

Combined Wind and Waves over a Fringing Reef

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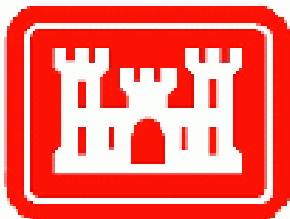
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U.S. Army Corps of Engineers, Vicksburg MS

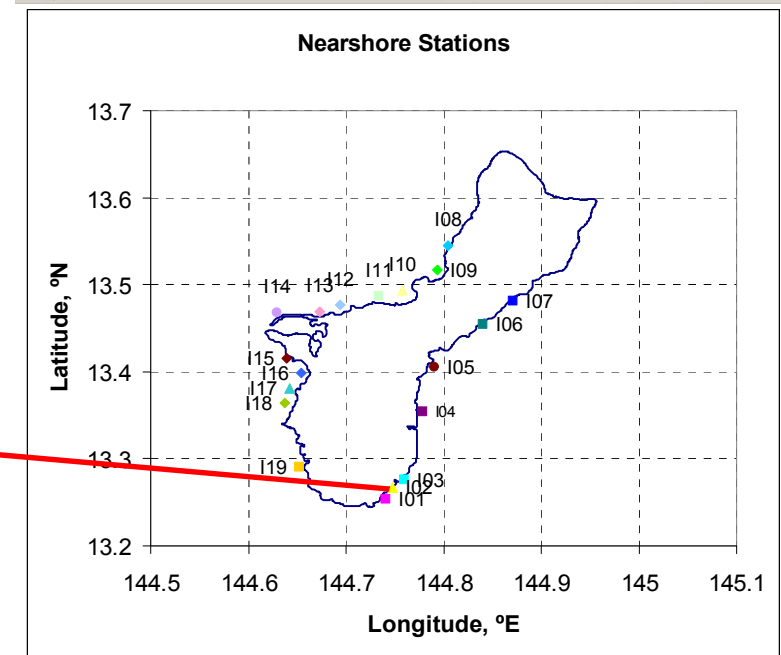
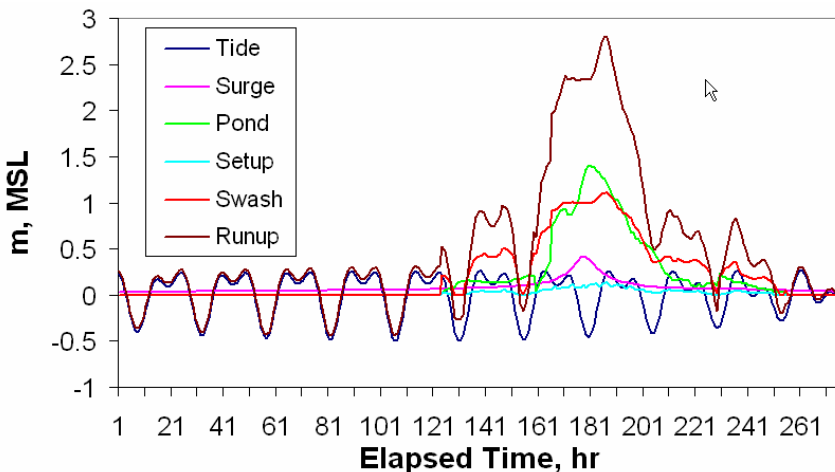
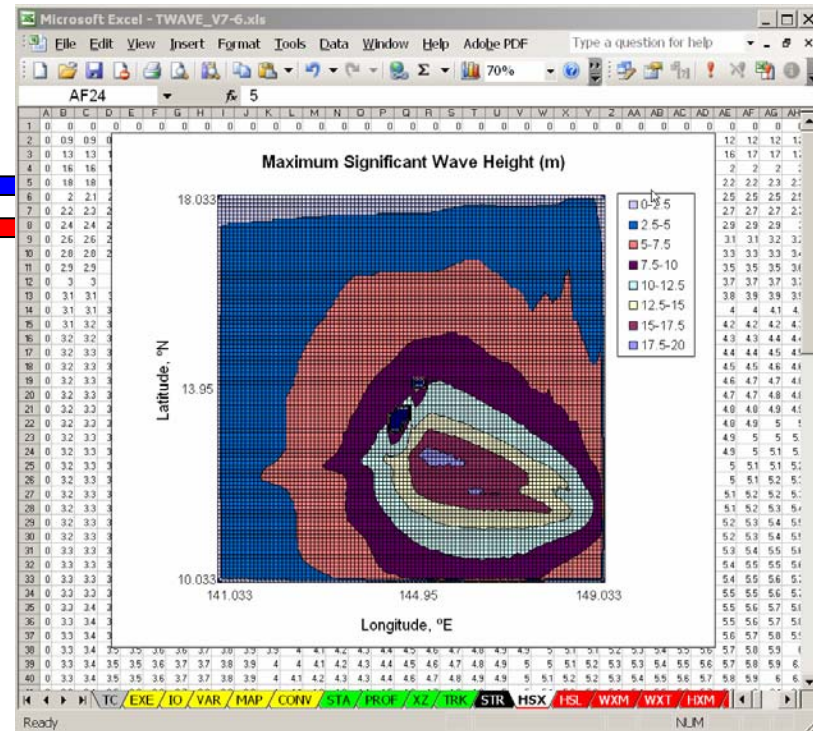
10th International Workshop on Wave Hindcasting and
Forecasting & Coastal Hazard Assessment

November 16, 2007



Introduction

- Surge and Wave Island Modeling Studies (SWIMS), USACE
 - Coastal modeling package: TWAVE
- Targeted for U.S. Civil Defense agencies and district offices
- PC-based, user-friendly, comprehensive package
- Multi-level: Quick answers with large uncertainty, and slow answers with small uncertainty



Objective

- To test the applicability of various models to simulate wave transformation and setup over fringing coral reefs

Summary and Conclusion

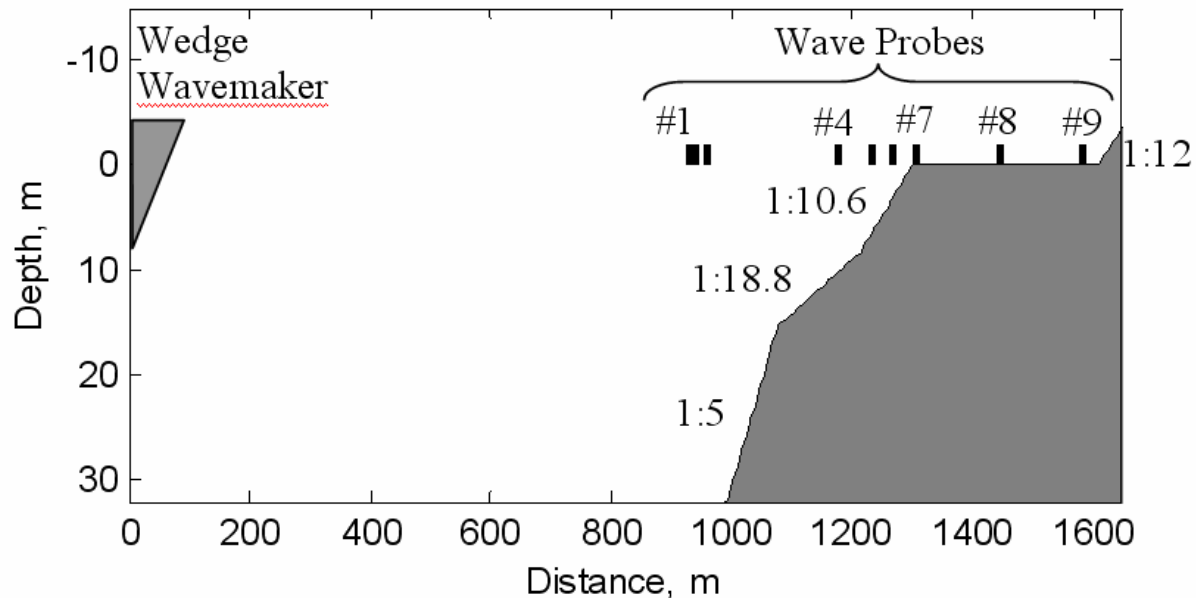
- Setup generated by strong winds is a significant contribution to water levels over fringing coral reefs
- Wind also causes increased wave breaking intensity causing the waves to break further offshore and reducing the setup
- STWAVE and ADCIRC are agreed relatively well with laboratory measurements of wave heights and water levels over a fringing reef
- 1-D wave energy balance models are robust, fast and are suitable for engineering applications, feasibility studies, etc.

Outline

- Laboratory Datasets
- Numerical Models
- Results
 - Waves only
 - Wind and waves
- Discussion
- Summary and Conclusion
- Future Work

Laboratory Dataset

- University of Michigan Laboratory Study
 - 83 Tests
 - 1:64 scale Guam-type reef
 - Wind and irregular waves
 - Gauges 1-6 on reef slope and gauges 7-9 on reef top



STWAVE and ADCIRC (STAD)

- STeady-state spectral WAVE model
 - Solves the wave action balance equation by finite-differences on a cartesian grid
 - **Wave breaking** modified to use **Battjes and Janssen (1978)**
$$D_b = \frac{1}{4} \rho g B \bar{f} H_b^2 Q_b \quad H_{rms}^2 \ln Q_b = H_b^2 (1 - Q_b) \quad H_b = 0.88 \tanh(kd) / k$$
 - 5-m grid resolution
 - No bottom friction
 - No wind generation (1-km fetch, simplicity)
- ADvanced CIRCulation model
 - Finite-element, nonlinear, depth-averaged flow model
 - 10- to 30-m grid resolution
- Coupling
 - Wave radiation stress gradients from STWAVE to ADCIRC
 - Water levels from ADCIRC to STWAVE
 - No wave-current interaction
 - At least 3 simulations of STWAVE and 2 of ADCIRC

One-dimensional Models

- Wave energy balance equation

$$\frac{\partial}{\partial x}(EC_g \cos \theta) + D_b + D_f = 0$$

- Wave Breaking

- Dally et al. 1985 (DDD85)

$$D_b = \frac{\kappa}{d} [EC_g - \min(E, E_s)C_g],$$

$$E_s = \frac{1}{8} \rho g (\Gamma d)^2$$

- Janssen and Battjes 2007 (ABJB07)

$$D_b = \frac{3\sqrt{\pi}}{16} \rho g B_f^- \frac{H_{rms}^3}{d} Q_b,$$

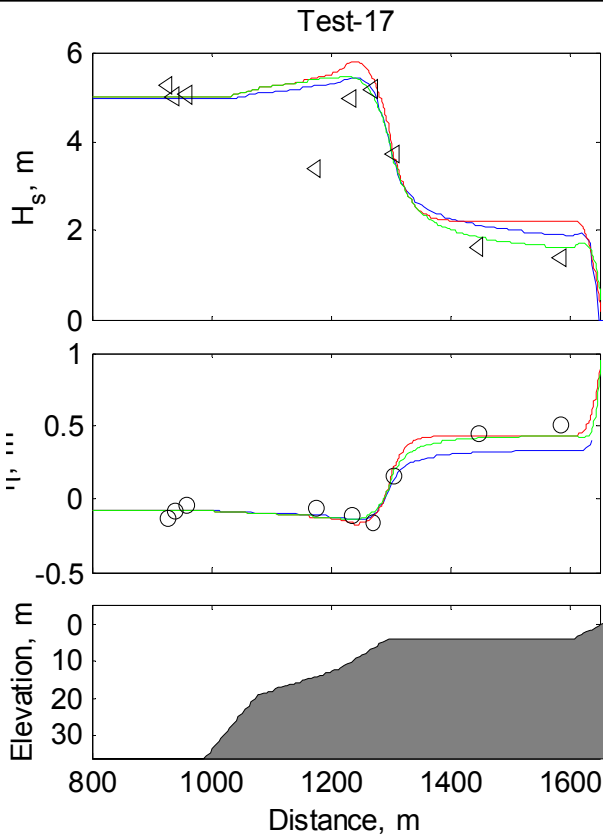
$$Q_b = 1 + \frac{4}{3\sqrt{\pi}} \left(R^3 + \frac{3}{2} R \right) \exp(-R^2) - \operatorname{erf}(R),$$

$$R = H_b / H_{rms}$$

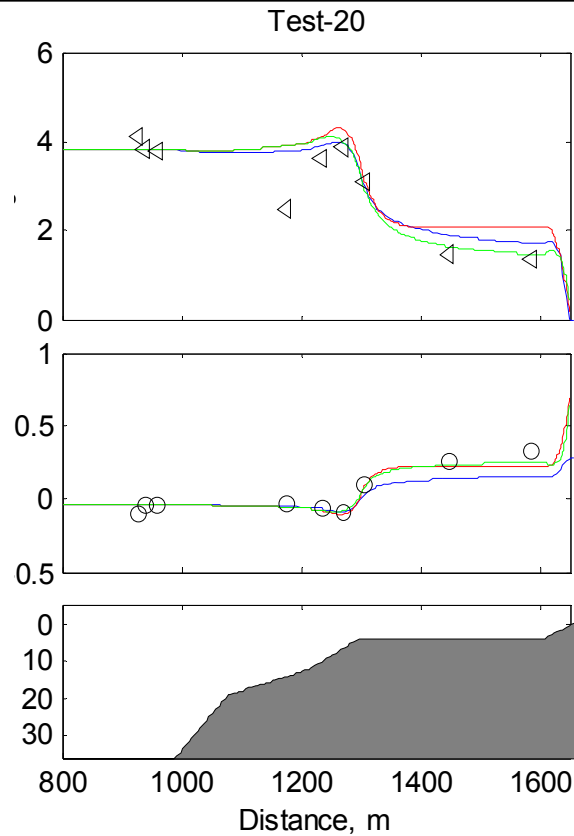
- Momentum balance

$$\rho g (h + \eta) \frac{\partial \eta}{\partial x} + \frac{\partial S_{xx}}{\partial x} = \tau_{wx},$$

