

Extreme Sea State Prediction at E.C.M.W.F

**Jean-Raymond Bidlot,
Peter Janssen,
*European Centre for Medium range Weather Forecasts,
Reading,
UK***

Motivations:

- There has been quite some recent progress in the understanding of freak waves.
- There is now a theoretical framework for deterministic simulation of freak waves.
- In operational forecasting, a stochastic approach is used, hence only statement of a probabilistic nature can be made.
- Janssen (2003) showed that the Kurtosis ($C4$) of the surface elevation (η), which is a measure of the deviation from the Normal Gaussian probability distribution of η , can be expressed in terms of 6th order integral of the wave action density to 3rd power.
- For operational implementation, a computationally tractable approximation was found, including shallow water effects and directionality.

Methodology:

- Following Janssen (2003), the expression for the Kurtosis of the sea surface elevation ($C4$) is simplified using the narrow band approximation (both in frequency and direction).
- It was extended to include the stabilizing effect in shallow water (Janssen and Onorato 2007).
- For operational implementation, a fit to the derived expression is used.
- It requires a proper evaluation of the relative spectral width at the peak both in frequency (δ_ω) and in direction (δ_θ).
- New output parameters, the maximum individual wave height H_{max} and the associated maximum period T_{max}
- Comparison with buoy data is attempted.

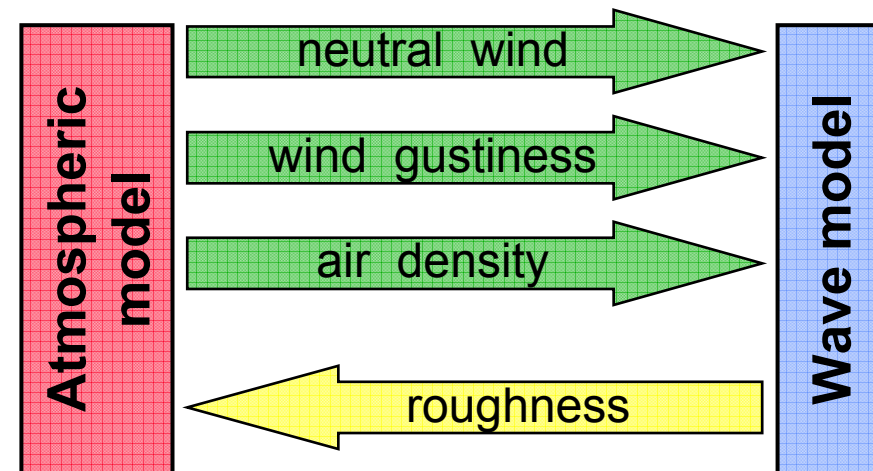
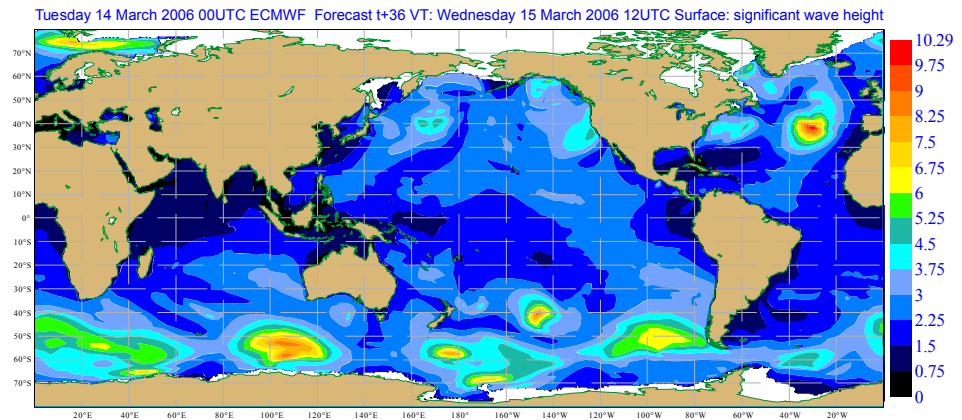
Conclusion:

- The freak wave warning system has been extended by including effects of directionality and shallow water in the estimation of $C4$.
- H_{max} provides a simple measure for extreme sea state.
- Preliminary validation of H_{max} is satisfactory.

