 89695 nodes,
- SHOM bathymetry with Litto3D (resolution around 5 meters)
- Resolution of 10 km offshore and around 200 m nearshore





1. The Atlantic and Mediterranean configurations





Parameterizations



TEST 451 for NORGAS-UG and TEST 405 for MED-UG (Ardhuin et al., 2010). Modifications in the wind source and dissipation terms described in Janssen et

al. (2014)

TEST	405	451	463
C _{ds}	-2.2	-2.2	-2.8
S _u	0	1	0.6
β _{max}	1.55	1.52	1.52
Z _{0,max}	0.002	0.0	0.0
Br	0.00085	0.0009	0.0009
f _{FM}	2.5		

- Implicit N scheme (Roland, 2009) for spatial propagation
- Bottom friction parameterization (Ardhuin et al., 2003a). A constant Nikuradse roughness length of respectively 12 cm is applied for rocks
- 24 directions and 30 frequencies exponentially spaced from 0.0345 Hz to 0.5473 Hz at an increment of 10%
- Wind forcing : Arpege 0.1° every 3 hours
- Global wave forcing : MFWAM 0.1° every 3 hours









Map of the median grain size D_{50} (m)







Homonim

Hindcasts on eight significant storms over the past twenty years and a long period run of 1-year (July 2011 to June 2012)

Sensitivity tests on the bottom friction, atmospherical forcings, regional forcings, mesh resolution, spatial propagation scheme and on the addition of the current and water levels changes

Configuration	Satellites/buoys	Bias (m)	RMSE	SI	CORR
MED-UG	ENVISAT	-0.002	0.235	0.134	0.988
	JASON1	0.027	0.231	0.132	0.989
	JASON2	-0.025	0.229	0.154	0.986
	Buoys	-0.005	0.194	0.111	0.937
NORGAS-UG	ENVISAT	0.006	0.210	0.109	0.988
	JASON1	0.01	0.222	0.115	0.989
	JASON2	-0.026	0.207	0.104	0.992
	Buoys	0.0485	0.151	0.172	0.956





Performances on the significant wave height





NORGAS-UG







Impact of bottom friction



More information in Roland and Ardhuin (2014)



The operational system



- 5 Runs every day (00h short, 00h, 06h, 12h, 18h) with different length of forecast (from 54 h to 102h)
- Forced by Arpege 0.1° (3hrs of resolution), and by MFWAM spectra (resolution of MFWAM grid 0.1°)



Run (UTC)	Forecast	Availability (UTC)
00 h (court)	T ₀ +54 h	5h
00 h	T ₀ +102h	6h45
06 h	T ₀ +72h	13h10
12 h	T ₀ +84h	18h15
18 h	T ₀ +60h	1h10









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The HYCOM configuration :

- curvilinear, from 2 km to 500 m in coastal areas
- barotropic configuration



The HYCOM operational circulation grid for Atlantic (ATL). Only one contour each twenty contours is shown







Scatter diagram of H_s at the different buoys for Johanna storm (03/2008). In blue the results without the HYCOM forcing and in red with the HYCOM forcing. The two numbers are the coeff correlation for the two simulations.







without the HYCOM forcing and in pink with the HYCOM forcing.









MINISTÈRE DE LA DÉFENS

Significant wave height on 02.28.2010 0h



46°20'

46°15'

46°10'

46° 5'

45°55'

45°50'

15°45'





Sea surface height (in m)

Barotropic current (m/s)



Difference in significant wave height (in m) between a simulation with the HYCOM forcing and without on 02/28 at 5 a.m.









(Up) Effects of current and water level on significant wave heights. Diff hs is the difference of significant wave height between a simulation with the forcing of the circulation model and without, (Bottom) ssh and current at the Oleron Buoy.







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REFERENCE

WW3-Charente forced by NORGAS-UG

COUPLING SIMULATION:

- REFERENCE simulation with current from HYCOM zone 3
- HYCOM zone 4 with wave-induced current (results of ssh and current not presented here)

Sea surface height (in m)

Barotropic current (m/s)

Difference in significant wave height (in m) between a simulation 2 way and 1way on 02/28 at 5 a.m.

(Up) Effects of current and water level on significant wave heights. Diff hs is the difference of significant wave height between a simulation with the forcing of the circulation model and without, for the full line with the NORGAS-UG simulation and for the dashed lines with the Charente simulation.

(Bottom) ssh and current at the Oleron Buoy.

Conclusion

- 1. Presentation of the new French operational coastal wave forecasting system and its performances
- 2. A study on the impact of the wave-current interactions on these operational configurations during the Xynthia storm
 - Improvement with a refinement around the Pertuis-Charente area and the use of the OASIS coupler and the HYCOM circulation model

Perspectives

1. For the wave operational forecasting system :

- Add the last ww3 developments : implicit scheme (see presentation of Huchet et al.), triplet parameterization...
- Coupling with the Hycom 2D model
- Forcing with the Arome wind model (resolution: 0.025°)
- New configurations for Antilles, Guyane and La Réunion

2. Wave/current interaction study :

- Study of the wave-induced current, wave-induced surface stress and wave setup during the Xynthia storm
- Implementation of the HYCOM 3D model in this coupling strategy
- Study on the Iroise Sea during the 2013-2014 winter storms (PROTEVS campaign)