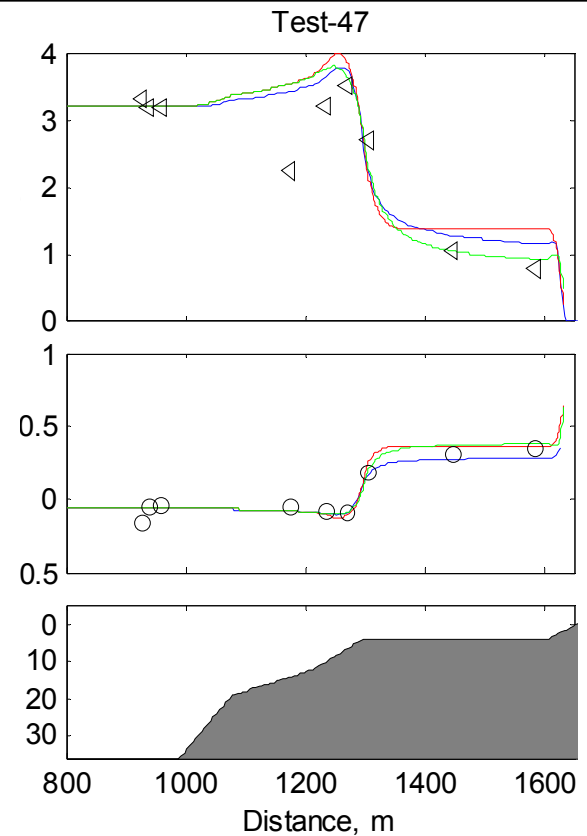
UM Dataset, Waves Only



$H_o = 4.99$ m $T_p = 12.0$ sec
 $h_r = 3.26$ m $U = 0.5$ m/sec



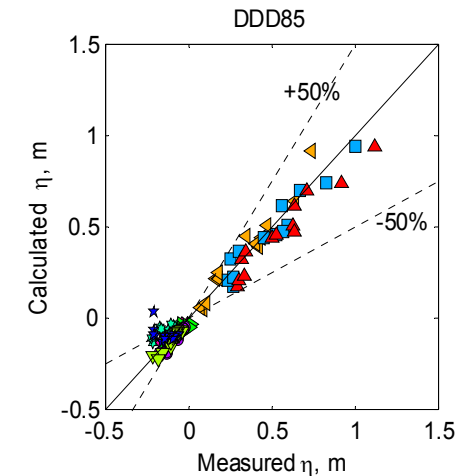
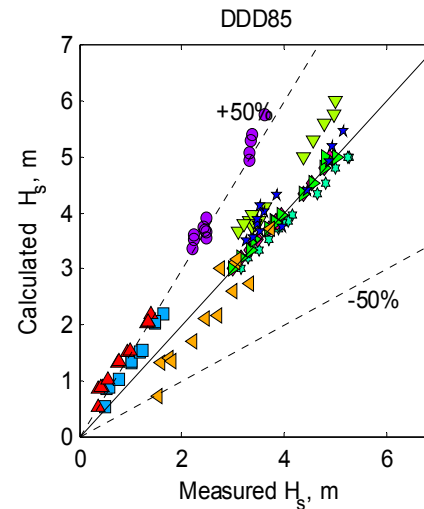
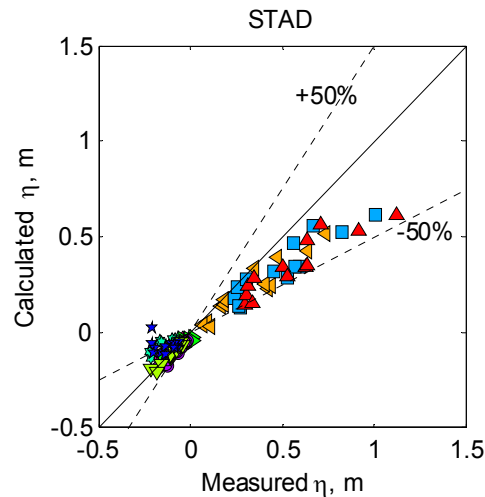
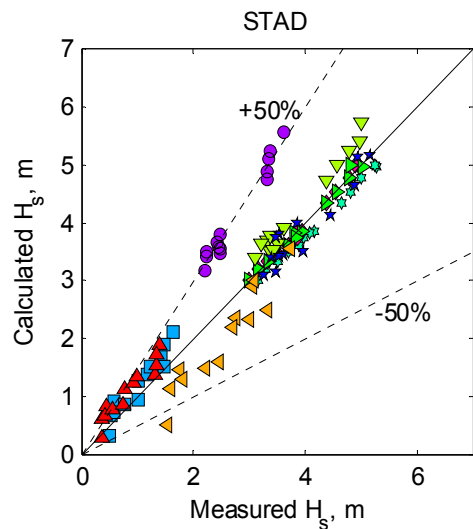
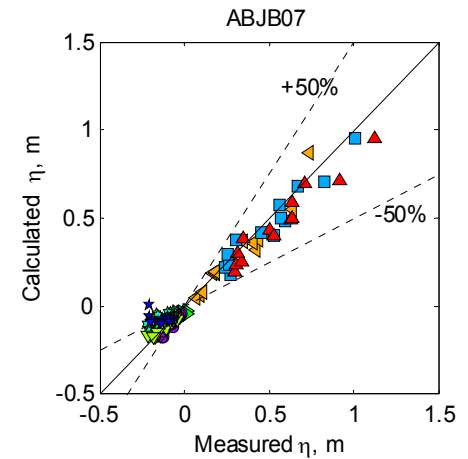
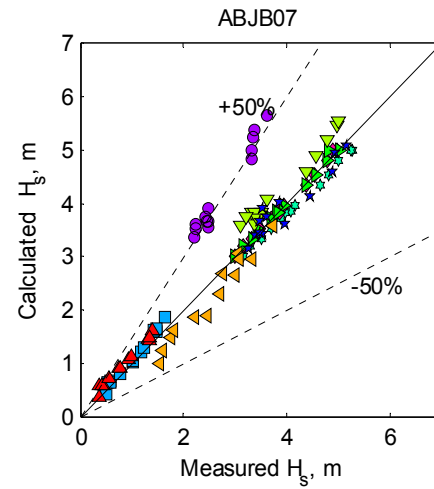
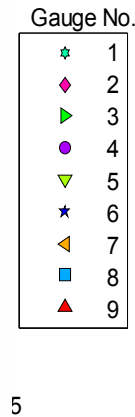
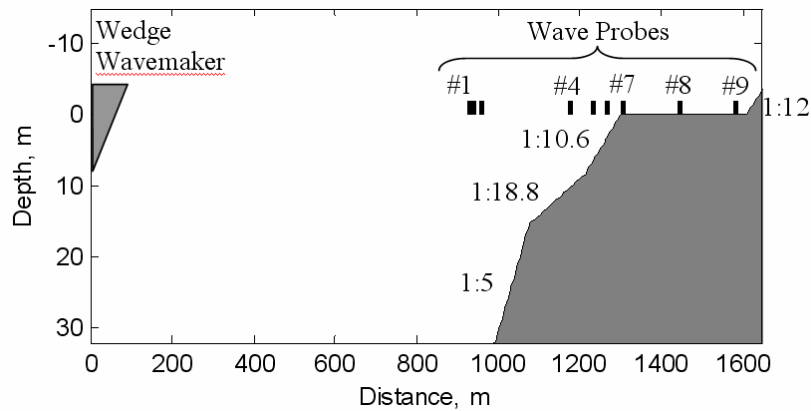
$H_o = 3.84$ m $T_p = 10.0$ sec
 $h_r = 3.26$ m $U = 0.4$ m/sec



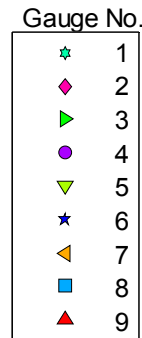
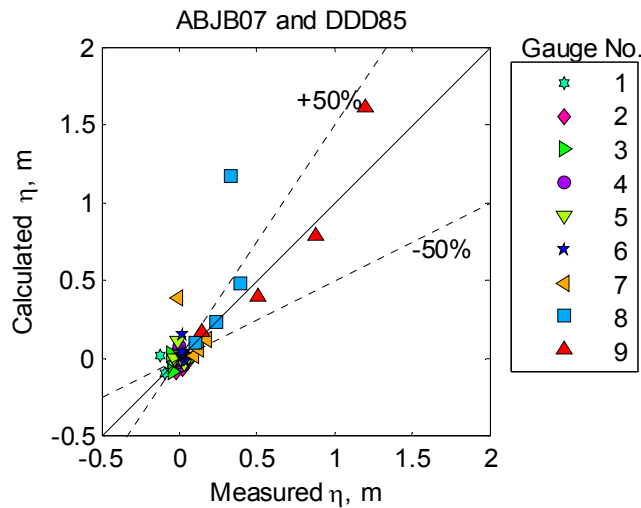
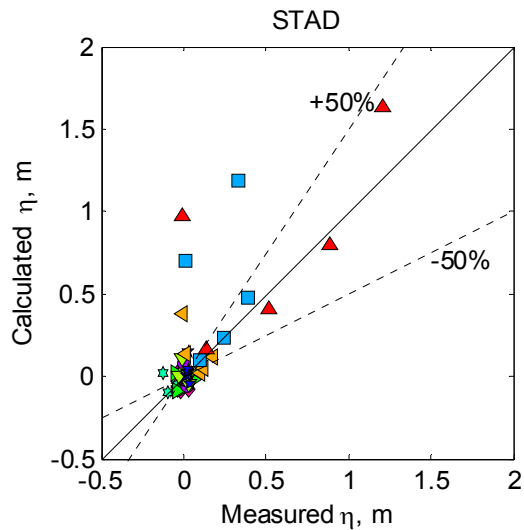
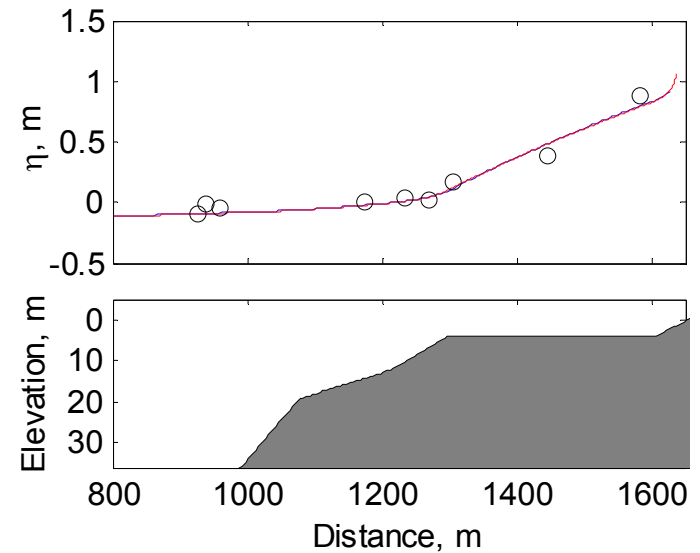
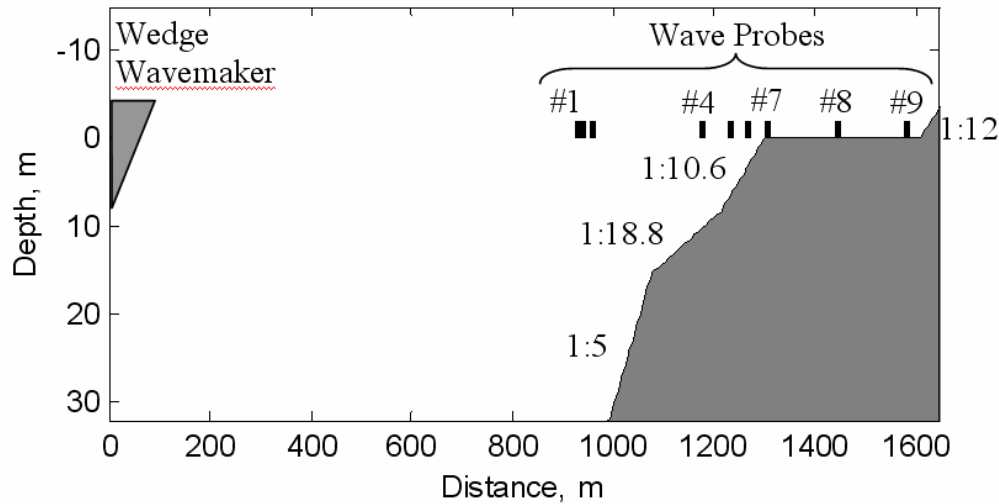
$H_o = 3.20$ m $T_p = 12.0$ sec
 $h_r = 1.92$ m $U = 0.7$ m/sec