Introduction:

ECMWF global wave model, ECWAM:

- Global from 81°S to 90°N
- Coupled to the atmospheric model with feedback of the sea surface roughness change due to waves.
- The interface between WAM and the IFS has been generalised to include air density and gustiness effects on wave growth and more recently neutral winds.
- Latest model changes (Sep. 2009) include a formulation for swell damping.



ECMWF Wave Model Configurations

Deterministic model

- 40 km grid spacing .
- 30 frequencies.
- 24 directions.
- Coupled to the TL799 model (25km).
- Analysis every 6 hrs and 10 day forecasts from 0 and 12Z.

Probabilistic forecasts

(EPS)

- 110 km grid spacing.
- 30 → 25 frequencies *.
- 24 → 12 directions *.
- Coupled to TL399 → TL255 model *.
- (50+1) (10+5) day forecasts from 0 and 12Z (monthly once a week).

* Change in resolutions after 10 days

NB: also in seasonal forecast at lower resolutions

ECMWF Wave Model **Future*** Configurations

Deterministic model

- **28** km grid spacing .
- **36** frequencies.
- **36** directions.
- Coupled to the TL**1279** model (16km).
- Analysis every 6 hrs and 10 day forecasts from 0 and 12Z.

Probabilistic forecasts

(EPS)

- **55** km grid spacing.
- **36** → 30 frequencies *.
- **36** → 24 directions *.
- Coupled to TL639 → TL319 model *.
- (50+1) (10+5) day forecasts from 0 and 12Z (monthly once a week).

* Change in resolutions after 10 days

*: resolution increase planned later in the year

Extension of the freak wave warning system:

Kurtosis of the sea surface elevation η :
$$C_4 = \frac{\langle \eta^4 \rangle}{3 \langle \eta^2 \rangle^2} - 1$$

$$C_4 = C_4^{dyn} + \alpha \varepsilon^2$$

For deep water,
with the narrow band approximation,
we use the fit:

$$C_4^{dyn} = \beta \frac{BFI^2}{\delta_\theta}$$

BFI: Benjamin Feir Index:

$$BFI = \sqrt{2} \frac{\varepsilon}{\delta_\omega}$$

δ_ω : relative frequency width at the peak

δ_θ : relative directional width at the peak

integral steepness ε :

$$\varepsilon = k_0 \sqrt{m_0}$$

$$m_0 = \langle \eta^2 \rangle = \iint E(\omega, \theta) d\omega d\theta$$

$E(\omega, \theta)$: 2D wave spectrum

k_0 : peak wave number

Extension of the freak wave warning system:

$$C_4 = C_4^{dyn} + \alpha \varepsilon^2$$

$$C_4^{dyn} = \beta \frac{BFI^2}{\delta_\theta} \quad \alpha = 6$$

$$\beta = 0.062 \frac{\pi}{3\sqrt{3}} \quad BFI = \sqrt{2} \frac{\varepsilon}{\delta_\omega}$$

$$\delta_\omega = \frac{1}{\pi} \frac{1}{Q_p}$$

peakedness: $Q_p = \frac{2}{m_0} \int \omega E^2 d\omega d\theta$

$$D: E(\omega) > 0.4 E(\omega_0)$$

$$\delta_\theta = \sqrt{2(1 - M_1)}$$

$$M_1 = \frac{1}{m_0} \int \cos(\theta) E(\omega, \theta) d\omega d\theta$$

$\delta\omega$ and $\delta\theta$ are also determined from parabolic fit around the peak of the frequency and direction spectra respectively.

Maximum wave height:

Expectation value of H_{\max}

$$\langle H_{\max} \rangle = \int H_{\max} p_m(H_{\max}) dH_{\max}$$

Starting from the pdf of the surface elevation which depends on skewness and kurtosis (Cram-Charlier expansion), $p_m(H_{\max})$ is derived from the pdf of the wave height, defined as twice the envelop of the wave train:

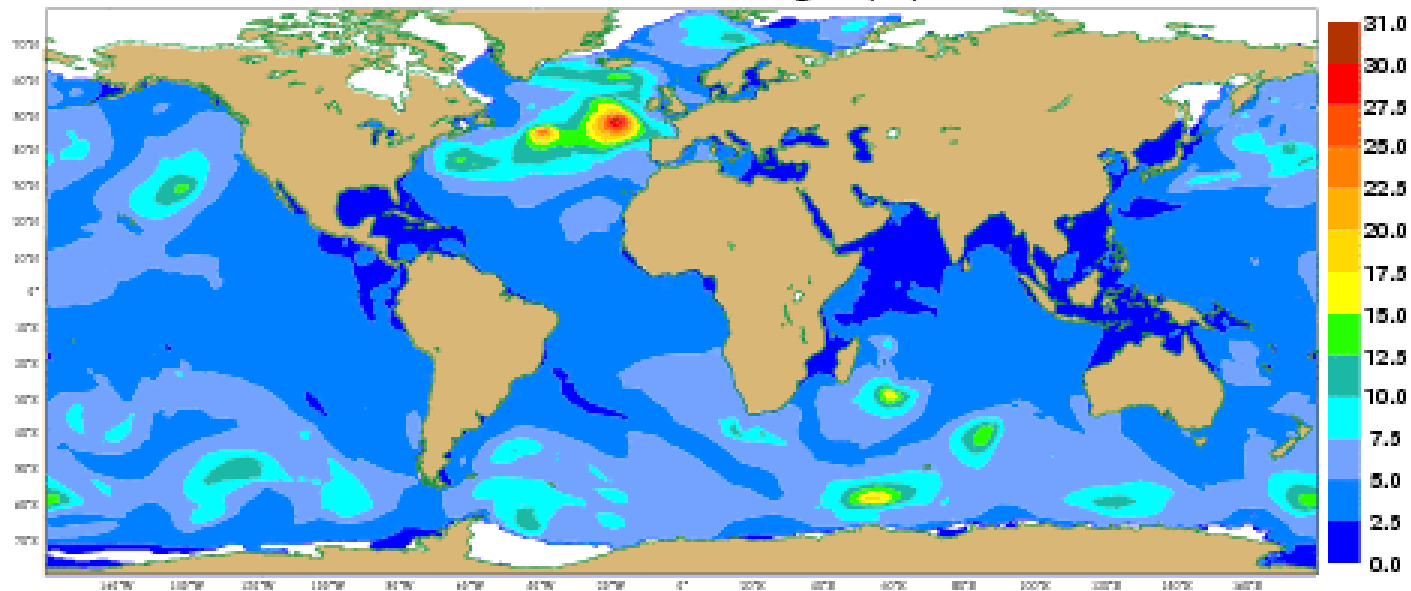
$$\frac{\langle H_{\max} \rangle}{H_{sig}} = \sqrt{z}$$

$$z = z_0 + \frac{\gamma}{2} + \frac{1}{2} \log \left[1 + C_4 \left\{ 2 z_0 (z_0 - 1) - \gamma (1 - 2 z_0) - \frac{1}{2} \left(\gamma^2 + \frac{\pi^2}{6} \right) \right\} \right]$$

$$z_0 = \frac{1}{2} \log(N) \quad \gamma = 0.5772 \quad \text{Number of waves } N = \frac{\text{duration}}{T_p}$$