Thank you

With	out HYCC	OM forcing							
	Bilbao	Cherbour	g CapFer	ret Yeu	Pierres-N	Bretagne	F3	Sandettie	Manche
Bias	-0.1141	0.1716	-0.0744	0.1147	0.1596	0.2431	0.7484	0.2025	0.4432
Corr	0.9795	0.9029	0.9801	0.9562	0.9616	0.9667	0.8297	0.6949	0.9574
RMS	E 0.8057	0.2512	0.5362	0.2655	0.4907	0.7865	0.8651	0.6882	0.7954
SI	0.1589	0.3079	0.1402	0.1789	0.2115	0.2635	0.7246	0.4292	0.4187
With	HYCOM	forcing							
	Dilhaa								
	Blibao	Cherbour	g CapFer	ret Yeu	Pierres-N	Bretagne	F3	Sandettie	Manche
Bias	-0.0970	Cherbour 0.2888	g CapFer -0.0825	ret Yeu 0.0903	Pierres-N 0.1422	Bretagne 0.2842	F3 0.8281	Sandettie 0.2638	Manche 0.4671
Bias Corr	-0.0970 0.9825	Cherbour 0.2888 0.9612	g CapFer -0.0825 0.9768	ret Yeu 0.0903 0.9686	Pierres-N 0.1422 0.9781	Bretagne 0.2842 0.9826	F3 0.8281 0.8655	Sandettie 0.2638 0.8571	Manche 0.4671 0.9599
Bias Corr RMS	-0.0970 0.9825 E 0.7304	Cherbour 0.2888 0.9612 0.2957	g CapFer -0.0825 0.9768 0.5510	ret Yeu 0.0903 0.9686 0.2289	Pierres-N 0.1422 0.9781 0.4275	Bretagne 0.2842 0.9826 0.8447	F3 0.8281 0.8655 0.8766	Sandettie 0.2638 0.8571 0.5188	Manche 0.4671 0.9599 0.8996

Momentum equations

Quasivelocities eulerian velocities velocities $(\hat{u}, \hat{v}, \hat{w}) = (u, v, w) - (U_s, V_s, W_s)$

Lagrangian

Stokes

 $\left(-\frac{\partial J}{\partial x},-\frac{\partial J}{\partial y}\right)$

Ardhuin et al. (2008b), Michaud et al. (2012) :

$$\frac{\partial \hat{u}}{\partial t} + \hat{u}\frac{\partial \hat{u}}{\partial x} + \hat{v}\frac{\partial \hat{u}}{\partial y} + \hat{w}\frac{\partial \hat{u}}{\partial z} - f\hat{v} + \frac{1}{\rho}\frac{\partial p}{\partial x} = \left[f + \left(\frac{\partial \hat{v}}{\partial x} - \frac{\partial \hat{u}}{\partial y}\right)\right]V_s - W_s\frac{\partial \hat{u}}{\partial z} - \frac{\partial J}{\partial x} + F_{m,x} + F_{d,x}$$

- $\left(\left[\frac{\partial \hat{v}}{\partial x} \frac{\partial \hat{u}}{\partial y}\right]V_s W_s \frac{\partial \hat{u}}{\partial z}, \left[\frac{\partial \hat{v}}{\partial x} \frac{\partial \hat{u}}{\partial y}\right]U_s W_s \frac{\partial \hat{u}}{\partial z}$ 1. Vortex force:
- 2. Stokes-Coriolis force: $(fV_s, -fU_s)$
- 3. Wave-induced pressure gradient force
- 4. Wave dissipation force:

 $(F_{d,x},F_{d,y}) = (F_{d,def,x} + F_{d,fond,x} + F_{d,turb,x},F_{d,def,y} + F_{d,fond,y} + F_{d,turb,y})$

5. Mixing force :

$$(F_{m,x},F_{m,y})$$

Boundary conditions

 $(F_{d,x},F_{d,y}) = (F_{d,def,x} + F_{d,fond,x} + F_{d,turb,x},F_{d,def,y} + F_{d,fond,y} + F_{d,turb,y})$

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Boundary conditions

 $(F_{d,x},F_{d,y}) = (F_{d,def,x} + F_{d,fond,x} + F_{d,turb,x},F_{d,def,y} + F_{d,fond,y} + F_{d,turb,y})$

Near the bottom

 $K_{z} \frac{\partial \hat{u}}{\partial z}|_{z=-h} = \rho C_{D} \Delta_{u} \sqrt{\Delta_{u}^{2} + \Delta_{v}^{2}}$ $K_{z} \frac{\partial \hat{v}}{\partial z}|_{z=-h} = \rho C_{D} \Delta_{v} \sqrt{\Delta_{u}^{2} + \Delta_{v}^{2}}$

With $\Delta_u = \hat{u}(z^1) - 1.5U_s$

Longuet-Higgins (1953), Bennis et al. (2011)

Wave effects on mixing

• At the surface : $K_z \frac{\partial E_k}{\partial z} = \phi_{oc}$

with :
$$\phi_{oc} = \alpha u \star^3$$

 $l = \kappa z_{surf}$
 $z_{surf} = 1.6 H_{sw}$

Terray et al. (1996), Rascle et al. (2008)

• Near the bottom :

$$\tau_{bot} = [\tau_c] 1 + 1.2(|\tau_w| + |\tau_c|)^{3.2}]$$
Bottom stress
linked to current
Bottom stress
unked to current
Bottom stress
unked to wave unked to wave

Craig et Banner (1994)

Surface stress computed by a bulk formula: $\vec{\tau}_{s} = \rho_{a} \cdot C_{d} \cdot \vec{U}_{10}^{2}$

- 3 possibilities for Cd :
 - a drag coefficient constant computed by Pond and Pickard (1998)
 - A drag coefficient dependent on the wave age that we consider constant in space and time : α = 0,025
 - A drag coefficient dependent on the wave age calculated by the wave model

Wave effect on surface stress