— ABJB07, — DDD85, — STAD

UM Dataset, Waves Only

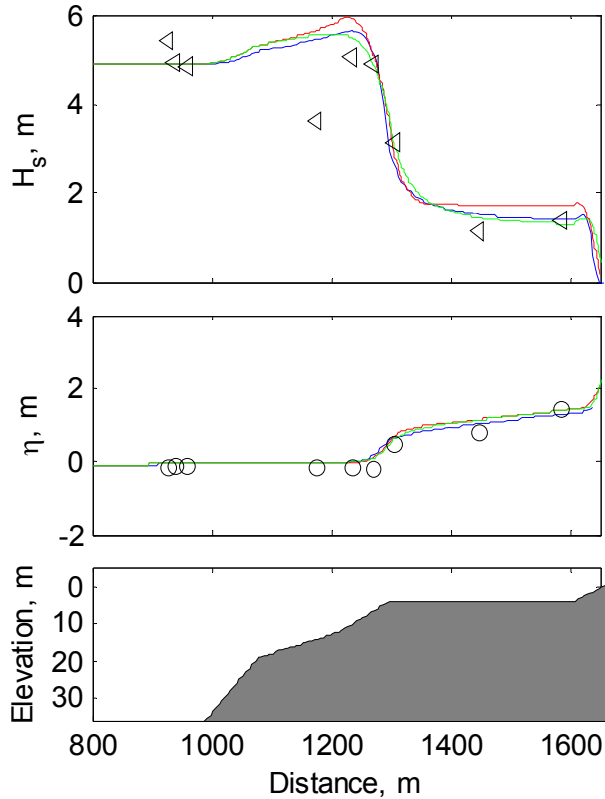


UM Dataset, Wind Only



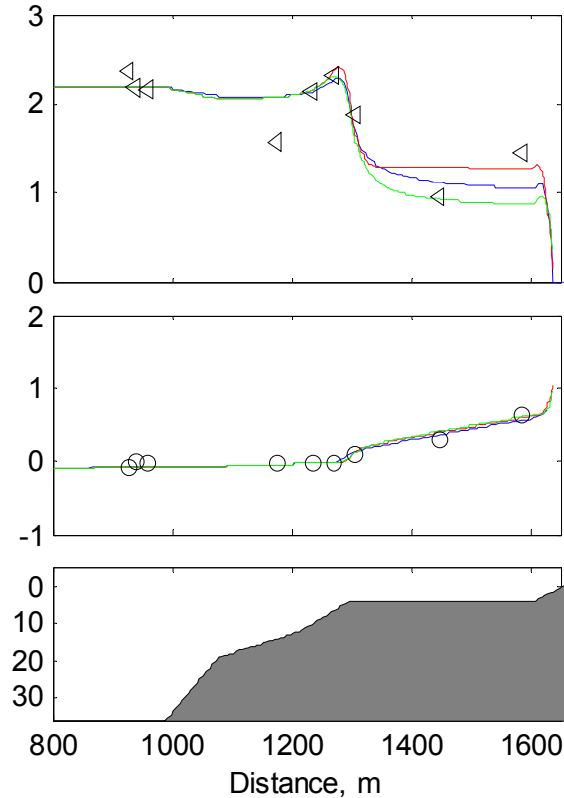
UM Dataset, Wind and Waves

Test-70



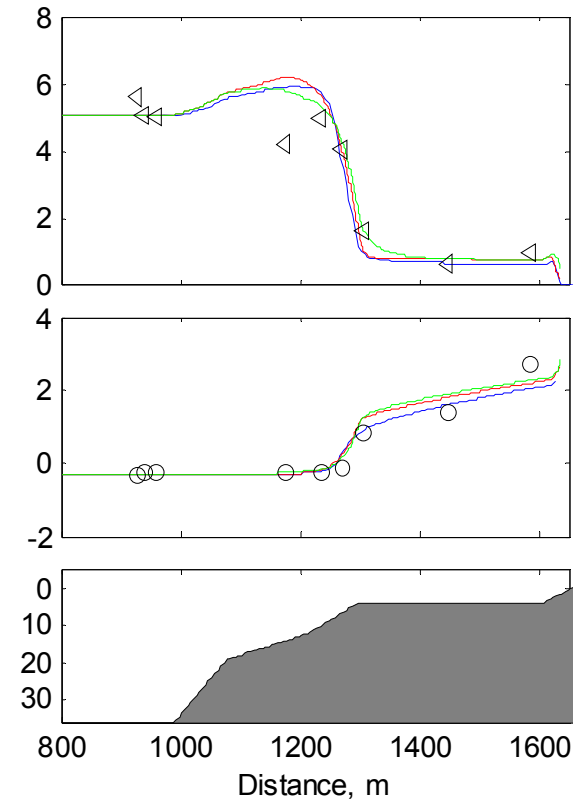
$H_o = 4.89$ m $T_p = 14.0$ sec
 $h_r = 1.92$ m $U = 41.0$ m/sec

Test-75



$H_o = 2.18$ m $T_p = 8.0$ sec
 $h_r = 1.92$ m $U = 32.4$ m/sec

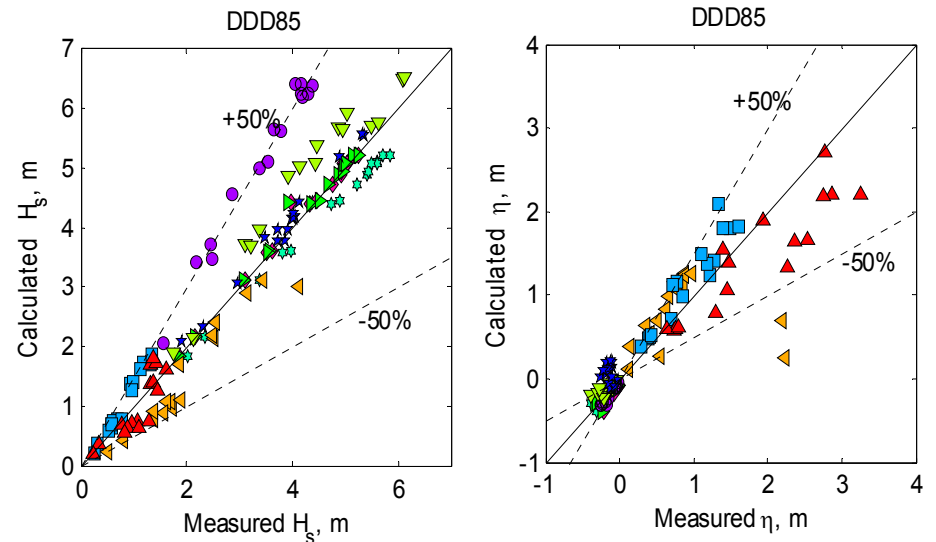
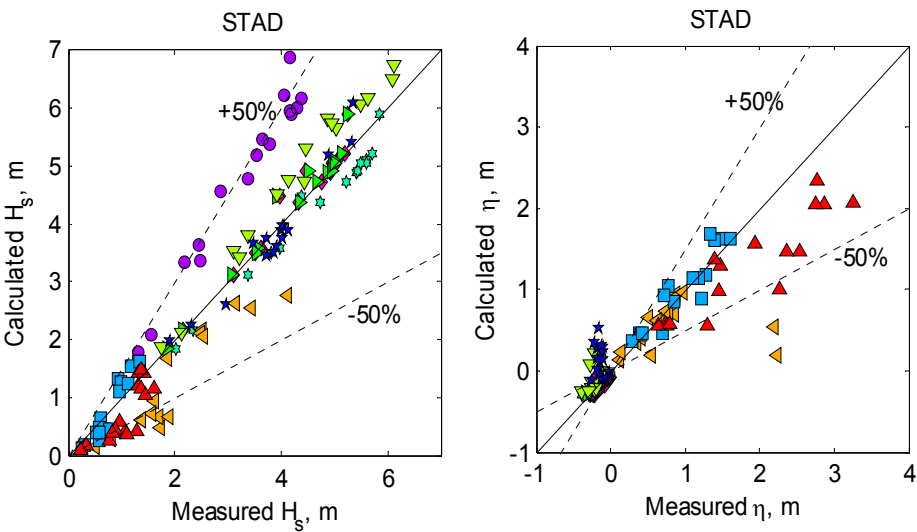
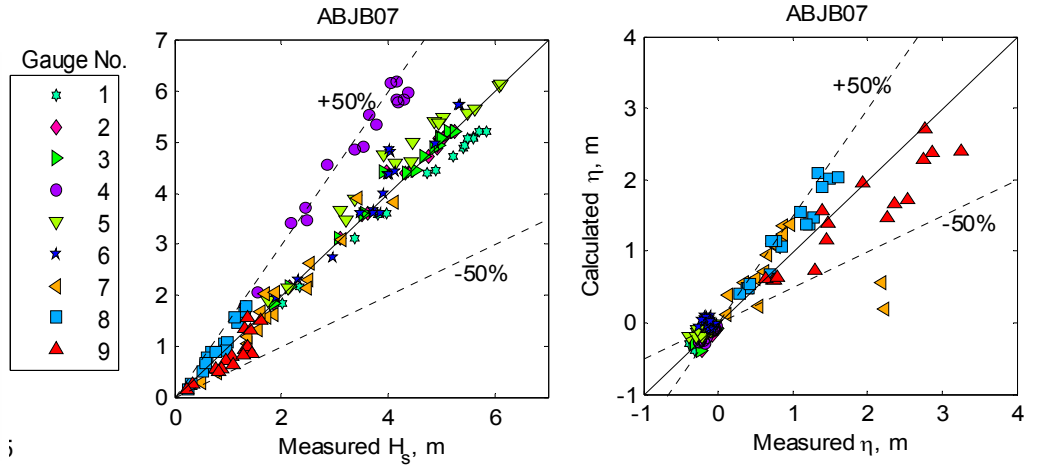
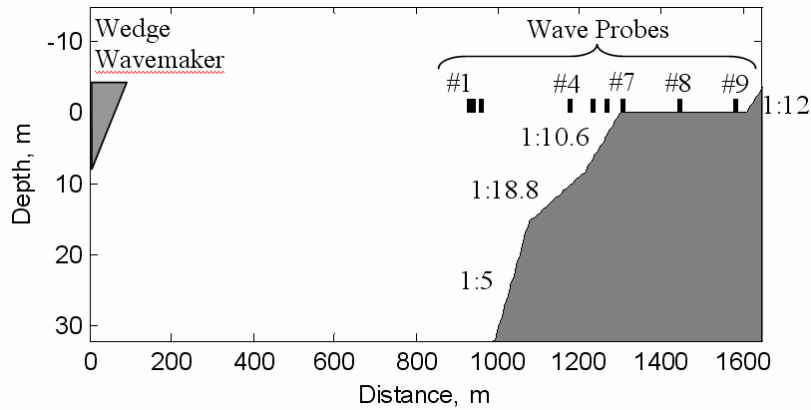
Test-85