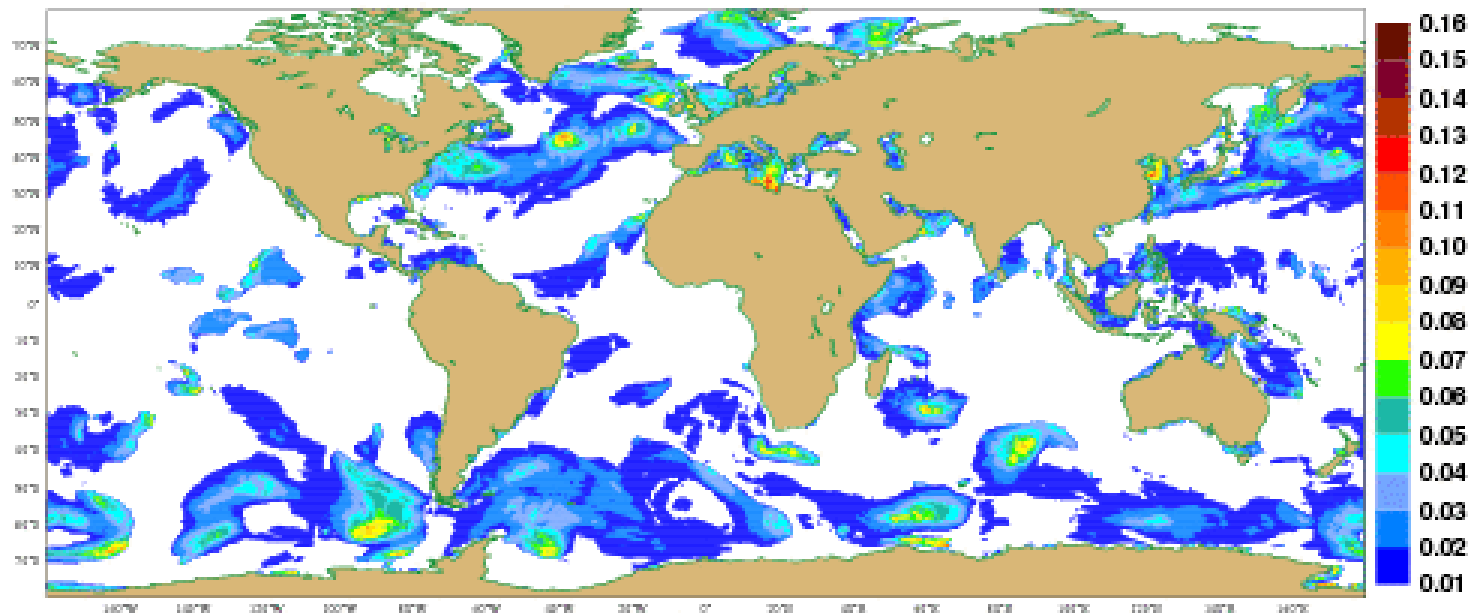
Example : expected Hmax within 3 hours

ECMWF Analysis VT:Saturday 10 February 2007 00UTC Surface:
Maximum wave height (m)