$H_o = 5.06$ m $T_p = 16.0$ sec
 $h_r = 0.0$ m $U = 41.4$ m/sec

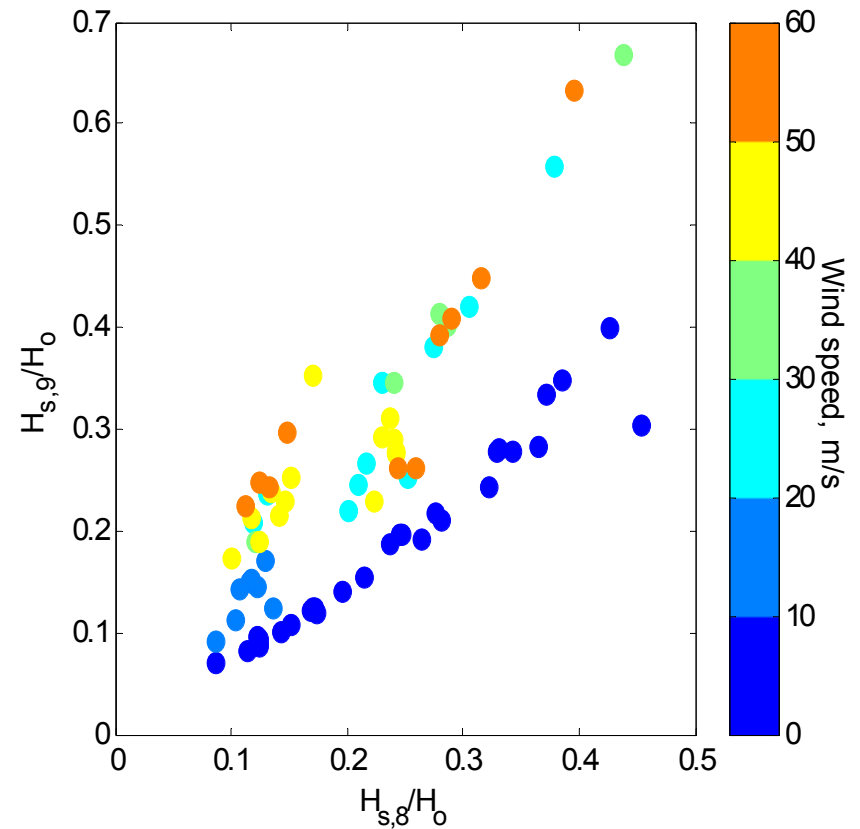
— ABJB07, — DDD85, — STAD

UM Dataset, Wind and Waves



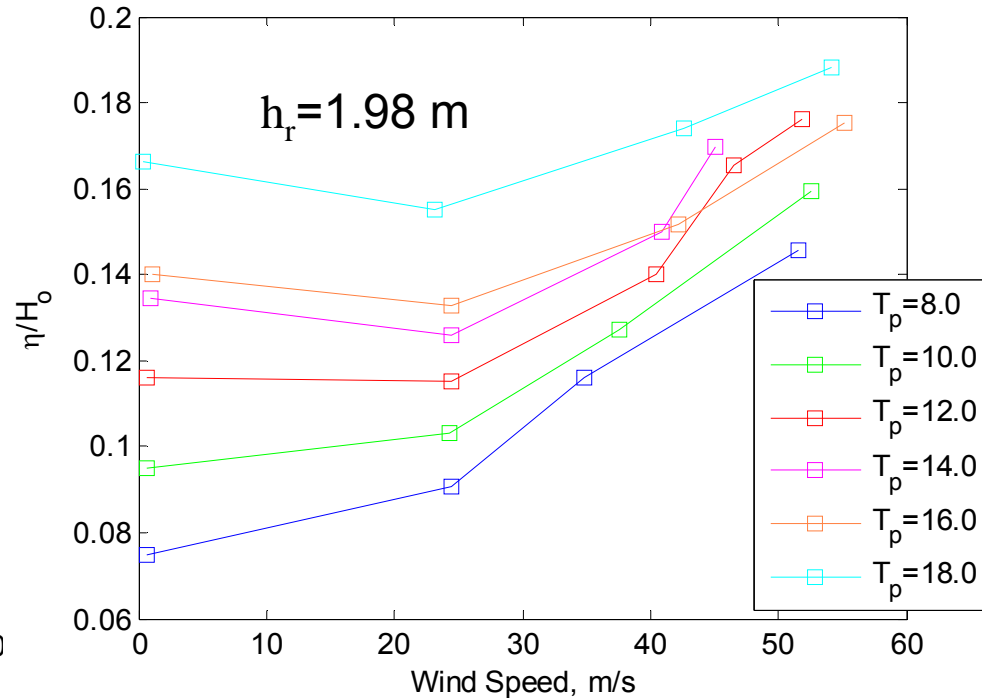
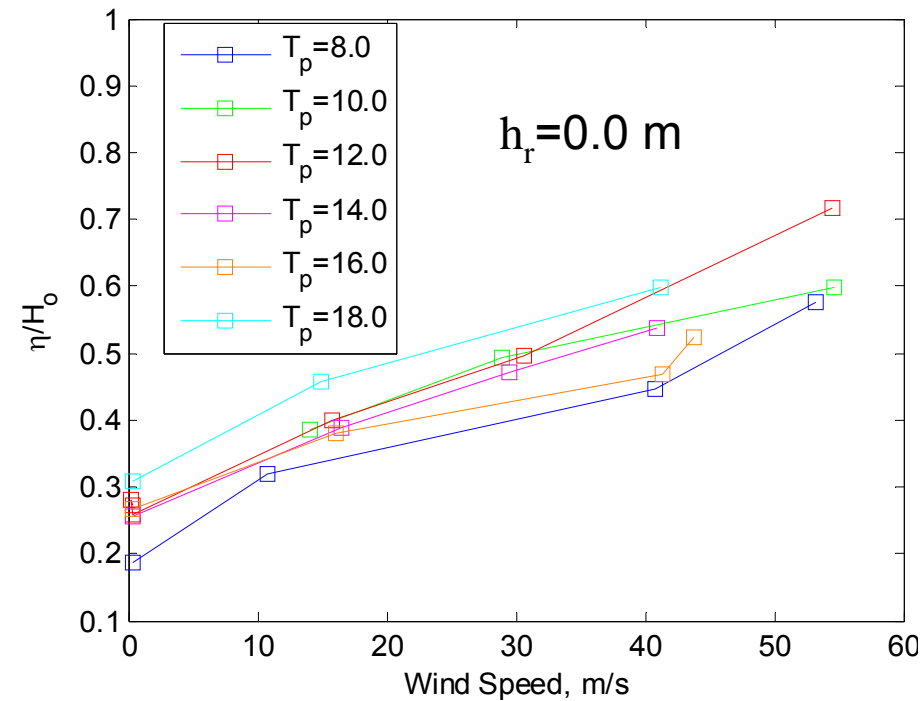
Wave Height Over Reef-top

- Wave height increase not related to wind speed?



Wind setup

- Wind setup important for strong winds or shallow depths

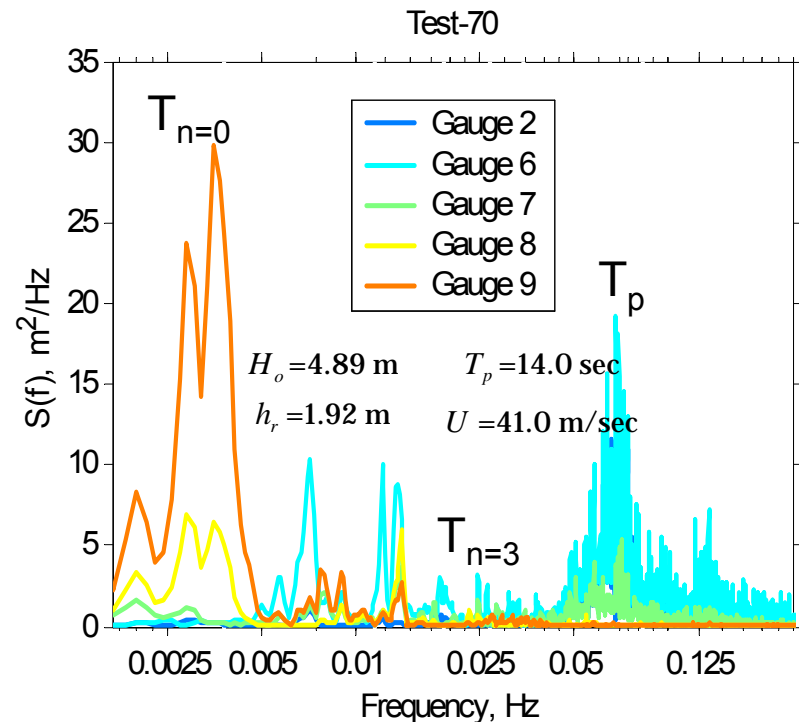
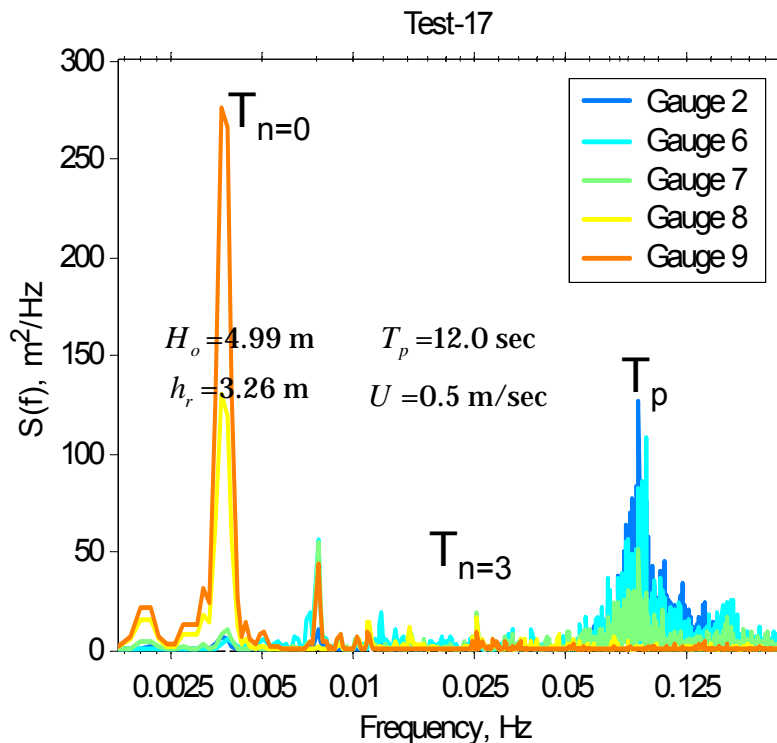


Spectral Wave Transformation

- Natural periods of oscillation for an open basin

$$T_n = \frac{4l_r}{(1+2n)\sqrt{gd_r}}$$

- Infragravity wave energy \gg gravity wave energy
- First and forth modes

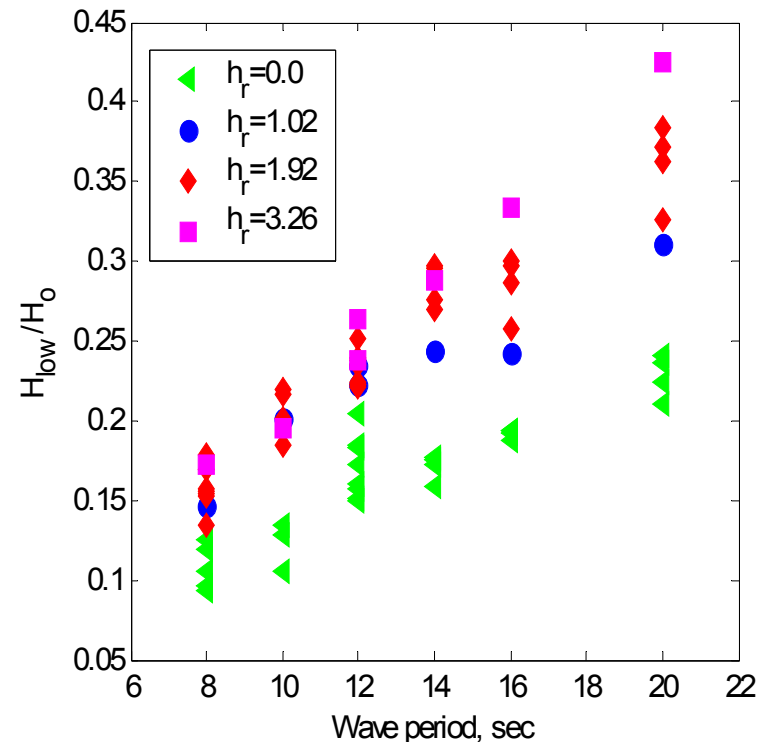


Infragravity Wave Energy

$$H_{low} = 4\sqrt{m_o}$$

$$m_o = \int_0^{f_c} S(f)df \quad \text{where } f_c = 0.02 \text{ Hz}$$

- Infragravity energy
 - < 0.02 Hz
 - Increases with increasing incident wave period
 - Increases with water depth



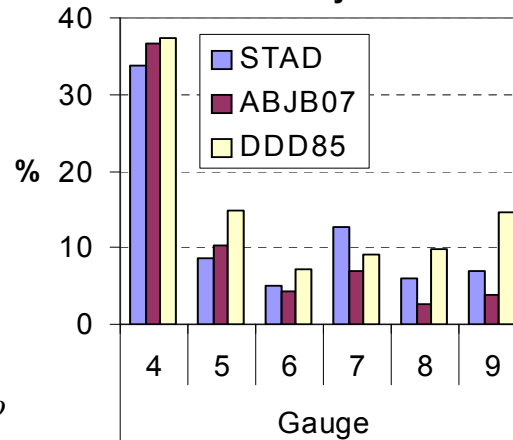
Wave Height Error Analysis

- Relative error (%)

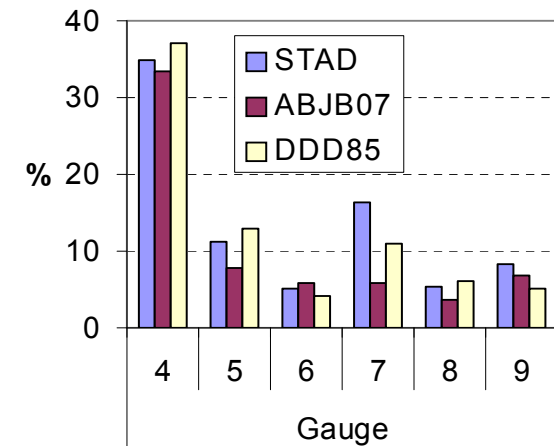
$$\varepsilon = \frac{100}{NH_o} \sum_{i=1}^N |H_{s,meas}^i - H_{s,comp}^i|$$

- Waves only
 - Average errors $< 0.15H_o$
 - Max errors $< 0.25H_o$
- Waves and Wind
 - Average errors $< 0.15H_o$
 - Max errors $< 0.25H_o$
- ABJB07 – Best results

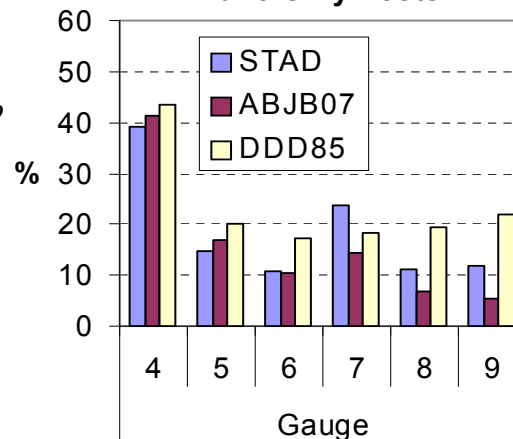
Hs Mean Relative Errors for Wave Only Tests



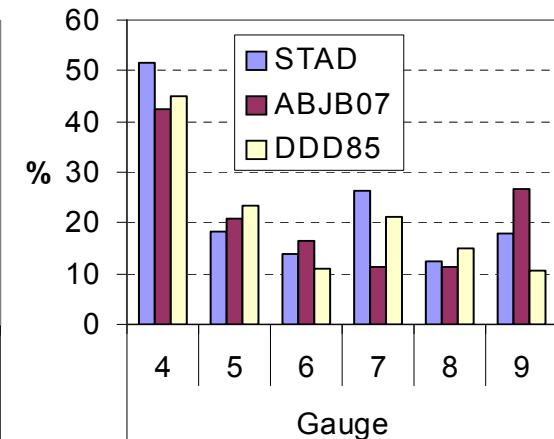
Hs Mean Relative Errors for Wind and Wave Tests



Hs Max. Relative Errors for Wave Only Tests



Hs Max. Relative Errors for Wind and Wave Tests



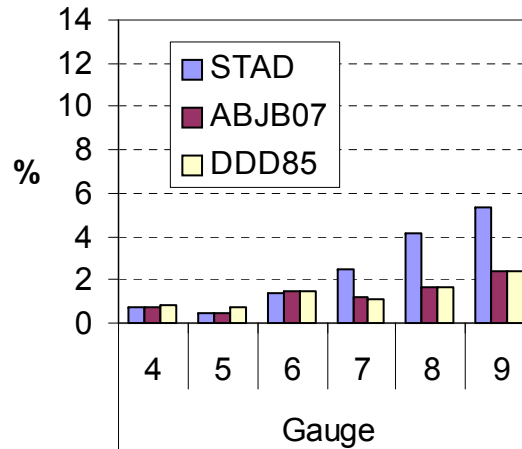
Setup Error Analysis

- Relative error (%)

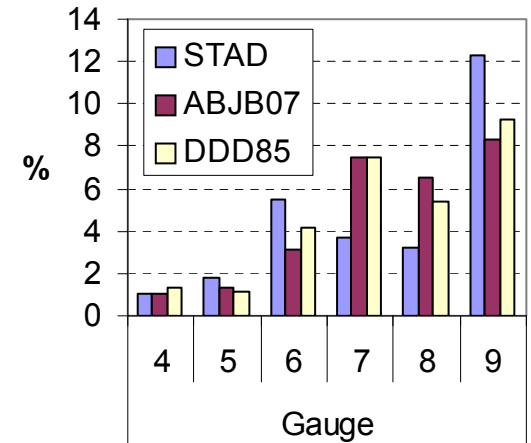
$$\varepsilon = \frac{100}{NH_o} \sum_{i=1}^N |\eta_{meas}^i - \eta_{comp}^i|$$

- Waves only
 - Average errors $< 0.05H_o$
 - Max errors $< 0.12H_o$
- Waves and Wind
 - Average errors $< 0.15H_o$
 - Max errors $< 0.35H_o$
- Excellent results for cases with no wind
- Ok results with wind
- ABJB07 – Best results

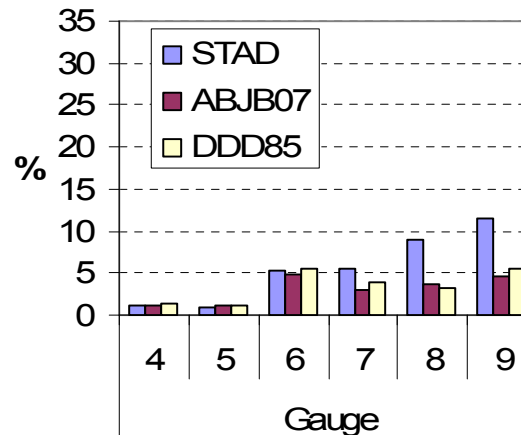
η Mean Relative Errors for Waves Only Tests



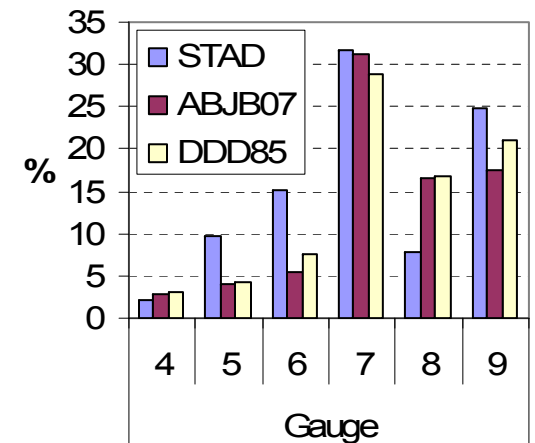
η Mean Relative Errors for Waves and Wind Tests



η Max. Relative Errors for Waves Only Tests



η Max. Relative Errors for Waves and Wind Tests

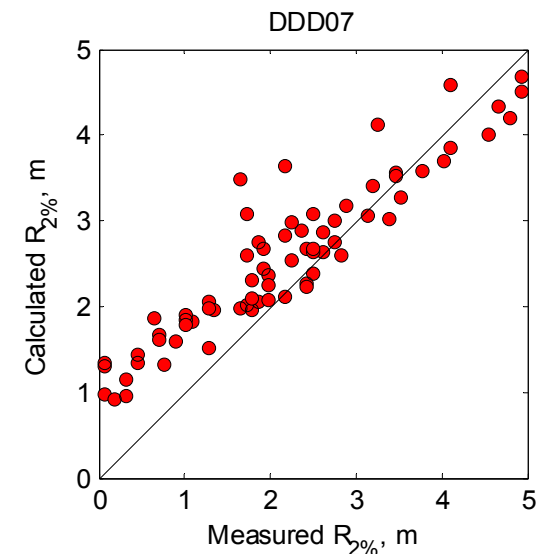
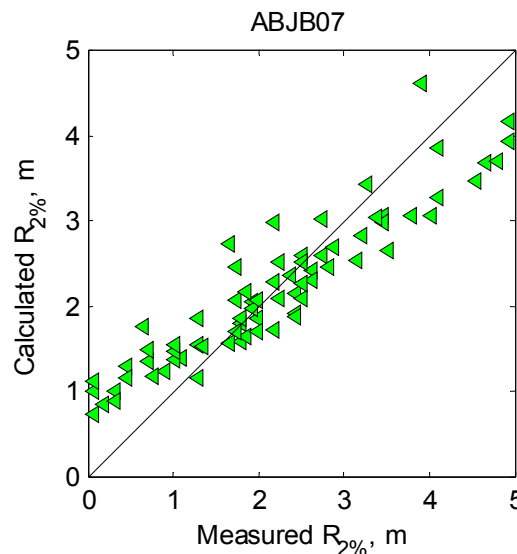


Runup, UM Dataset

- $R_{2\%}$ = Runup exceeded 2% of the time
- Runup with respect to still-water level
- Slope 1:12
- Mase (1989)

$$R_{2\%} = 1.86\xi^{0.71}$$

$$\xi = \tan \theta / \sqrt{H_r / L_o}$$



Discussion

- Although the 1-D models performed slightly better than the STWAVE/ADCIRC, their applicability is limited, and STWAVE and ADCIRC have a lot more physics such as wave-current interaction, wave growth terms, 2-D effects etc.
- Empirical coefficients likely difference than for sandy beaches and need to be estimated based on breaker types, wind, roughness etc.
- More work needed on the sensitivity of ADCIRC to grid resolution
- Despite the presence of long period infragravity motions, the models are able to predict reasonably well wave heights and average water levels

Summary and Conclusion

- Setup generated by strong winds is a significant contribution to water levels over fringing coral reefs
- Wind also causes increased wave breaking intensity causing the waves to break further offshore and reducing the setup
- STWAVE and ADCIRC are agreed relatively well with laboratory measurements of wave heights and water levels over a fringing reef
- 1-D wave energy balance models are robust, fast and are suitable for engineering applications, feasibility studies, etc.

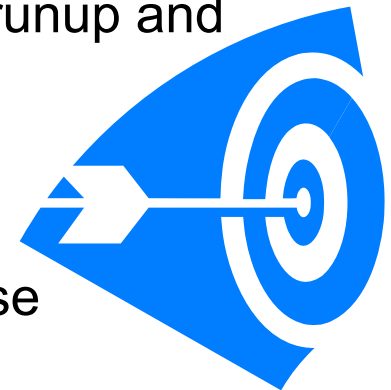
Future Work

- Include the formulation for wave breaking dissipation of Janssen and Battjes (2007) in STWAVE
- Incorporate a formulation for wave setup in STWAVE which would decrease the number of iterations between STWAVE and ADCIRC
- Develop and incorporate an empirical formulation for wave runup in STWAVE

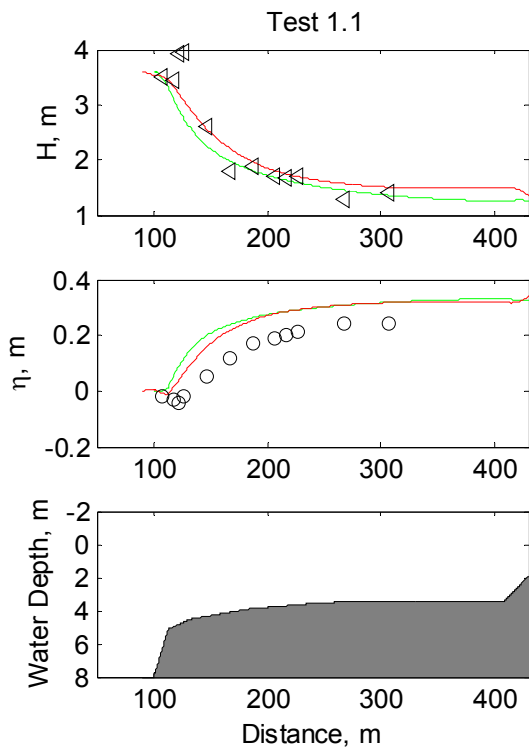
Thank you.
Questions?

Motivation

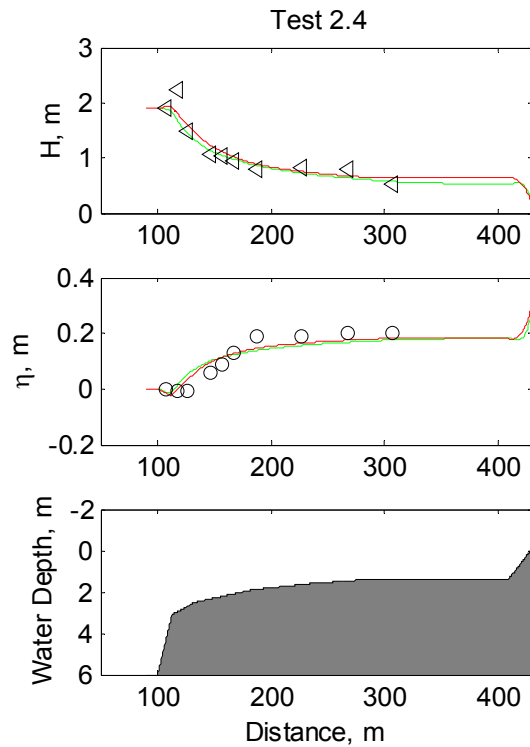
- Forecast
 - 36-hr forecast at 6-hr intervals – interpolated to 1-hr intervals
 - Unfeasible to simulate whole time history using complex nonlinear models such as Boussinesq-type models
 - Need to identify worst case conditions for potential runup and inundation for nonlinear models
 - Backup model
- Hindcast
 - Not enough data on hurricane events to merit the use nonlinear models
- Hypothetical events
 - Only need to be realistic
- Engineering Applications
 - Sometimes you just don't need so much accuracy