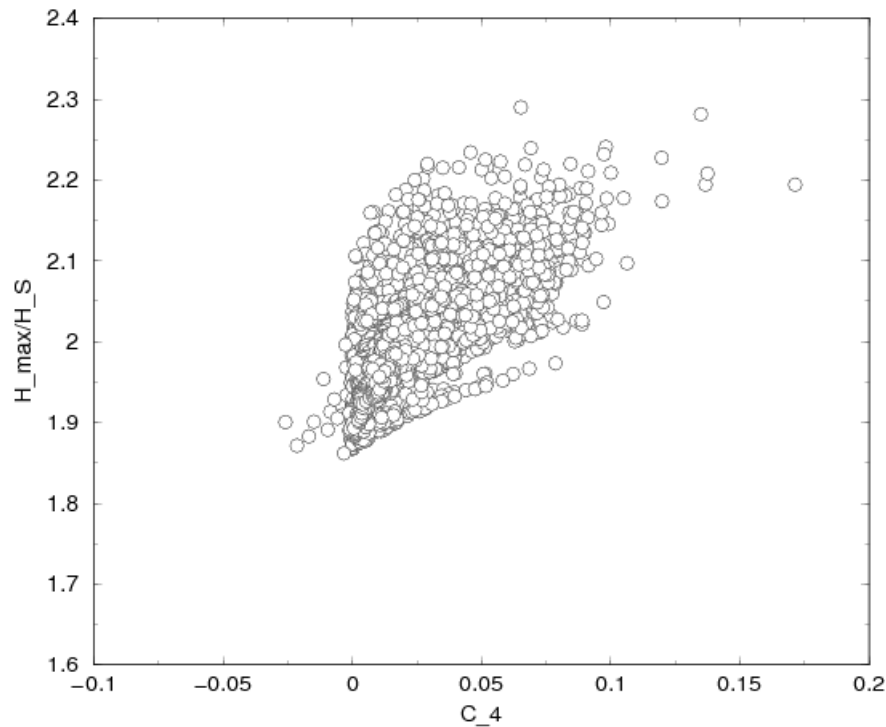


Example : corresponding kurtosis

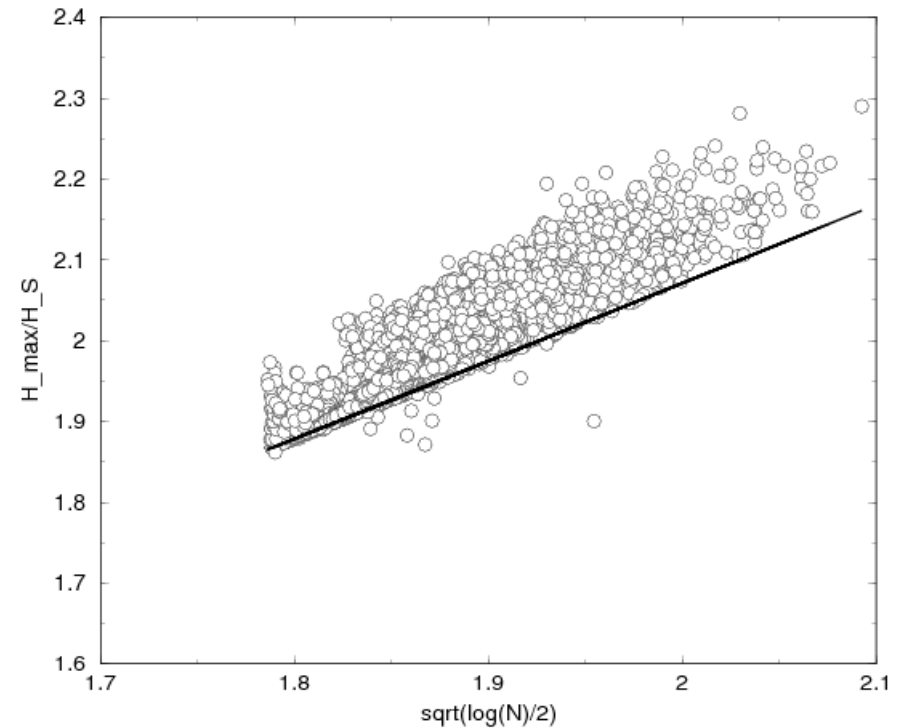
ECMWF Analysis VT:Saturday 10 February 2007 00UTC Surface: Wave spectral kurtosis
Kurtosis



Results :



H_{max}/H_S vs C_4
for all grid points of previous
figures

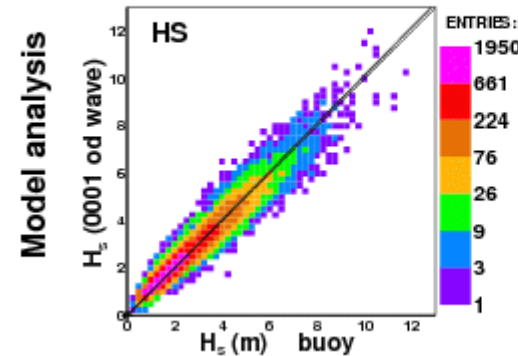


H_{max}/H_S vs number of waves (N)
for all grid points of previous
figures

Comparison with buoy data :

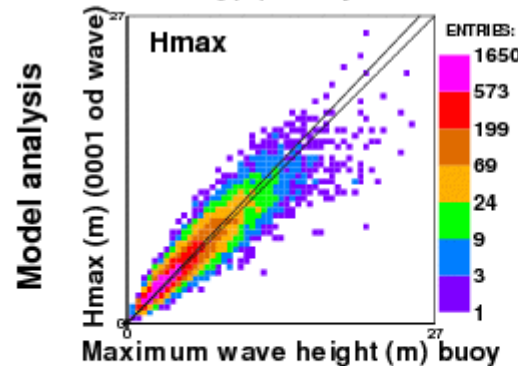
Comparison against Canadian (MEDS) and Norwegian (Oceanor) buoys:

All buoys 20060202 to 20080131



ENTRIES = 36520
MODEL MEAN = 2.44 STDEV = 1.273
BUOY MEAN = 2.37 STDEV = 1.325
LSQ FIT: SLOPE = 0.933 INTR = 0.228
RMSE = 0.324 BIAS = 0.069
CORR COEF = 0.971 SI = 0.134
SYMMETRIC SLOPE = 1.013

NB: Hs and Hmax as recomputed from archived spectra.