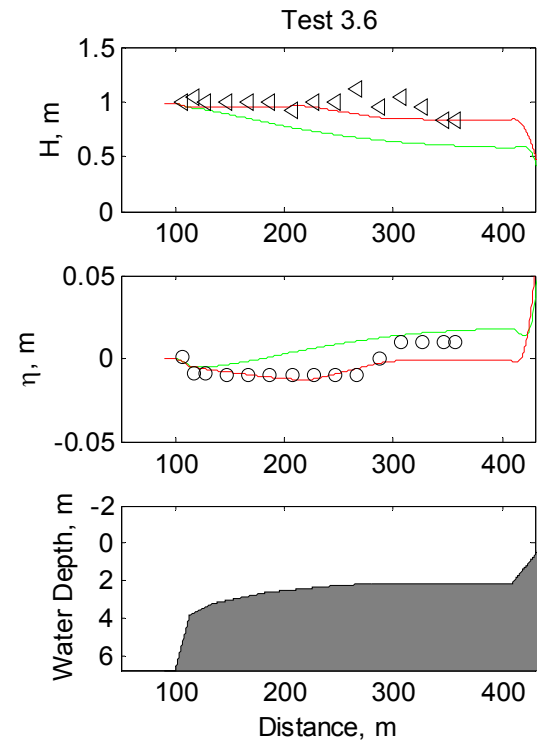
Hayman Island Dataset



$H_i = 3.44$ m $T = 6.8$ sec $h_r = 3.4$ m

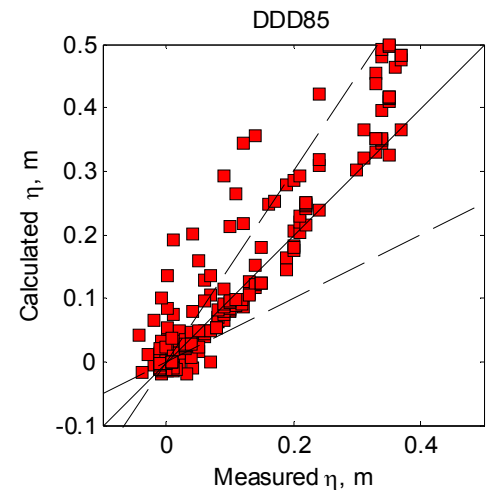
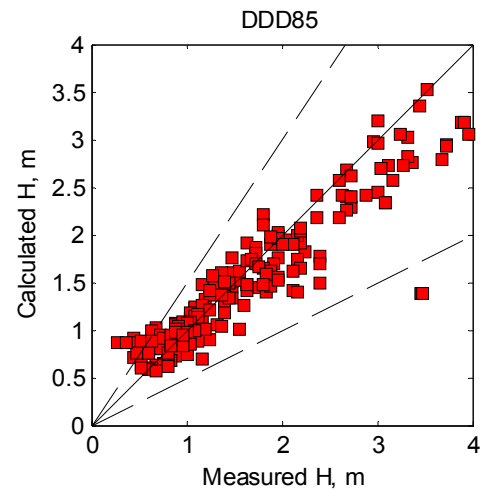
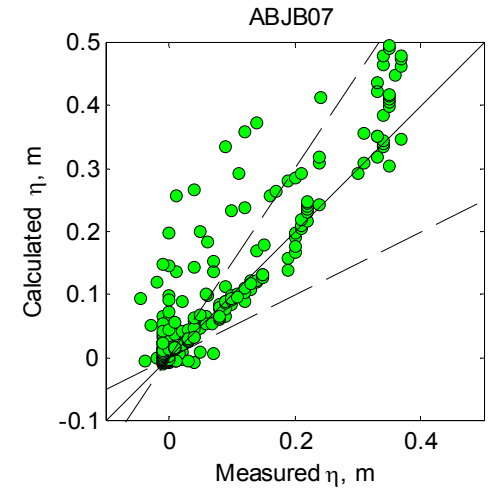
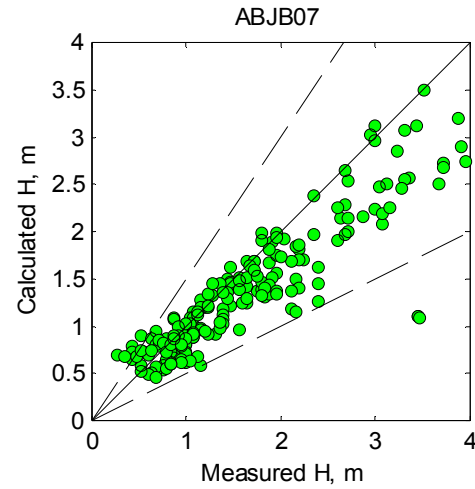


$H_i = 1.90$ m $T = 5.4$ sec $h_r = 1.4$ m



$H_i = 0.99$ m $T = 3.8$ sec $h_r = 2.1$ m

Hayman Island Dataset



Setup: Review of Empirical Relations

- Seelig (1983)

$$\Delta\eta_r = \begin{cases} -0.92 + 0.77 \log_{10}(H_o^2 T) & \text{for } h_r = 0 \text{ m} \\ -1.25 + 0.73 \log_{10}(H_o^2 T) & \text{for } h_r = 2 \text{ m} \end{cases}$$

- Gourlay (1996)

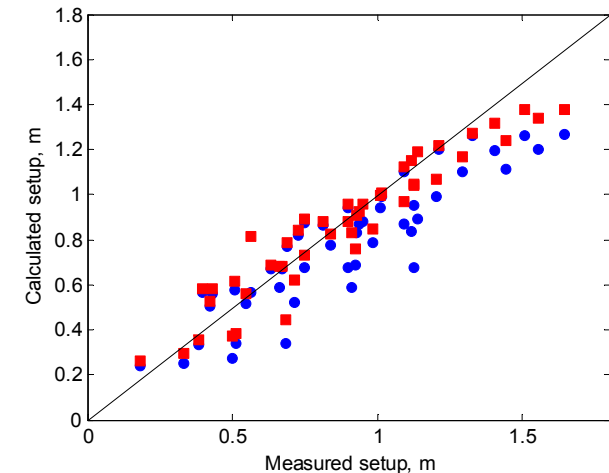
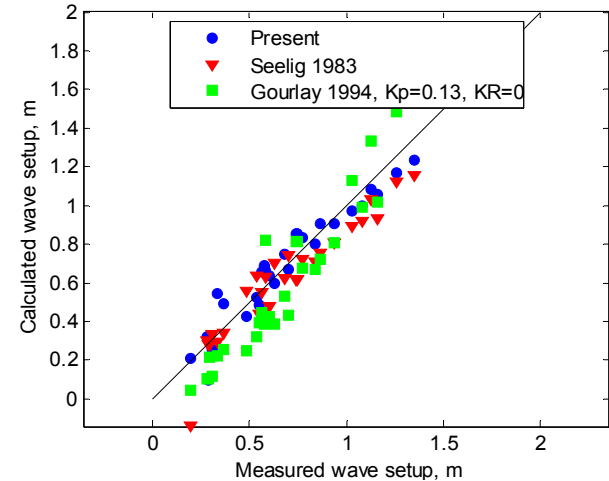
$$\Delta\eta_r = \frac{3}{64\pi} K_p \frac{g^{1/2} H_o^2 T}{(h_r + \eta_r)^{3/2}} \left[1 - K_R^2 - 4\pi K_r^2 \frac{1}{T} \sqrt{\frac{h_r + \eta_r}{g}} \right]$$

- Proposed

$$\Delta\eta_{total} = \Delta\eta_{wave} + \Delta\eta_{wind}$$

$$\Delta\eta_{wave} = -0.18h_r + 0.48 \log_{10}(H_o^2 T) - 5.53H_o / T^2$$

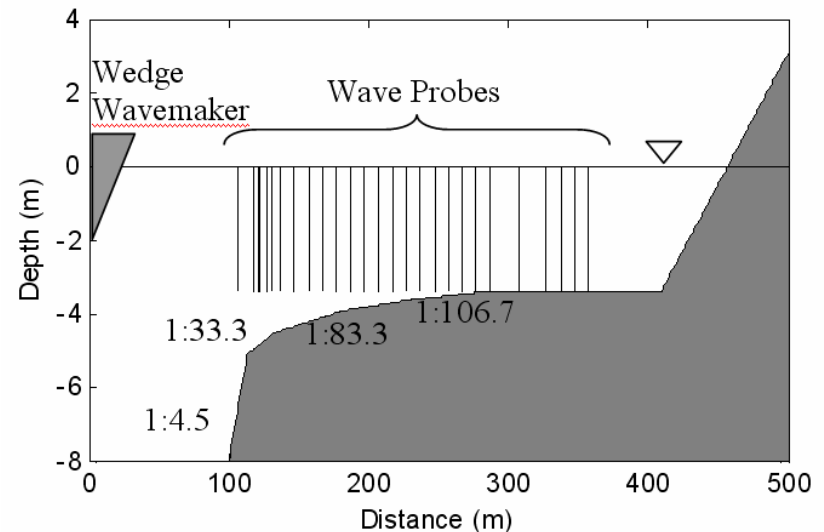
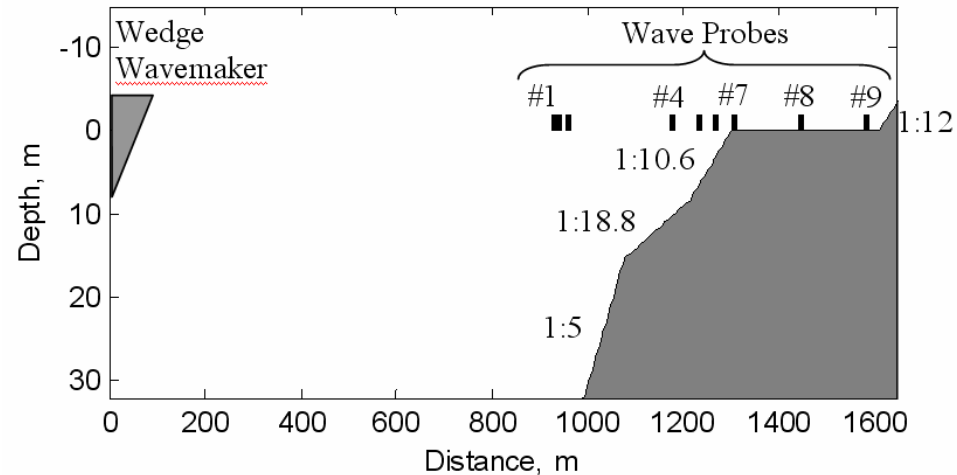
$$\Delta\eta_{wind} = \frac{WC_d U^2}{10^5 (h_r + \Delta\eta_{wave})}$$



● Only wave setup, ■ Wind and Wave setup

Laboratory Dataset

- University of Michigan Laboratory Study
 - 83 Tests
 - 1:64 scale Guam-type reef
 - Irregular waves
 - Wind and waves
- Hayman Island Fringing Reef Study (Gourlay, 1994, Coast. Eng. Vol. 23)
 - 18 Tests
 - 1:20 scale, Australian reef
 - Regular Waves
 - No wind



One-dimensional Models

- Wave energy balance equation

$$\frac{\partial}{\partial x}(EC_g \cos \theta) + D_b + D_f = 0 \quad E = \frac{1}{8} \rho g H_{rms}^2 \quad C_g = nC \quad n = \frac{1}{2} + \frac{kd}{\sinh 2kd}$$

– Wave Breaking

- Dally et al. 1985 (DDD85)

$$D_b = \frac{\kappa}{d} [EC_g - \min(E, E_s)C_g],$$

$$E_s = \frac{1}{8} \rho g (\Gamma d)^2$$

- Janssen and Battjes 2007 (ABJB07)

$$D_b = \frac{3\sqrt{\pi}}{16} \rho g B \bar{f} \frac{H_{rms}^3}{d} Q_b,$$

$$Q_b = 1 + \frac{4}{3\sqrt{\pi}} \left(R^3 + \frac{3}{2} R \right) \exp(-R^2) - \operatorname{erf}(R), \quad R = H_b / H_{rms}$$

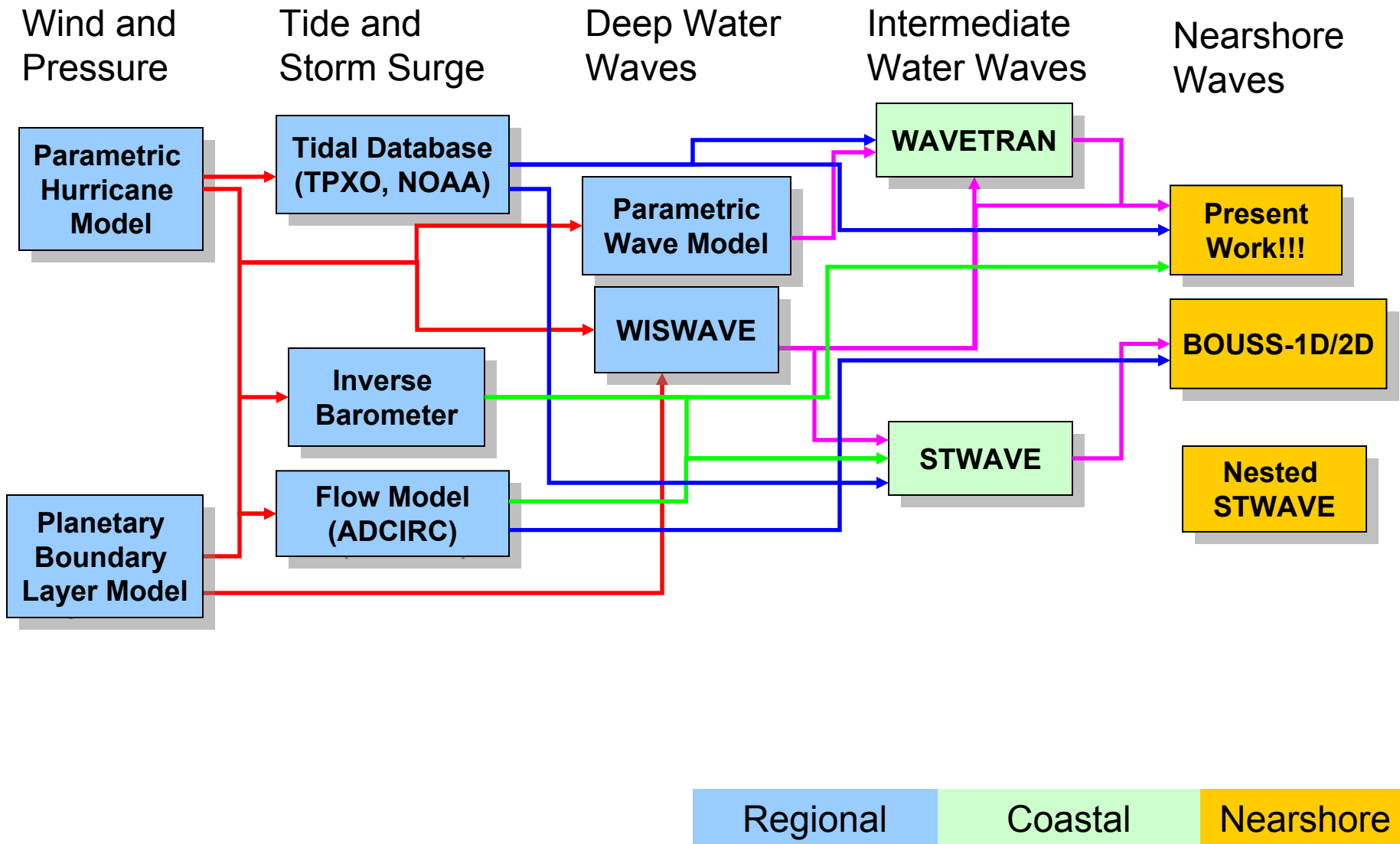
$$H_b = 0.88 \tanh(\gamma kd / 0.88) / k \quad \gamma = H_b / d = 0.5 + 0.4 \tanh(33H_o / L_o)$$

- Momentum balance

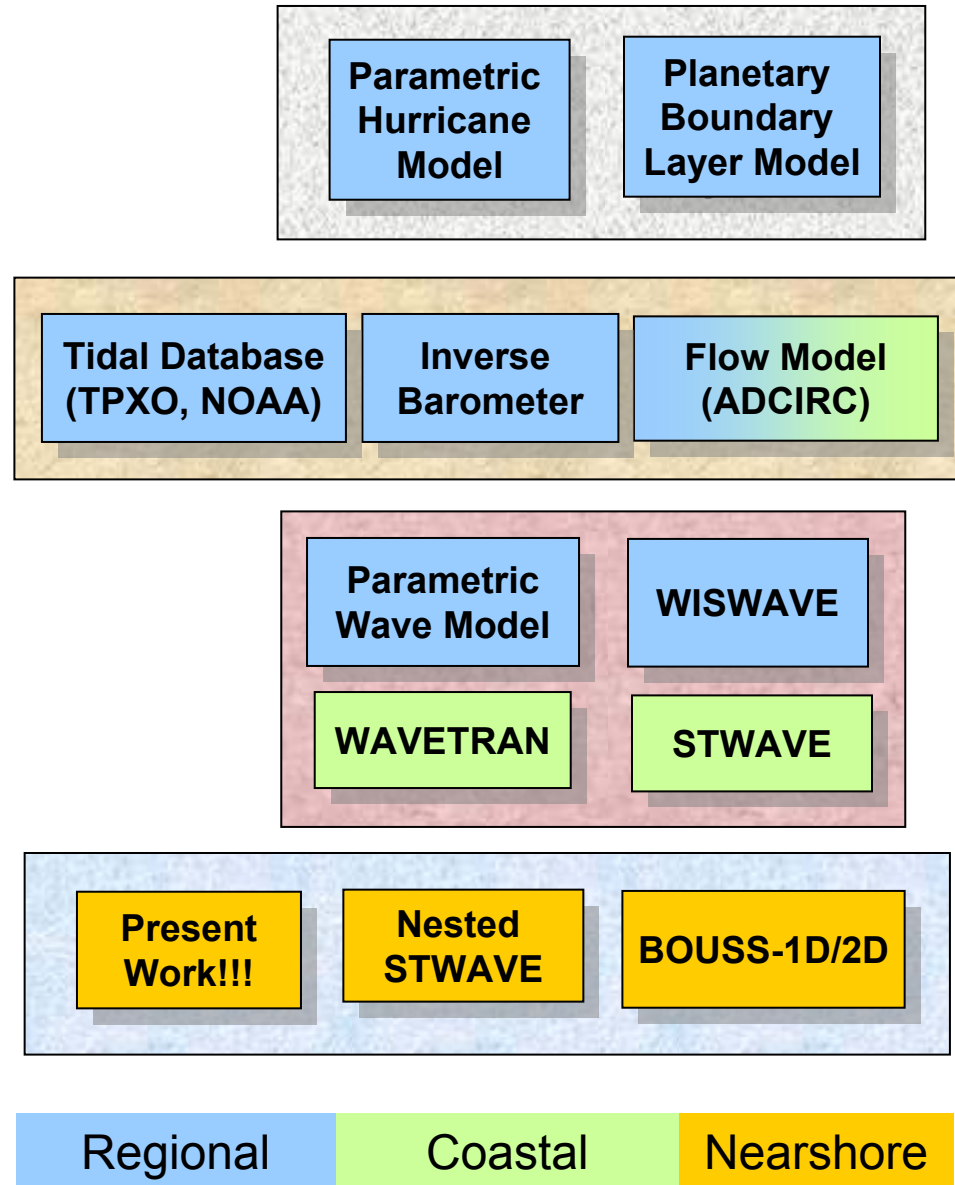
$$\rho g (h + \eta) \frac{\partial \eta}{\partial x} + \frac{\partial S_{xx}}{\partial x} = \tau_{wx}, \quad \tau_{wx} = C_d \rho_a U |U|, \quad S_{xx} = E \left(n(\cos^2 \theta + 1) - \frac{1}{2} \right),$$

$$H_s = 4\sqrt{m_o} \quad m_o = \int_{f_c}^{f_{ny}} S(f) df \quad \text{where } f_c = 0.02 \text{ Hz, } f_{ny} = \text{Nyquist Freq.}$$

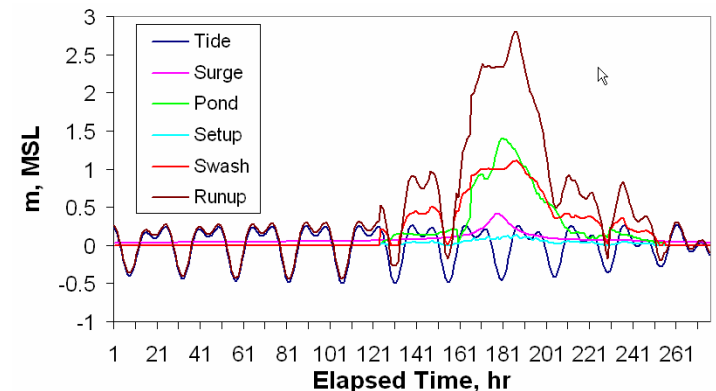
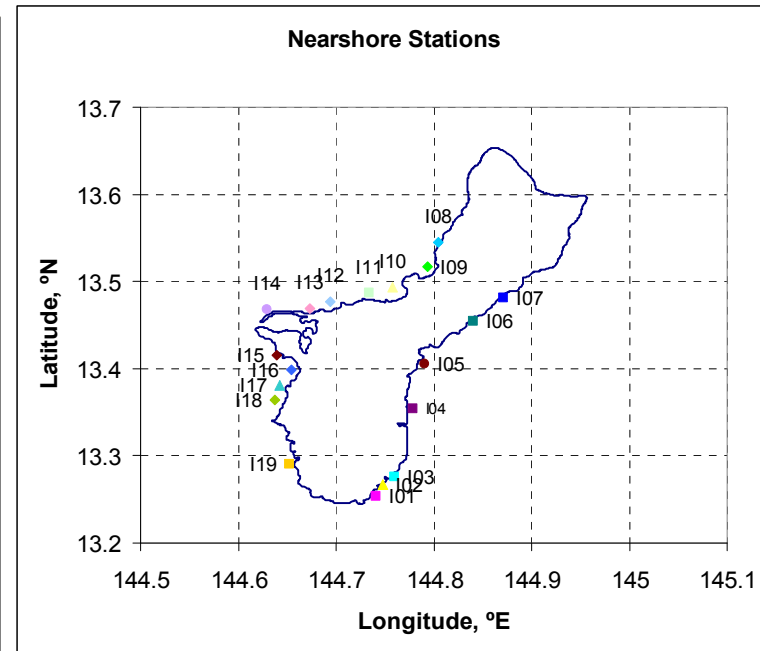
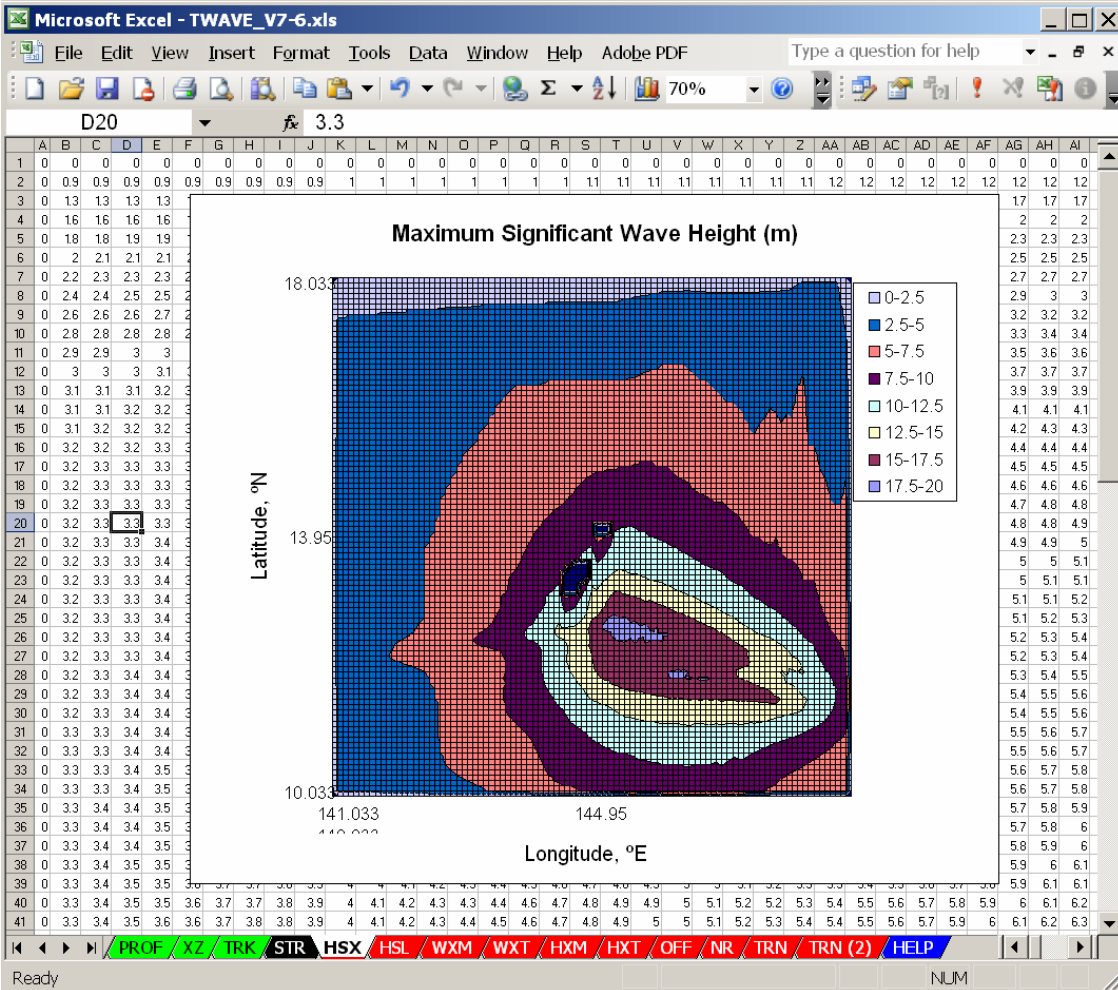
Coastal Modeling Package: TWAVE