ENTRIES = 32495
MODEL MEAN = 4.89 STDEV = 2.495
BUOY MEAN = 4.54 STDEV = 2.584
LSQ FIT: SLOPE = 0.911 INTR = 0.750
RMSE = 0.922 BIAS = 0.348
CORR COEF = 0.944 SI = 0.188
SYMMETRIC SLOPE = 1.051

Model Hmax is the expected value in a 3 hour record

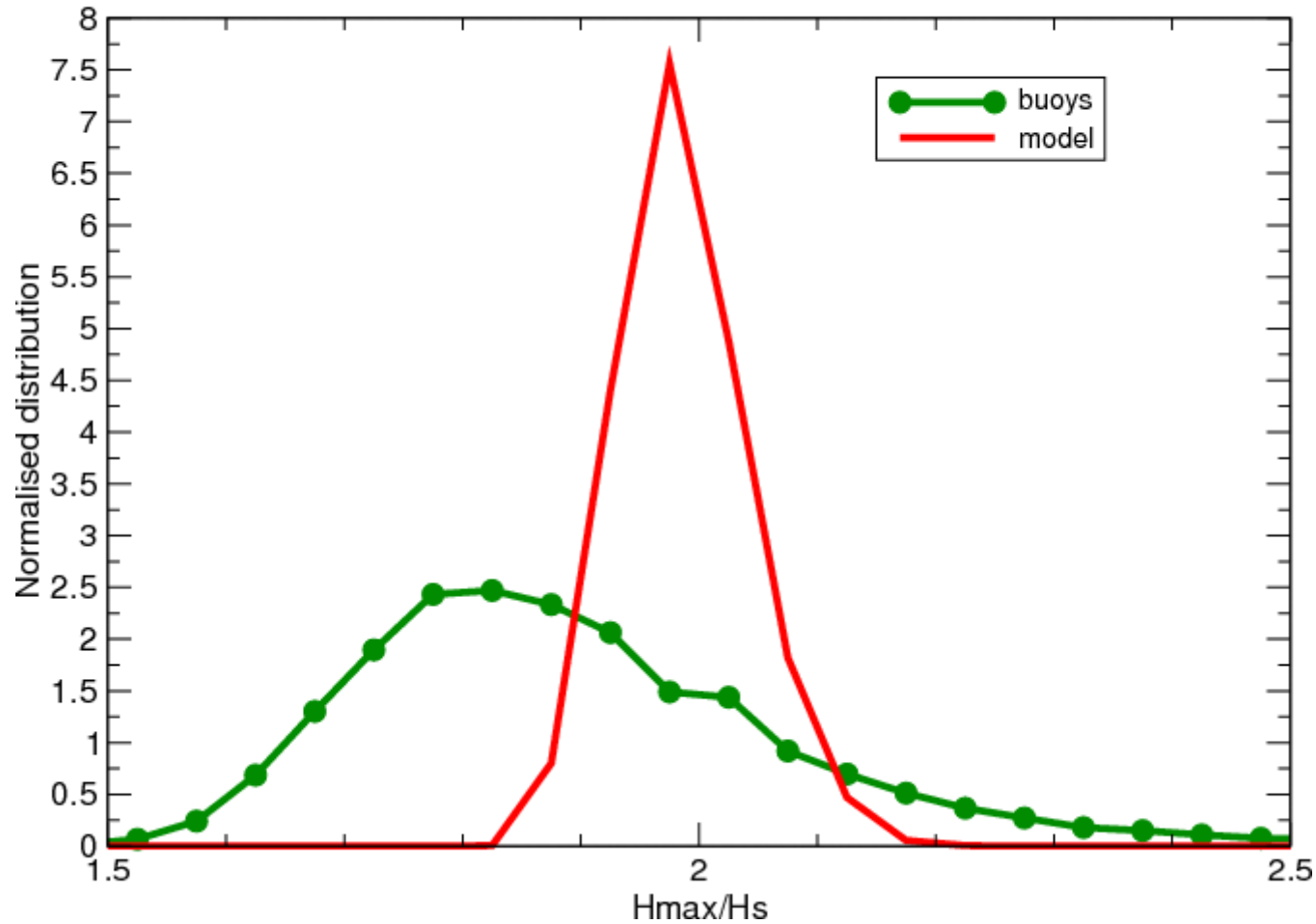
Buoys used:

MEDS: 44137,44138, 44139, 44140, 44150, 44251, 44255, 46036, 46132, 46147,46184, 46205, 46206, 46207, 46208.

Oceanor: LFB1, LFB2

Comparison with buoy data :

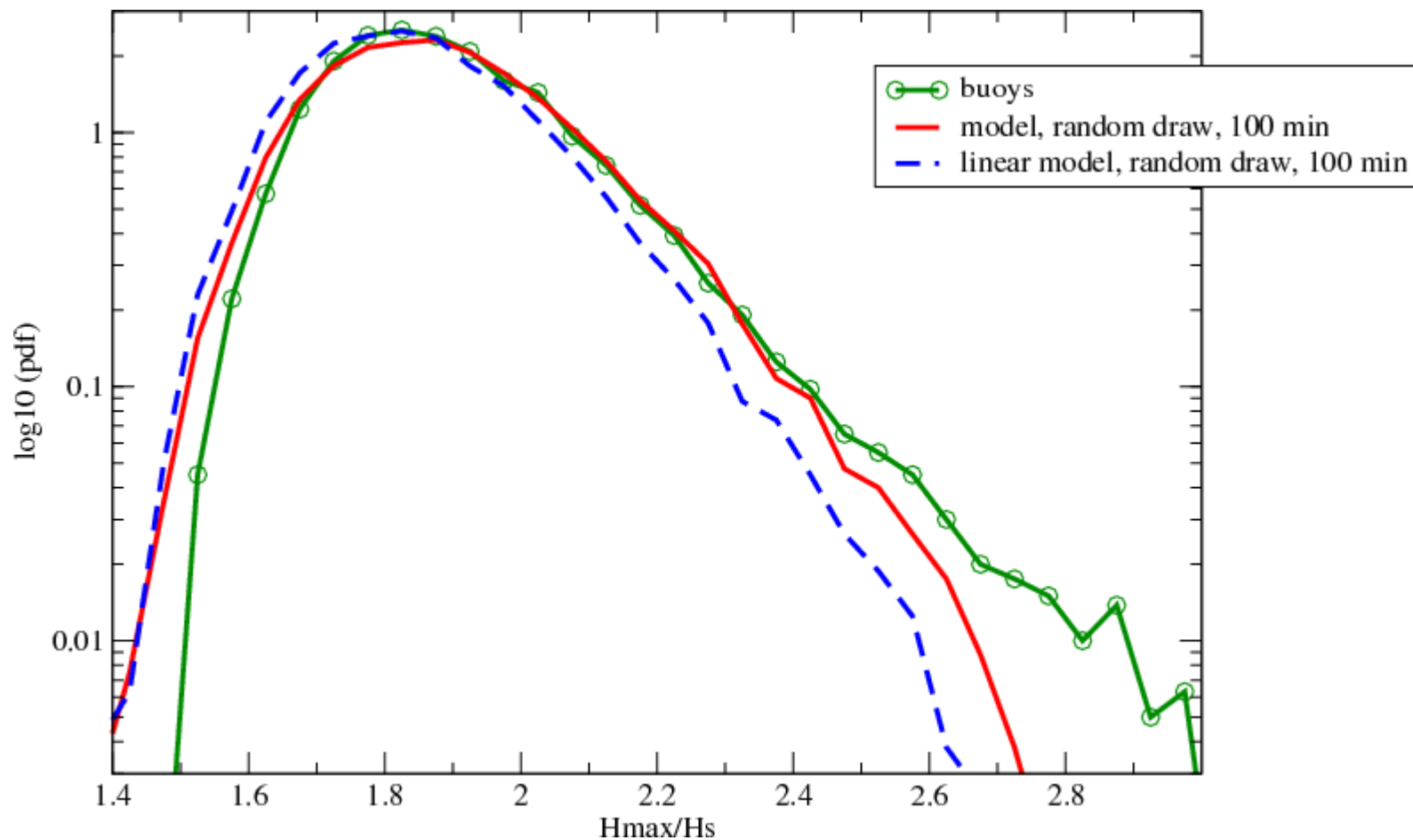
Comparison to Canadian off-shore buoys
from February 2006 to January 2008



Comparison with buoy data :

- H_{\max} observed is from a single realization, where as H_{\max} modeled is the expectation value.
- Can the observed distribution be simulated?
- Yes, by generating a random draw from the theoretical $p_m(H_{\max})$, with given N and C4.