- Sy

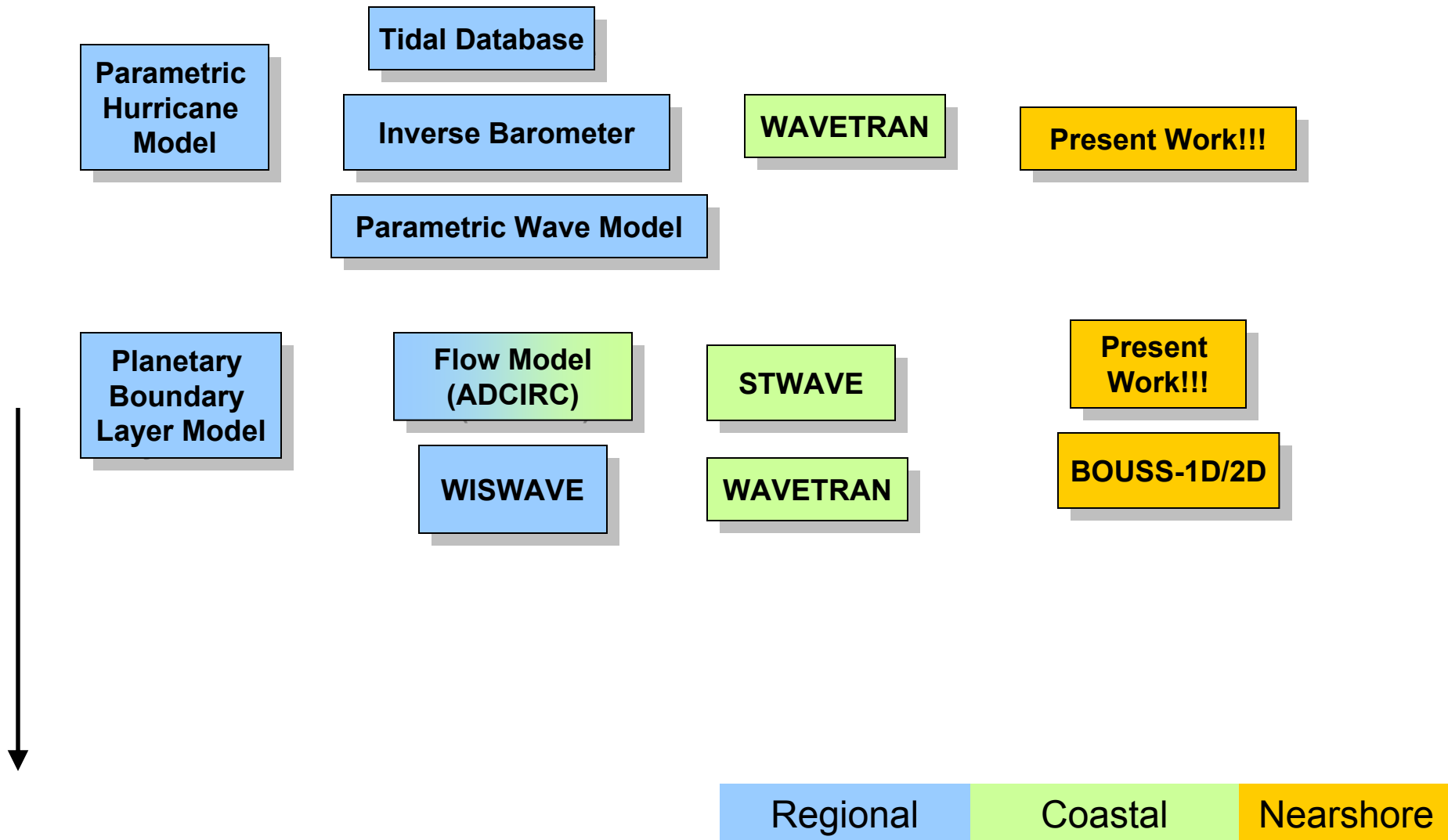


TWAVE: Example

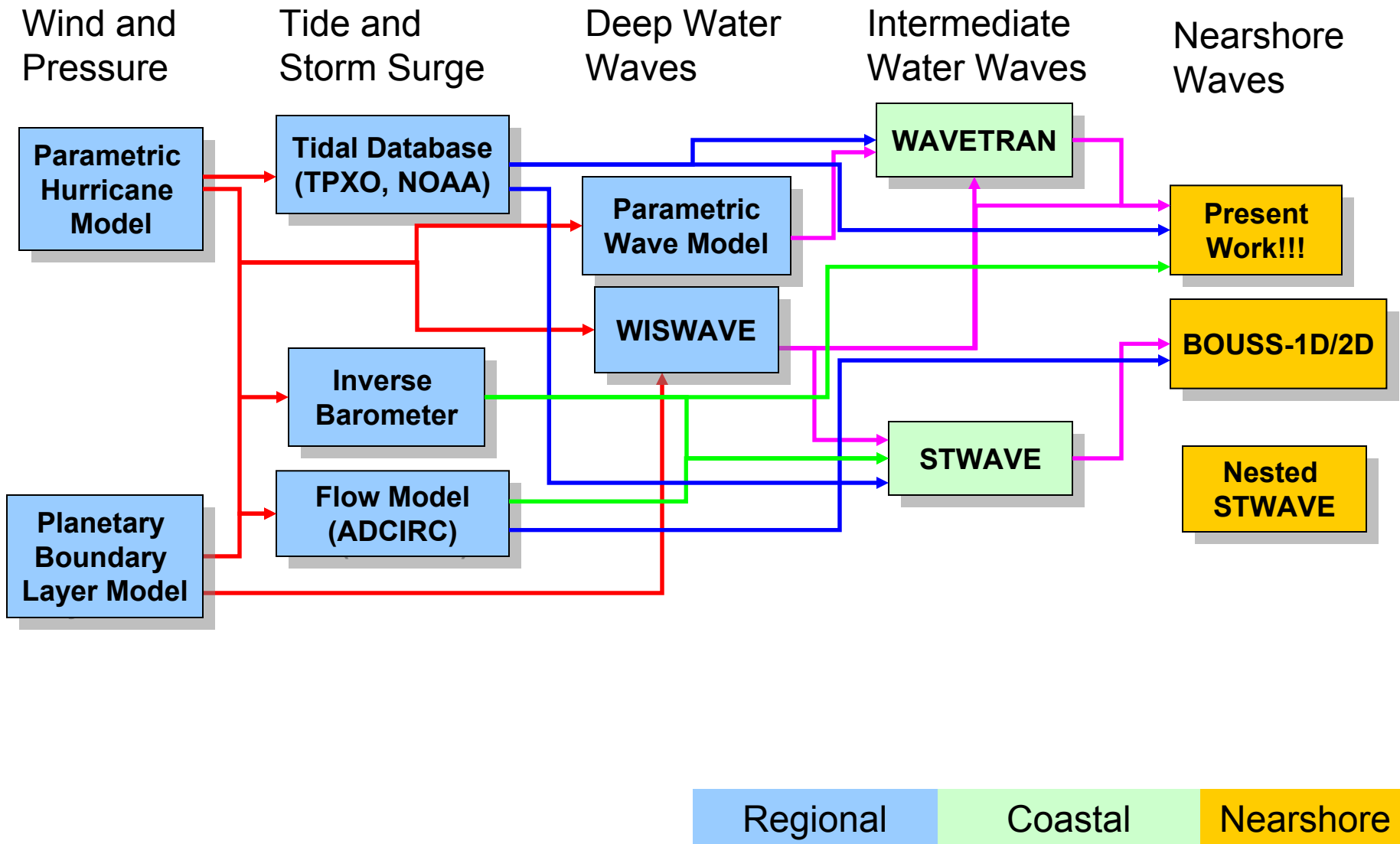


Multi-level Approach

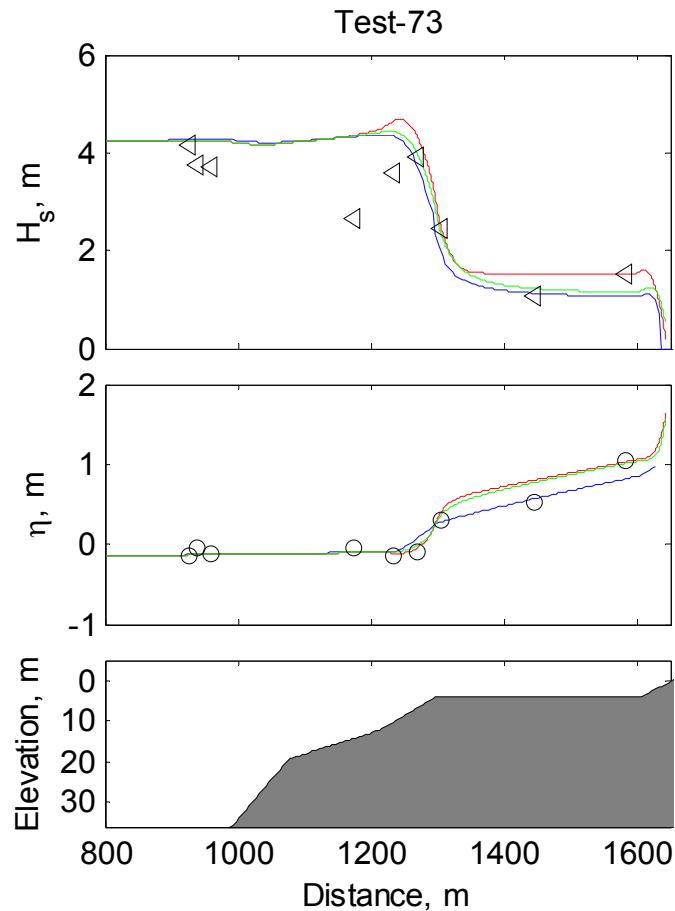
Coastal Modeling Package



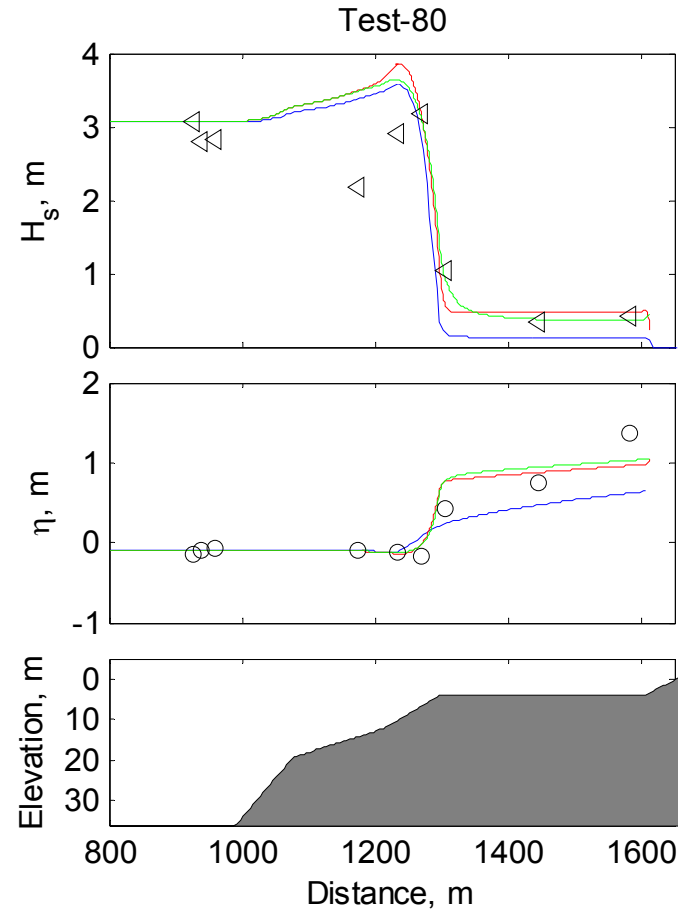
Coastal Modeling Package: TWAVE



UM Dataset, Wind and Waves



$H_o = 4.22$ m, $T_p = 10.0$ sec, $h_r = 1.92$ m, $U = 37.5$ m/s

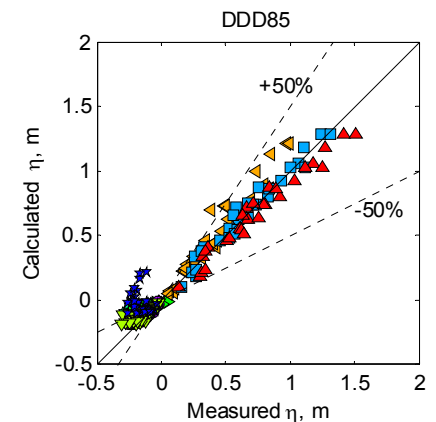
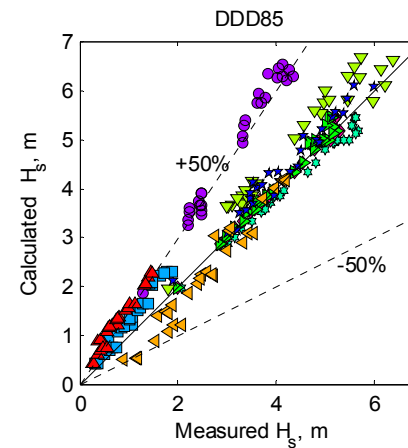
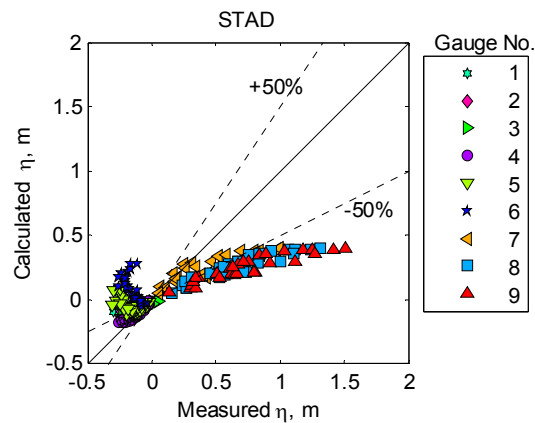
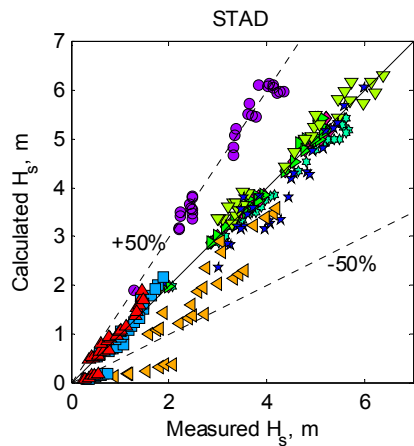
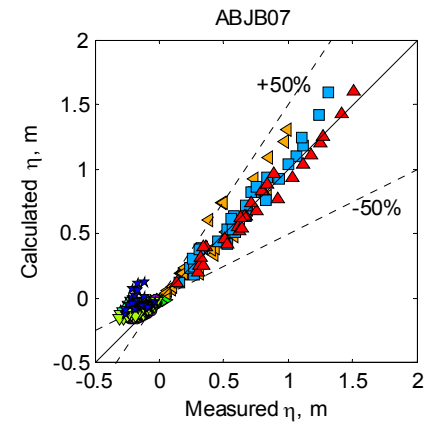
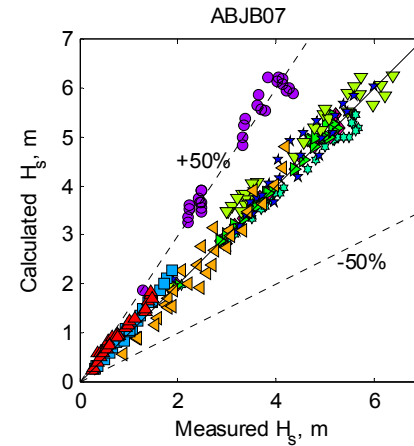


$H_o = 3.07$ m, $T_p = 12.0$ sec, $h_r = 0.0$ m, $U = 13.8$ m/s

— ABBJ07, — DDD85, — STAD

UM Dataset, Waves Only

- Hayman Island



UM Dataset, Wind and Waves

- Hayman Island