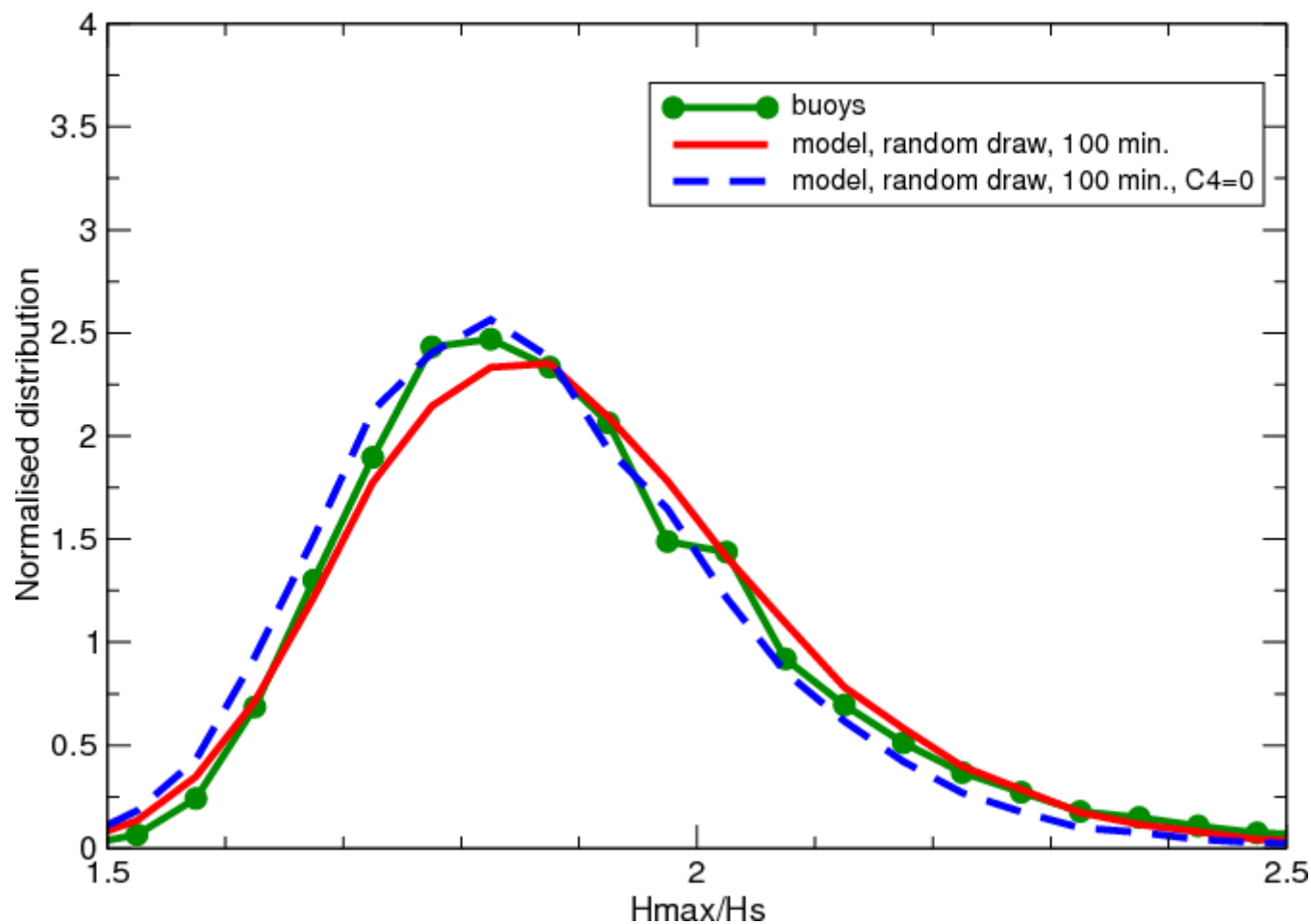
Comparison with buoy data :



Comparison with buoy data :

Comparison to Canadian off-shore buoys

from February 2006 to January 2008



Conclusion:

- The freak wave warning system has been extended by including effects of directionality and shallow water in the estimation of $C4$.
- H_{\max} provides a simple measure for extreme sea state.
- H_{\max} in operations since June 2008.
- Preliminary validation of H_{\max} is satisfactory.